



# Warm plasma catalytic reforming of biogas in a heat-insulated reactor: Dramatic energy efficiency and catalyst auto-reduction



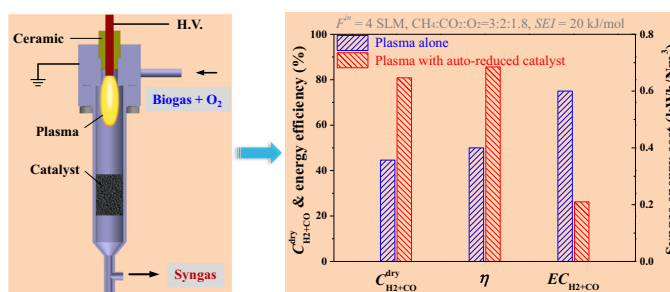
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## HIGHLIGHTS

- Highly efficient warm plasma catalytic reforming of biogas was reported.
- Ni-based catalyst could be auto-reduced in the heat-insulated reactor.
- Energy efficiency improved dramatically to 86%.
- Syngas energy cost reduced significantly to  $0.21 \text{ kW h/N m}^3$ .

## GRAPHICAL ABSTRACT



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## ABSTRACT

Highly efficient warm plasma catalytic reforming of biogas in a compact and heat-insulated reactor using gliding arc discharge with a co-axial electrode configuration and Ni-based catalyst was reported. The effect of inlet flow rate at a special energy input (SEI) of 20 kJ/mol for the plasma alone was first investigated and the inlet flow rate was selected at 4 SLM. Then, it was found that the Ni-based catalyst could be auto-reduced by the outgoing gas from the warm plasma via comparing with the pre-reduced catalyst in the reforming reaction testing and characterizations of Brunauer–Emmett–Teller (BET) surface area, X-ray diffraction (XRD) and transmission electron microscopy (TEM). The effect of catalyst-bed position ( $l$ ) was also examined. Feeding with the molar ratio of  $\text{CH}_4:\text{CO}_2:\text{O}_2 = 3:2:1.8$ , for the warm plasma with the auto-reduced Ni/CeO<sub>2</sub>/Al<sub>2</sub>O<sub>3</sub> catalyst located at  $l = 4 \text{ cm}$ , dry-basis concentration of syngas rose substantially to 81% and energy efficiency improved dramatically to 86%. Syngas energy cost reduced significantly to  $0.21 \text{ kW h/N m}^3$ , which is nearly a threefold reduction compared with the plasma alone. The stability of the warm plasma catalytic reforming was preliminarily evaluated over time-on-stream (TOS) of 13.5 h.

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## 1. Introduction

Biogas, typically consisting of 60% CH<sub>4</sub> and 40% CO<sub>2</sub>, is a renewable, carbon-neutral and widely available resource for syngas (H<sub>2</sub> + CO) production via reforming [1,2]. Oxidative reforming (also

called partial oxidation) of biogas with O<sub>2</sub> or air is of low energy cost due to its mild exothermicity and has attracted more attention. Conventional catalytic technique for oxidative reforming bears a drawback of hot-spot which results in catalyst sintering and subsequently deactivation [3,4].

An alternative technique is non-thermal plasma, in which reactant molecules collide with energetic electrons to produce radicals via excitation and dissociation pathways, followed by radical reactions to form final products. It has several merits, such as

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compactness, feed flexibility, durability, and quick start. Non-thermal plasma can be categorized into two types, *i.e.* cold and warm plasmas [5]. Cold plasma, usually generated by corona or dielectric barrier discharges, suffers high energy cost of syngas ( $>10 \text{ kW h/N m}^3$ ) or low energy efficiency ( $<10\%$ ) in biogas reforming [6–10]. Warm plasma, normally produced by spark or gliding arc discharges, exhibits much higher energy efficiency than cold plasma for biogas reforming [11–16]. Using gliding arc discharge, Wu et al. [11] reported energy efficiency of 27% and syngas energy cost of  $3.3 \text{ kW h/N m}^3$  with 36% of  $\text{CH}_4$  conversion and 35% of  $\text{CO}_2$  conversion at a molar ratio of  $\text{CH}_4:\text{CO}_2 = 1$ ; Tu et al. [12] reported energy efficiency of 41% and syngas energy cost of  $4.0 \text{ kW h/N m}^3$  with 13% of  $\text{CH}_4$  conversion and 8% of  $\text{CO}_2$  conversion at a molar ratio of  $\text{CH}_4:\text{CO}_2 = 0.43$ . In our previous work, using spark discharge, energy efficiency of 41% and syngas energy cost of  $4.3 \text{ kW h/N m}^3$  with 76% of  $\text{CH}_4$  conversion and 57% of  $\text{CO}_2$  conversion at  $\text{CH}_4:\text{CO}_2:\text{O}_2$  molar ratio of 3:2:1 was reported [14]. Subsequently, developed a rotating-electrode spark-shade plasma, energy efficiency of 54% and syngas energy cost of  $1.2 \text{ kW h/N m}^3$  with 83% of  $\text{CH}_4$  conversion and 35% of  $\text{CO}_2$  conversion at  $\text{CH}_4:\text{CO}_2:\text{O}_2$  molar ratio of 3:2:2 was reported [16].

Although the energy efficiency of warm plasma in biogas reforming is much higher than that of cold plasma, it should be further improved to meet the requirement of practical application. The exploration for the combination of warm plasma with catalyst in biogas reforming has been made. We [17] recently explored the spark-shade plasma with Ni-based catalyst kept at  $800^\circ\text{C}$  by a tube furnace, assuming that the plasma could supply the heat energy for the subsequent catalytic reaction at  $800^\circ\text{C}$ , and achieved energy efficiency of 70% and syngas energy cost of  $1.0 \text{ kW h/N m}^3$  with 100% of  $\text{CH}_4$  conversion and 35% of  $\text{CO}_2$  conversion at  $\text{CH}_4:\text{CO}_2:\text{O}_2$  molar ratio of 3:2:1.8. Rafiq et al. [18] investigated gliding arc discharge followed by  $\text{Ni}/\text{Al}_2\text{O}_3$  catalyst in a heat-insulated reactor and reported energy efficiency of 59% and syngas energy cost of  $0.8 \text{ kW h/N m}^3$  with 86% of  $\text{CH}_4$  conversion and 4% of  $\text{CO}_2$  conversion at  $\text{CH}_4:\text{CO}_2:\text{O}_2$  molar ratio of 3:2:2. However, due to their gliding arc technique using two-dimensional (2D) flat electrode configuration, the complete stoichiometric burning of propane was required to increase the temperature during the start-up

stage. Moreover, almost no  $\text{CO}_2$  was converted and syngas energy cost should be further reduced.

In the present paper, we report warm plasma catalytic reforming of biogas in a compact and heat-insulated reactor using a three-dimensional (3D) co-axial electrode configuration for gliding arc discharge. It features dramatic energy efficiency, easy and fast start-up where any assistance do not need. Additionally, the Ni-based catalyst for biogas reforming is usually available in the oxide form and hence the catalyst pre-reduction prior to start-up is necessary. This work revealed the Ni-based catalyst could be auto-reduced during the start-up, which offers a simple technique without any activation or pre-reduction of catalyst for plasma catalytic reforming.

## 2. Experimental

### 2.1. Warm plasma catalytic reactor

The schematic diagram of the warm plasma catalytic reactor, which is made of stainless steel, was shown in Fig. 1(a). The cylinder with inner diameter of 20 mm was grounded. The high-voltage electrode with a ceramic electric insulator was located at the axis of the cylinder and powered by an AC high-voltage power supply (CTP-2000K, Nanjing Suman electronics Co., China) to generate gliding arc discharge. For heat insulation, ceramic fiber cotton was wrapped around the reactor (Fig. 1(b)). The simulated biogas ( $\text{CH}_4:\text{CO}_2 = 3:2$ ) mixed with  $\text{O}_2$  at a molar ratio of  $\text{CH}_4:\text{CO}_2:\text{O}_2 = 3:2:1.8$  was used as the feed gas and introduced tangentially into the reactor from its top at room temperature. This experiment was conducted at atmosphere pressure and the gas flow rates were controlled by mass flow controllers.

The supported  $\text{Ni}/\text{CeO}_2/\text{Al}_2\text{O}_3$  catalyst was packed into the cylinder and the temperature variation with axial distance from the catalyst-bed entrance was measured by a thermocouple. The catalyst-bed position was indicated by the distance ( $l$ ) between the entrance of the catalyst bed and the top of the cylinder. It should be pointed out that, for heating the catalyst, the thermal energy only came from the warm plasma and there was not any extra heater.

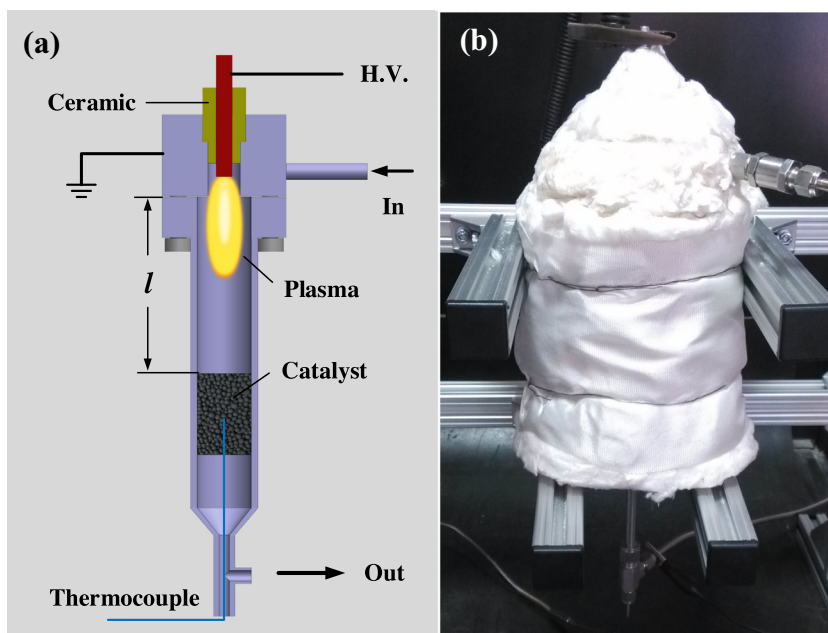


Fig. 1. (a) Schematic of the warm plasma catalytic reactor and (b) photo of the reactor with heat-insulation jacket.

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