



Optimized integration of renewable energy technologies into Alberta's oil sands industry

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ABSTRACT

An energy optimization model for the integration of renewable technologies into the energy infrastructure of the oil sands industry is presented. The proposed model determines the optimal configuration of oil producers and the energy infrastructure required to meet their energy demands. The model is geared toward the minimization of cost subject to carbon dioxide emission constraints. A mixed integer non-linear optimization model is developed that simultaneously optimizes capacity expansion and new investment decisions of conventional and renewable energy technologies. To illustrate its applicability, the proposed model was applied to a case study using data reported in the literature for various years of oil sands operations. A rolling horizon approach was implemented to determine the effect of investment decisions of previous operational years on the selection of new investment options. Results were compared with and without the incorporation of renewable energy technologies. The results obtained indicate that the proposed model is a practical tool that can be employed to evaluate and plan oil sands and energy producers for future scenarios. Moreover, the results show that renewable energy technologies have significant potential in reducing reliance on fossil-fuel based technologies and their associated CO₂ emissions. The emission constraints set for the operational year 2025 can only be achieved by the incorporation of renewables in the energy production mix.

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1. Introduction

1.1. Alberta's oil sands industry—current and future challenges

The majority of oil reserves in Canada are located in the Western Canada Sedimentary Basin, of which the oil sands in Alberta comprise the majority of reserves. The majority of Canadian oil sands are located in Alberta in three major deposits, which are Peace River, Cold Lake and Athabasca. The largest and most heavily developed among them is the Athabasca oil sands deposit, which includes deposits that can be surface mined and extensive in situ reserves. The Canadian Oil Sands is the third largest crude oil proven reserves in the world, which amount to proven reserves of about 168 billion barrels constituting approximately 97% of Canada's total oil reserves (Woynilowicz, 2005; National Energy Board, 2006).

The oil sands are a mixture of bitumen, sand, clay and water. Bitumen is a heavy viscous crude that requires significant amounts of energy for production, upgrading and transportation. Extracted bitumen can be diluted by solvents (e.g., naphtha) to reduce

its viscosity for further transportation to be sold as commercial crude bitumen or to be upgraded to higher quality synthetic crude oil (SCO). Bitumen upgrading operations can be integrated with mining or steam assisted gravity drainage (SAGD) extraction operations, and they typically consist of hydrocracking or thermoc-racking processes to break the heavy hydrocarbon molecules into lighter ones. Mining extraction is typically employed for bitumen deposits located at depths up to 75 m. The oil sands are mined by electric and hydraulic shovels, which are then transported by trucks to separation units in which hot water and solvents are used to extract the bitumen from the oil sands mixture. In-situ methods are used for deep bitumen deposits that are located more than 75 m below the earth's surface, and they have been employed to recover deposits at depths within the range of 350–600 m below the surface. In-situ methods rely on the use of steam, solvents or thermal energy to extract the bitumen from the oil sands in order to enhance its flow, which is then pumped to the surface. The two prominent production technologies are mining and in-situ, the latter being more economically and environmentally preferable and will account to approximately two-thirds of future oil sands production capacity. Mining extraction is currently the dominant method used for bitumen extraction (National Energy Board, 2006; Oil Sands Discovery Centre, 2014; Kubik, 2013).

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Nomenclatures

Indices

<i>b</i>	Type of steam and hot water boilers
<i>e</i>	Type of existing energy production technology
<i>h</i>	Type of hydrogen production technology
<i>i</i>	Type of energy production technology
<i>m</i>	Type of integrated mining/upgrading SCO production route
<i>o</i>	Type of SCO production route
<i>p</i>	Type of power production technology
<i>s</i>	Type of integrated SAGD/upgrading SCO production route

Sets

<i>B</i>	Set of boilers
<i>E</i>	Set of existing energy production units (i.e., power, hydrogen, steam and hot water producers)
<i>H</i>	Set of hydrogen production plants
<i>I</i>	Set of all energy production technologies
<i>M</i>	Set of integrated mining/upgrading SCO production routes
<i>O</i>	Set of all SCO production routes
<i>P</i>	Set of power production plants
<i>S</i>	Set of integrated SAGD/upgrading SCO production routes

Parameters

AWP	Annual energy yield of VESTAS wind turbine (kWh)
CCB _{<i>b</i>}	Amortized capital cost of boiler type <i>b</i> (\$/year)
CCGEO	Amortized capital cost of geothermal plants (\$/year)
CCH _{<i>h</i>}	Amortized capital cost of hydrogen plant type <i>h</i> (\$/year)
CCHE	Amortized capital cost of electrolyzer (\$/year)
CCP _{<i>p</i>}	Amortized capital cost of power plant type <i>p</i> (\$/year)
CO ₂ E	Maximum allowable level of CO ₂ emissions (ton CO ₂ /h)
<i>d_m</i>	Distance between mining location and extraction plant (m)
DR	Fraction of diluent
<i>dT_m</i>	Distance between extraction plant and tailing ponds (m)
ECB	Electricity requirement for the production of commercial crude bitumen (kWh/ton)
ECC _{<i>i</i>}	Electricity requirement for compressing CO ₂ for transport (kWh/ton/km)
ECR	Power requirement for centrifugation (kWh/m ³)
ED _{<i>o</i>}	Electricity requirement for delayed cokers (kWh/ton)
EER	Electrolyzer energy requirement (kWh/Nm ³)
EL _{<i>o</i>}	Electricity requirement for LC-finiers (kWh/ton)
EPVF	Annuity factor for existing technologies
ESMR	Electricity requirement of steam methane reforming plants (kW/ton H ₂)
ΔHSS	Change in enthalpy of SAGD steam (MJ/ton)
ΔHPS	Change in enthalpy of process steam (MJ/ton)
ΔHHW	Change in enthalpy of hot water (MJ/ton)
HHG	Hydrogen requirement for hydrotreatment of HGO (ton H ₂ /ton LGO)
HH _{<i>h</i>} ^{max}	Maximum production capacity of hydrogen plant <i>h</i> (ton/h)
HHV _{<i>b</i>}	High heating value of fuel used in boiler technology <i>b</i> i.e., natural gas, biomass etc. (MJ/ton)
HHV _{<i>h</i>}	High heating value of fuel used in hydrogen technology <i>h</i> i.e., coal, natural gas, etc. (MJ/ton)

HHV _{<i>p</i>}	High heating value of fuel used in power technology <i>p</i> i.e., coal, natural gas, etc. (MJ/ton)
HLG	Hydrogen requirement for hydrotreatment of LGO (ton H ₂ /ton LGO)
HN	Hydrogen requirement for the hydrotreatment of naphtha (ton H ₂ /ton naphtha)
HNG	Heating value of natural gas (GJ/Nm ³)
HP _{<i>h</i>} ^{co_gen}	Power co-produced or consumed by hydrogen plants (kW/ton H ₂)
HRP _{<i>p</i>}	Heat rate of power plant <i>p</i> (MJ/kWh)
HRH _{<i>h</i>}	Heating rate of hydrogen production technology <i>h</i> (MJ/ton H ₂)
HRU _{<i>o</i>}	Hydrogen requirement for hydrocracking in low and high conversion LC-finiers (ton H ₂ /ton feed)
HRGEO ^{max}	Maximum heat rate provided by a geothermal plant (MJ/h)
FR _{<i>o</i>}	Natural gas requirement for LC-finiers and delayed cokers (GJ/ton VTB)
<i>L</i>	Length of CO ₂ pipeline (km)
MDC	Diesel consumption for mining extraction (L diesel/bbl bitumen)
<i>η_b</i>	Efficiency of boiler type <i>b</i>
OMB _{<i>b</i>}	Operating and maintenance cost of boiler type <i>b</i> (\$/year)
OMGEO	Operating and maintenance cost of geothermal plants (\$/year)
OMH _{<i>h</i>}	Operating and maintenance cost of hydrogen plant <i>h</i> (\$/year)
OMHE	Operating and maintenance cost of electrolyzer (\$/year)
OMP _{<i>p</i>}	Operating and maintenance cost of power plant <i>p</i> (\$/year)
PFB _{<i>b</i>}	Unit cost of fuel utilized by SAGD boiler <i>b</i> (\$/GJ or \$/ton)
PF _{<i>m</i>}	Pumping factor for hydrotransport (kWh/ton/m)
PFH _{<i>h</i>}	Unit cost of fuel utilized by hydrogen plant <i>h</i> (\$/GJ or \$/ton)
PPF _{<i>p</i>}	Unit cost of fuel utilized by power plant <i>p</i> (\$/GJ or \$/ton)
PFT _{<i>m</i>}	Pumping factor for transport of tailings (kWh/ton/m)
PD	Unit cost of diesel (\$/L)
PNG	Unit cost of natural gas utilized by natural gas boilers (\$/GJ)
pp _{<i>p</i>} ^{max}	Maximum power production capacity of plant <i>p</i> (kWh)
PVF	Annuity factor for newly established technologies
EPVF _{<i>e</i>}	Annuity factor for existing technologies
S _{<i>b</i>} ^{max}	Maximum production capacity of boiler type <i>b</i> (ton/h)
SSC	Unit sequestration cost (\$/ton CO ₂)
SC _{<i>m</i>}	Steam requirement for conditioning stage (ton steam/ton feed)
SF	Steam requirement for bitumen extraction (ton steam/ton froth)
SOR	Steam to oil ratio (ton of steam/ton of bitumen)
SRD	Steam requirement for the diluent recovery unit (ton steam/ton feed)
SRF	Steam requirement for the fluid coker (ton steam/ton feed)

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