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Synthesis of industrial park water reuse networks considering treatment systems and merged connectivity options

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ABSTRACT

A number of optimization approaches for the synthesis and design of effective wastewater regeneration and reuse networks in industrial parks have been proposed to support decision making for careful management of water resources by the industrial sector. The approaches allow the identification of optimal wastewater treatment and reuse strategies. All such available methods for interplant water network synthesis assign a single pipeline for every viable water allocation identified, which results in inefficient and costly pipe networks. Instead, this work presents a water network design approach that accounts for a number of pipeline merging scenarios for wastewater reuse and regeneration networks considering central and decentral treatment options. Merging common pipe segments that carry similar water qualities allows for cost-improvements in network design, in addition to reducing the overall pipeline network complexity due to fewer required interconnecting pipes. The benefits of the proposed method are illustrated with a case study.

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1. Introduction

Industrial water and wastewater management has become a research priority in many regions, due to the vast scale of waterintensive activities in many industrial operations, which in turn are continually increasing as a result of industrial expansion initiatives. Moreover, industrial sites that lie in proximity to coastal areas involve large volumes of unused wastewater being diverted back into the sea, which negatively impacts aquatic life (Englert et al., 2013). Industrial wastewater reuse certainly alleviates the depletion of available freshwater sources that are present around industrial areas. Hence, wastewater reuse also helps reduce the excessive wastewater quantities being discharged back into natural water bodies. Identifying appropriate wastewater treatment alternatives is considered of significant importance due to the stringent discharge limits being imposed on industrial wastewater, as well as the strict effluent standards that industries are expected to adhere to. Potential opportunities for industrial wastewater reuse (Ehrenfeld and Gertler, 1997) would absolutely vary from

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http://dx.doi.org/10.1016/j.compchemeng.2016.02.003 0098-1354/© 2016 Elsevier Ltd. All rights reserved. one industry to another, depending on the quantity and quality of wastewater produced.

The design of cost-effective wastewater regeneration and reuse networks has been the primary focus of many previous studies. Chew et al. (2008, 2009) developed a centralized hub topology that involves the collection, treatment and distribution of water amongst coexisting plant arrangements within an industrial zone. Rubio-Castro et al. (2010, 2011) devised a Mixed Integer Non-Linear (MINLP) optimization model for interplant water networks whilst incorporating environmental regulations for wastewater discharge. Additionally, a reformulation of the same problem has also been proposed, which handles bilinear terms involved. Several Multi-objective optimization strategies for water network design in Eco-Industrial Parks have also been studies by Biox et al. (2012). More recent research contributions in the field of water network design have also been proposed. For instance, a structured representation that is capable of capturing the spatial aspects of water network design (Alnouri et al., 2014a) has been introduced in which effective planning of wastewater reuse networks has been handled with a focus on the following aspects: (1) accounting for site locations and the spatial distribution of all plant entities that lie within geographic proximity within an industrial zone(2) the ability of incorporating layout information associated with processing facilities that entail water use or production, (3) capturing information related to the presence of common city infrastructure, such as the

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Nomenclature			~max	Maximum permissible pollutant a composition in
	Indicas		c,jp	Maximum permissible pollutant c composition m
	a	First lovel node associated with pipeline branching		sink J, plant p (ppm)
	u h	Cocond lovel node associated with pipeline branching	ρ	Density in kg/m ³
	D	second level node associated with pipeline branch-	γ	Annual cost factor (1/yr)
		Illg		
	С	Inird level node associated with pipeline branching	Variables	S
	n ·	Nth level node associated with pipeline branching	D _{rp}	Wastewater mass flowrate discharged by intercep-
	1	Water Source		tor r, plant p (kg/h)
	j	Water Sink	D _{st}	Wastewater mass flowrate discharged by central
	р	Plant/Process		interceptor s of type t (kg/h)
	r	De-central treatment	D _{ip}	Wastewater mass flowrate discharged by source i,
	S	Central treatment		plant p (kg/h)
	t	Type of central treatment	DI	Diameter of pipe segment (m)
			DC	Calculated diameter of pipe segment (m)
	Sets:		FC	Total Freshwater Costs (\$/y)
	Ν	Set of nth level nodes n (must be defined for every	Flip	External freshwater mass flowrate of type I required
		merged connection)	1015	in sink i, plant p (kg/h)
	Р	Set of Plants/Processes in Industrial City	Min in'	Mass flowrate from source i, plant p to sink i plant
	R	Set of Decentralized Treatment Interceptors r	ibîb	n'(kg/h)
	SUn	Set of Water Sources in Plant p	PCM	Total Pining Costs associated with source-sink
	SNp	Set of Water Sinks in Plant p	I Civi	merged connectivity(\$)
	S	Set of Central Treatment Intercentors		Total Diping Costs associated with source to
	T	Set of Central Treatment Interceptors	rcbi	decontrolized treatment and de controlized
	X	Set of first level nodes a (must be defined for every		treatment to sink marged connectivity (f)
	Λ	merged connection)	DCCT	Total Diving Costs associated with source to
	v	Set of second level nodes b (must be defined for	PCCI	Total Piping Costs associated with source-to-
	1	every merged connection)		centralized treatment, and centralized treatment-
	7	Sot of third level podes c (must be defined for every		to-sink merged connectivity (\$)
	L	merged connection)	PCD	Total Piping Costs associated with decentral-
		merged connection)		ized treatment-to-waste, centralized treatment-to-
	Daramata	2		waste, and source-to-waste merged connectivity (\$)
	runnete	is.	PCF	Iotal Piping Costs associated with freshwater-to-
	<i>u</i>	Coefficient associated with piping cost calculations		sink merged connectivity (\$)
	D	Power coefficient associated with piping cost calcu-	T _{ip,rp}	Mass flowrate from source i, plant p to interceptor r
	CINV			plant p (kg/h)
	Crp	Decentralized Treatment r within Plant p Unit Cost	T _{ip,st}	Mass flowrate from source i, plant p to interceptor s
	CINV			of type t (kg/h)
	CREM	Central Treatment Type t Unit Cost (\$)	T _{rp,jp}	Mass flowrate from interceptor r plant p to sink j,
	Crp	Decentralized Treatment r within Plant p mass		plant p (kg/h)
	PEM	removed Cost (\$/kg)	T _{st,jp}	Mass flowrate from interceptor s of type to sink j,
	CREW	Central Treatment Type t mass removed Cost (\$/kg)		plant p (kg/h)
	CWASIE	Cost of Wastewater Discharge (\$/kg)	TDC	Total Central Treatment Costs (\$/y)
	CIKESH	Cost of Freshwater of type I (\$/kg)	TCC	Total De-central Treatment Costs (\$/y)
	⊿DI	Pipe diameter difference (m)	WC	Total Wastewater Discharge Costs (\$)
	G _{jp}	Flowrate required in sink j, plant p (t/h)	$x_{c.rp}^{in}$	Inlet concentration of contaminant c into intercep-
	Hy	Operating hours per year (h/yr)		tor r, plant p (ppm)
	K _F	Treatment Annualized Factor (yr ⁻¹)	x _c rp	Outlet concentration of contaminant c into intercep-
	L	Length of pipe segment (m)	-,- F	tor r, plant p (ppm)
	RR _{c,rp}	Removal Ratio of pollutant c in treatment intercep-	xREM	Total mass removed of contaminant c in interceptor
		tor r, plant p	C,SL	r, plant p (ppm)
	RR _{c,st}	Removal Ratio of pollutant c in central treatment	xin	Inlet concentration of contaminant c into central
		interceptor s of type t	C,SL	interceptor s of type t (ppm)
	$W_{\rm in}$	Flowrate available in source i, plant $p(t/h)$	xout	Outlet concentration of contaminant c into central
	x ^{Source}	Pollutant c composition in source i, plant p (ppm)	··c,st	interceptor s of type t (ppm)
	c,ıp √FRESH	Pollutant c composition in External Freshwater of	x REM	Total mass removed contaminant c in central inter-
	^c,l	tune l(nem)	^c,st	centor s of type t (ppm)
	Max	type <i>i</i> (ppm)	, Discharge	Total discharge concentration of contaminant a
	XC	waximum permissible discharge concentration of		Pinamy variable accorded with intercenter a utili-
	ЕРЕСЦ	pollutant c (ppm)	yst yst	binary variable associated with interceptor's utiliz-
	$\chi_{c,l}^{rresn}$	Pollutant c composition in External Freshwater of	_in	Ing type t central treatment
	mi-	type <i>l</i> (ppm)	c,jp	Politicant C Composition in sink J, plant p (ppm)
	$z_{cj,p}^{min}$	Minimum permissible pollutant c composition in		
		sink j, plant p (ppm)		
			1	

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