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# Elemental mercury oxidation over manganese-based perovskite-type catalyst at low temperature



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#### HIGHLIGHTS

• La<sub>0.6</sub>Sr<sub>0.4</sub>MnO<sub>3</sub> showed excellent performance on Hg<sup>0</sup> oxidation at 100–200 °C.

• La<sub>0.6</sub>Sr<sub>0.4</sub>MnO<sub>3</sub> oxidized Hg<sup>0</sup> efficiently in flue gas with low HCl concentration.

• La<sub>0.6</sub>Sr<sub>0.4</sub>MnO<sub>3</sub> had potential on low temperature SCR of NO with NH<sub>3</sub>.

• The adsorbed active surface oxygen species was significant for the Hg<sup>0</sup> oxidation.

• Good Hg<sup>0</sup> oxidation activity was gotten under the SCR atmosphere.

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#### ABSTRACT

 $La_{1-x}Sr_xMnO_3$  (LSx, x = 0/0.2/0.4/0.6) perovskite-type oxides catalysts were synthesized for elemental mercury (Hg<sup>0</sup>) oxidation in simulated coal-fired flue gas at low temperature. LS0.4 exhibited superior catalvtic behavior for  $Hg^0$  oxidation at 100–200 °C. The superior performance was mainly due to the surface adsorbed oxygen species in the catalysts. Effects of different components in the flue gas including HCl,  $O_2$ , SO<sub>2</sub>, H<sub>2</sub>O, NO and NH<sub>3</sub> on Hg<sup>0</sup> oxidation efficiencies were studied. The results suggested that HCl significantly enhanced  $Hg^0$  oxidation efficiency in the presence of  $O_2$  and 10 ppmv HCl was sufficient for enhancing the oxidation process. As the catalyst had strong oxygen storage capacity, the Hg<sup>0</sup> oxidation activity was less dependent on  $O_2$  concentration. As a result, the catalyst could be applied in the power plants burning low-chlorine coals. SO<sub>2</sub>, H<sub>2</sub>O and NH<sub>3</sub> had inhibitory effect on Hg<sup>0</sup> oxidation, while NO enhanced it. SO<sub>2</sub> could deactivate the catalyst and the deactivation was irreversible. In terms of mechanism, Hg<sup>0</sup> oxidation with LSx could be explained by the suprafacial process (Langmuir-Hinshelwood mechanism) whereby reactive species from adsorbed flue gas components reacted with adsorbed Hg<sup>0</sup>. The catalyst also had potential for selective catalytic reduction (SCR) of NO with NH<sub>3</sub> at low temperature, and the simultaneous removal of NO and Hg<sup>0</sup> over LS0.4 was investigated. The NO and Hg<sup>0</sup> conversion were higher than 50% and 85% when the space velocity was 40,000  $h^{-1}$ , respectively. The results indicated that the catalyst might be used to remove NO and Hg<sup>0</sup> simultaneously after the cold-side electrostatic precipitators in flue gas with low concentration of ash.

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#### 1. Introduction

Coal combustion is one of the main sources of anthropogenic mercury emission around the world. Mercury and its compounds, especially methyl mercury species, are of high toxicity and bioaccumulation [1]. Three forms of mercury exist in coal combustion flue gas: elemental mercury (Hg<sup>0</sup>), oxidized mercury (Hg<sup>2+</sup>) and particle-bound mercury (Hg<sup>P</sup>). Hg<sup>2+</sup> can be easily removed by the

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wet flue gas desulfurization (WFGD) due to its water solubility.  $Hg^{p}$  can be captured along with the fly ash by the electrostatic precipitators (ESP). However,  $Hg^{0}$  is difficult to control because it is extremely volatile and water-insoluble [2]. Therefore,  $Hg^{0}$  is the dominant form of mercury that released to the atmosphere. One of the feasible ways to remove  $Hg^{0}$  is to use catalytic oxidation method to convert  $Hg^{0}$  to  $Hg^{2+}$ .

The SCR catalyst was recognized as a promising catalyst for  $Hg^0$  oxidation, as it can be used for NO reduction simultaneously. In particular, the V<sub>2</sub>O<sub>5</sub>-based commercial SCR catalysts for NO removal have been reported as  $Hg^0$  oxidation catalysts [3,4]. Since the activities of V<sub>2</sub>O<sub>5</sub>-based commercial SCR catalysts are signifi-



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cantly affected by flue gas temperature, the catalytic activities are unstable due to the load variation of the boiler. Meanwhile, as the catalysts are placed before the ESP, they are deactivated easily due to the high concentration of dust in the flue gas [5,6]. It has been found that, relative to its effects on the efficiency of NO reduction, the catalyst deactivation could more significantly reduce Hg<sup>0</sup> oxidation efficiency [7]. In this case, there is a need for a novel catalyst that could perform well for Hg<sup>0</sup> oxidation at lower temperature, which can be located after the cold side ESP. Meanwhile, Huaneng group, a huge power generation company in China, has issued a strict NO<sub>x</sub> emission standard (less than 50 µg/m<sup>3</sup>) for the coalfired power plants. The existing commercial SCR catalysts cannot meet the emission standards. Therefore, to save the cost, the catalyst used for Hg<sup>0</sup> oxidation at lower temperature was required to remove the NO escaped from upstream simultaneously.

Fortunately, the low toxic  $MnO_x$  catalysts have been proved to be the co-benefit catalysts for NO and  $Hg^0$  removal at lower temperature, and they exhibit excellent performance under certain conditions [8–10]. However, the  $Hg^0$  oxidation efficiencies of these catalysts strongly depended on HCl concentration in the flue gas, a factor that cannot be controlled in the power plants. The catalysts exhibited excellent mercury oxidation activities at ~250 °C, which were not the typical flue gas temperature after the cold-side ESP. Considering the above limitations, Mn-based oxides could be modified to be used for Hg oxidation at lower temperature subject to less influence of HCl concentration.

The Mn-based perovskite oxides seem an attractive candidate for Hg<sup>0</sup> oxidation due to its excellent thermal stability, superior redox properties and great versatility [11,12]. The general formula of perovskite oxides is ABO<sub>3</sub>. The A-site ions fitted into the dodecahedral interstices are always large rare-earth or alkaline-earth metal ions. The B-site ions are always the transition metal ions which occupy oxygen octahedrons and play a dominant role in the catalytic process. It is generally believed that the properties of the B-site ions, the concentration of oxygen species, and the existence of lattice defects are responsible for the good catalytic activities of the perovskite-type oxides [13]. A-site cations in the perovskite oxides play a role of structure-stabilizing and partial substitution of A-site cations can modify the physicochemical properties of perovskite oxides. The incorporation of a low valence cation in the A-site decreases the valence that is compensated by the creation of oxygen vacancies and generation of more higher valence B-site cations. The most common Mn-based perovskite catalyst is LaMnO<sub>3</sub>, which has been investigated as a low temperature SCR catalyst recently [11].

Few researches investigated catalytic effects of LaMnO<sub>3</sub> for Hg<sup>0</sup> oxidation. Hence, some tests need to be carried out to investigate whether LaMnO<sub>3</sub> can be served as an efficient catalyst for Hg<sup>0</sup> oxidation. The abundant active oxygen species on the catalyst surface may be conducive for the formation of oxy-chloride or active chlorine species which are active for Hg<sup>0</sup> oxidation. In addition, it has been reported that the perovskites exhibits better catalytic performance when the A-site ions  $La^{3+}$  are partially substituted by  $Sr^{2+}$ [14]. This is because partial substitution of La<sup>3+</sup> with Sr<sup>2+</sup> can generate mixed-valence manganese (Mn<sup>3+</sup> and Mn<sup>4+</sup>) and more active oxygen species. The shift between Mn<sup>3+</sup> and Mn<sup>4+</sup> is beneficial for the generation of labile oxygen vacancies and bulk oxygen species [15]. The redox couple may also benefit the Hg<sup>0</sup> oxidation due to the Mars-Maessen mechanism in the absence of HCl. It seems likely that the LaMnO<sub>3</sub> modified by partial substitution of La<sup>3+</sup> by  $Sr^{2+}$  could oxidize Hg<sup>0</sup> with low concentration of O<sub>2</sub> and HCl in the flue gas when low rank coals are burned.

Accordingly, we hypothesize that the  $La_{1-x}Sr_xMnO_3$ (x = 0/0.2/0.4/0.6) perovskite catalysts could exhibit remarkable catalytic performance on Hg<sup>0</sup> oxidation with low concentration of O<sub>2</sub> and HCl in the flue gas at low temperatures. In the present work, the Mn-based perovskite oxides were synthesized and characterized to investigate the catalytic activity of the oxides on  $Hg^0$ oxidation. In order to improve the catalytic activity of the LaMnO<sub>3</sub>, the La<sup>3+</sup> ions were partially substituted by  $Sr^{2+}$  ions to increase the surface defects so as to generate more oxygen vacancies and active oxygen species. The catalytic performance of the oxides under conditions such as low concentration of O<sub>2</sub> and HCl at low temperature was also investigated, and the Hg<sup>0</sup> oxidation mechanism was identified. The effects of  $SO_2$ , H<sub>2</sub>O, NO and NH<sub>3</sub> on the Hg<sup>0</sup> oxidation efficiency were studied. Hg<sup>0</sup> oxidation efficiency under SCR atmosphere and the SCR activity of the selected catalysts (La<sub>0.6</sub>Sr<sub>0.4</sub>-MnO<sub>3</sub>) were considered as well. It is demonstrated that the synthesized perovskite oxides may serve as an environmentally friendly catalyst for simultaneous removal of NO and Hg<sup>0</sup> from coal combustion flue gas at low temperature.

#### 2. Experimental

#### 2.1. Preparation of catalysts

The  $La_{1-x}Sr_xMnO_3$  (x = 0/0.2/0.4/0.6) catalysts were prepared by complexation method using citric acid as a complexation agent [11]. They are denoted as LSx, where L is the raw LaMnO<sub>3</sub>, S is the doped Sr, and x represents the mole ratio of Sr/(Sr + La). Stoichiometric amounts of lanthanum nitrate, strontium nitrate and manganese nitrate were dissolved in deionized water. Citric acid was separately dissolved in distilled water and added to the mixed solution. The amount of the citric acid was equal to the total number of moles of the metal ions. The solution was then stirred and heated up to 60 °C to form the sol, and then turned to dry gel at 105 °C overnight. After spontaneous combustion at 180 °C, the dry gel turned to a spongy mixture. The mixture was then ground and the resulted powder was calcined from room temperature to 500 °C, which was maintained for 2 h. The powder was then calcined from 500 °C to 800 °C, which was kept for another 4 h. All the heating processes were conducted at a rate of 3 °C/min.

#### 2.2. Characterization of catalysts

The samples were investigated by X-ray powder diffraction (XRD) analysis (X'pert PRO, PANalytical, Holand) to understand the crystal phase structure. The surface property was analyzed by X-ray photoelectron spectroscopy (XPS) using VG Multilab 2000 X-ray photoelectron spectrometer. The pore size distribution and Bru nauer–Emmett–Teller (BET) surface area were determined using a Micromeritics ASAP 2020 N<sub>2</sub> adsorption apparatus. Fourier transform infrared (FTIR) spectra were investigated with a Nicolet Protegé 460 spectrometer in KBr pellets.

#### 2.3. Catalytic activity measurement

The mercury oxidation performance of LSx catalysts were evaluated on a fixed bed system, as shown in Fig. 1. The system consisted of a simulated flue gas system with an Hg<sup>0</sup> permeation device (VICI Metronics), a quartz reactor (length 550 mm, inner diameter 10 mm) and a vertical furnace, an on line RA-915 M mercury analyzer (sensitivity:  $0.1 \,\mu g/m^3$ , Lumex-Marketing JSC, Russia) coupled with a mercury speciation conversion system and a carbon trap to purify the exhaust. The simulated flue gas was prepared by mixing individual gases. The total flow rate was 1 L/min. A flow of pure N<sub>2</sub> passed the permeation tube carrying the Hg<sup>0</sup> vapor to provide a constant feed of mercury concentration (~60  $\mu g/m^3$ ). The water vapor was fed by a high performance liquid chromatography (HPLC) pump (P600, LabTech). The tube was heated to 150 °C to ensure all the liquid water turns into steam. Download English Version:

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