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## Double sodium salt-promoted mesoporous MgO sorbent with high  $CO<sub>2</sub>$ sorption capacity at intermediate temperatures under dry and wet conditions



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### HIGHLIGHTS highlights are the control of the c

- The MgO·Na<sub>2</sub>CO<sub>3</sub>·NaNO<sub>3</sub> composites were prepared using an aerogel method.
- $\bullet$  The composite showed a high CO<sub>2</sub> sorption capacity at intermediate temperatures.
- $\bullet$  Na<sub>2</sub>CO<sub>3</sub> worked as a CO<sub>2</sub> carrier while  $NaNO<sub>3</sub>$  functioned as a reaction promoter.
- $\bullet$  Mg(OH)<sub>2</sub> in wet condition led to fast sorption rate and high sorption capacity.
- $\bullet$  One phase condition of NaNO<sub>3</sub> in cyclic test resulted in high stability of sorbent.

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### GRAPHICAL ABSTRACT



Mesoporous MgO·Na<sub>2</sub>CO<sub>3</sub>·NaNO<sub>3</sub> composites were prepared using supercritical drying of methanol for  $CO<sub>2</sub>$  capture in power plants at an intermediate temperature range between 250 and 450 °C. The effects of the molar ratio of salt, temperature, and gas composition on the  $CO<sub>2</sub>$  sorption were investigated under dry and wet conditions in order to clarify the sorption mechanisms and roles of NaNO<sub>3</sub> and Na<sub>2</sub>CO<sub>3</sub>. The composites exhibited excellent sorption capacities of 56.0 wt.% at 325 °C in pure CO<sub>2</sub> and 50.8 wt.% at 275 °C in a wet gas mixtures (10% CO<sub>2</sub>, 2.5% H<sub>2</sub>O, and balanced N<sub>2</sub>). The CO<sub>2</sub> sorption mechanism was dominated through the formation of MgCO<sub>3</sub> and Na<sub>2</sub>Mg(CO<sub>3</sub>)<sub>2</sub> with Na<sub>2</sub>CO<sub>3</sub> working as a CO<sub>2</sub> carrier, while NaNO<sub>3</sub> functioned as a reaction promoter. Under wet conditions, the formation of Mg(OH)<sub>2</sub> resulted in fast sorption rates and high capacities even at low  $CO<sub>2</sub>$  concentrations in the gas feedstock. One phase (liquid) condition of NaNO<sub>3</sub> and water vapor during a sorption and regeneration cycle resulted in a high stability of the sorbent. The working capacity in a 14 cycle test under  $N_2$  regeneration (10 min) at 450 °C was 31.8 wt.% at 325 °C in pure dry CO<sub>2</sub> and 29.4 wt.% at 275 °C with a wet CO<sub>2</sub> mixture. 2016 Elsevier B.V. All rights reserved.

### 1. Introduction

An excess of  $CO<sub>2</sub>$  in the atmosphere is widely accepted as one of the main contributors toward global warming [\[1\]](#page--1-0). Since fossil fuelbased power plants represent a massive  $CO<sub>2</sub>$  emission source, various efforts have been directed toward capturing  $CO<sub>2</sub>$  from the effluent gases to reduce the levels of  $CO<sub>2</sub>$  within the atmosphere.

CO2 sorption based on solid materials has received considerable attention toward overcoming the problems inherent to current  $CO<sub>2</sub>$ capture technologies. Various porous solid materials such as activated carbons  $[2,3]$ , zeolites  $[4,5]$ , porous silica composite  $[6]$ ,

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polymers [\[7,8\]](#page--1-0) and metal organic frameworks [\[9–11\]](#page--1-0) have been studied for the removal of  $CO<sub>2</sub>$  from emission gases. However, since the performances of these materials are not enough for practical application to  $CO<sub>2</sub>$  capture, the improved materials with higher  $CO<sub>2</sub>$  capacity are needed.

Recently, magnesium oxide (MgO) has received enormous interest as an alternative solid sorbent for the sorption of toxic chemicals and carbon dioxide due to its excellent physical properties, including: its large specific surface area, high pore volume, narrow pore size distribution, and high sorption capacity [\[12–15\].](#page--1-0)

Many MgO-based sorbents have focused on post-combustion CO2 capture and sorbent evaluations are usually carried out at relatively low temperatures (below 100 °C) [\[16–23\]](#page--1-0). Another important aspect related to carbon capture and sequestration (CCS) is pre-combustion  $CO<sub>2</sub>$  capture, which requires intermediate to high temperature conditions. If  $CO<sub>2</sub>$  can be efficiently captured from the effluent gas of a water–gas-shift reactor (WGSR), gasifier or combustor, at intermediate to high temperature conditions, more energy-efficient combustion processes with  $CO<sub>2</sub>$  capture can be designed due to relatively mild operating temperatures and accessible regeneration heat sources. For example, the temperature of flue gas in the Integrated Gasification Combined Cycle (IGCC) process is usually supplied to a gas turbine in the range of 150–450 °C  $[24]$ . Furthermore, low temperature WGSR can be applied to the synthesized gas to maximize  $H_2$  production in the IGCC. Therefore, sorbents can be regenerated by using heat sources obtained from process heat network.

The incorporation of alkaline metal salts to MgO materials has been shown to enhance the  $CO<sub>2</sub>$  sorption capacity at intermediate temperatures. It was reported that the peculiar effects of alkali metal nitrates were attributed to the presence of a high concentration of oxide ions in the molten alkali metal nitrates [\[25\].](#page--1-0) Mixtures of MgO and  $K_2CO_3$  prepared via a precipitation method exhibited a  $CO<sub>2</sub>$  sorption capacity of 8.69 wt.% at 375 °C and 1 bar under dry  $CO<sub>2</sub>$  condition [\[26\]](#page--1-0). The MgO·KNO<sub>3</sub> composite prepared from an aerogel method had a maximum sorption capacity of 13.9 wt.% at 325 °C and 1 bar under dry  $CO<sub>2</sub>$  condition. In particular, MgO promoted by double sodium salts synthesized via a wet mixing method had the highest  $CO<sub>2</sub>$  sorption capacity of 15.4 wt.% at 380 °C and 1 bar under dry  $CO<sub>2</sub>$  condition [\[27,28\],](#page--1-0) but the roles of NaNO<sub>3</sub> and Na<sub>2</sub>CO<sub>3</sub> in CO<sub>2</sub> sorption need to be clarified. The performance was still lower than those obtained for CaO at high temperatures and metal organic framework (MOF) and porous carbon at low temperatures [\[10,29,30\]](#page--1-0).

To reduce the costs associated with  $CO<sub>2</sub>$  capture, the performance of the sorbent needs to be further improved with regard to the sorption capacity and rate. And developed sorbents must be evaluated under the emitted gas conditions which contain water vapor for practical application. Typically, effluent gases from power plants contain  $10-15\%$  CO<sub>2</sub> with water vapor and the composition of effluent gas from WGSR in syn-gasifier plants is 15–60% CO<sub>2</sub>, 20–30% H<sub>2</sub>O, and other components  $[31-33]$ . Furthermore, it is reported that the presence of steam in the feed gas accelerates the  $CO<sub>2</sub>$  capture in several adsorbents [\[34\]](#page--1-0). Furthermore, the working capacity of sorption and regeneration is more important than the absolute sorption capacity.

In this study, we report the mesoporous  $MgO\cdot Na<sub>2</sub>CO<sub>3</sub>$ . NaNO<sub>3</sub> composite materials prepared via supercritical drying of methanol for  $CO<sub>2</sub>$  capture at intermediate temperatures. The  $CO<sub>2</sub>$  sorption capacity and rate of the as-prepared composites were evaluated at an intermediate temperature range between 200 and 400 $\degree$ C under dry and wet gas conditions. The mechanisms of  $CO<sub>2</sub>$  sorption at dry and wet gas conditions were elucidated by controlling compositions of double sodium salts quantitatively. The sorption mechanism of  $CO<sub>2</sub>$  uptake on the composite was analyzed through X-ray diffraction patterns (XRD), transmission electron microcopy

(TEM), scanning electron microscopy (SEM), energy-dispersive X-ray spectroscopy (EDS),  $N_2$  adsorption/desorption isotherms, and  $CO<sub>2</sub>$  sorption isotherms. In addition, the stability and working capacity of the composites were evaluated via cyclic testing under both wet (10% CO<sub>2</sub>, 2.5% H<sub>2</sub>O, and balanced N<sub>2</sub>) and dry (10% CO<sub>2</sub> and balanced  $N_2$ ) conditions.

### 2. Experimental

### 2.1. Chemicals

The following materials were used in this study: Toluene (Daejung, Korea; 99.8%), magnesium methoxide in methanol (Aldrich, USA; 7.85%),  $Na<sub>2</sub>CO<sub>3</sub>$  (Aldrich, 99.5%), and  $NaNO<sub>3</sub>$  (Duksan, Korea; 99.0%) were used without any further purification.  $N_2$ (Deokyang, Korea; 99.999%) was used as a purge gas during activation and cyclic regeneration.  $CO<sub>2</sub>$  (Deokyang; 99.999%) was applied for sorption. De-ionized water was used to generate the wet gas mixture.

### 2.2. Sorbent preparation

Mesoporous  $MgO\cdot Na<sub>2</sub>CO<sub>3</sub>$  NaNO<sub>3</sub> composites were synthesized via an aerogel method with a supercritical drying. At room temperature, a mixture of toluene (100 mL) and magnesium methoxide (20 mL) was stirred in a glass reactor for 30 min.  $Na<sub>2</sub>CO<sub>3</sub>$  and  $NaNO<sub>3</sub>$  (varying mass) were dissolved in distilled water (2.0 mL) and slowly added to the previously prepared solution via syringe. To minimize evaporation, the top of the reactor was covered with aluminum foil. The mixture was stirred vigorously overnight at room temperature to undergo full hydrolysis.

The hydrolyzed gel was transferred into a high pressure autoclave reactor. The reactor was subsequently flushed and pressurized up to 1 bar with  $N_2$  gas. The autoclave reactor was gradually heated from room temperature to 265 °C at the rate of 1.0 °C/ min, and maintained at 265  $\degree$ C for 10 min. The reactor pressure was rapidly reduced by releasing solvent vapors. The isolated powder was dried in an oven at 120 $\degree$ C for 12 h to remove residual organic solvents. As a final step, the dried powder was placed in a furnace. The following calcination procedure was applied under air: the temperature was ramped to  $450^{\circ}$ C at a heating rate of 10 °C/min and soaked at 450 °C for 3 h. The sample was stored for  $CO<sub>2</sub>$  sorption measurement.

Since some experimental temperatures were higher than the melting temperature of NaNO<sub>3</sub> (308 °C), excessive addition of  $NaNO<sub>3</sub>$  to the composite may lead to filling the composite pores with liquid NaNO<sub>3</sub> during sorption and/or regeneration. Therefore, the  $CO<sub>2</sub>$  sorption capacity and the sorption rate of MgO $\cdot$ NaNO<sub>3</sub> composite at the molar ratio of 1:0.2 were higher and faster than those of other composites at different molar ratios (1:0.5; 1:0.1; 1:0.4; and 1:0.6) (Fig.  $S1$ ). It was similar to the results observed from MgO·KNO<sub>3</sub> composites in the previous report  $[35]$ . Therefore, under the fixed molar ratio of  $MgO/NaNO<sub>3</sub>$  at 1:0.2, the effects of additional  $Na<sub>2</sub>CO<sub>3</sub>$  content on the physical properties and  $CO<sub>2</sub>$ sorption behavior of the MgO $Na<sub>2</sub>CO<sub>3</sub>$ . NaNO<sub>3</sub> composites were investigated. The MgO $Na_2CO_3$ ·NaNO<sub>3</sub> composites was investigated by fixing the molar ratio of NaNO<sub>3</sub>. MgO $\cdot$ Na<sub>2</sub>CO<sub>3</sub> $\cdot$ NaNO<sub>3</sub> composites with a mole ratio of  $MgO/Na_2CO_3/NaNO_3$  [1:X:0.2] (where 1, X, and 0.2 were the molar contents of MgO,  $Na<sub>2</sub>CO<sub>3</sub>$ , and  $NaNO<sub>3</sub>$ , respectively) were denoted as MgONaNa-X, where  $X = 0.05, 0.1$ , 0.2, 0.4, and 0.6 for the  $Na<sub>2</sub>CO<sub>3</sub>$  molar ratio. Additionally, pure MgO, MgO·Na<sub>2</sub>CO<sub>3</sub>, and MgO·NaNO<sub>3</sub> composites were prepared via the same procedure to be compared with the MgO $Na<sub>2</sub>CO<sub>3</sub>$ .  $NaNO<sub>3</sub>$  composites.

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