ARTICLE IN PRESS

Data in Brief 🛛 (■■■) ■■==■■



Please cite this article as: I. Lee, et al., Data on conceptual design of cryogenic energy storage system combined with liquefied natural gas regasification process, Data in Brief (2017), http://dx. doi.org/10.1016/j.dib.2017.09.015

2

61 62

63 64

65

66

67

68

69 70 71

72 73

74

75

76 77 78

79 80

81 82

83

84

85

86

87

88

89 90

91 92

93

94

95

96

97 98

ARTICLE IN PRESS

I. Lee et al. / Data in Brief ■ (■■■) ■■■-■■■

55	Experimental	Feasibility check, sensitivity analysis, performance evaluation
56	features	
57	Data source	Department of Chemical and Biomolecular Engineering, Yonsei University,
58	location	Republic of Korea
59	Data accessibility	Data with this article
60		

Value of the data

- The increase of the air flow rate causes increase of the power generation.
- The increase of the air flow rate causes decrease of the minimum temperature difference of the heat exchanger.
- The pinch point can be shown not only at the inlet or outlet but also inside the heat exchanger when the phase changing occurs.

1. Data

In this data article, we share sensitivity analysis data of the cryogenic energy storage system combined with liquefied natural gas (LNG) regasification process. In this data, the case study simulation results by air flow rate and the heat exchanging composite curves are illustrated.

2. Experimental design, materials and methods

2.1. Sensitivity analysis of the air flow rate

The air is used as the working fluid in this integrated energy storage system. To find the optimal flow rate of the air, the simulation case study is performed by the air flow rate for the sensitivity analysis. The flow rate of the LNG is fixed as 1.00 kg/s for every case. We set five cases of the air flow rate as follows: Case 1 is 0.40 kg/s, Case 2 is 0.45 kg/s, Case 3 is 0.50 kg/s, Case 4 is 0.55 kg/s and Case 5 is 0.60 kg/s of air flow rate. The specific work output of the cryogenic energy release system by the air flow rate is shown in Table 1. The stream notations are shown in Fig. 2 in Ref. [1].

The simulation result shows that the total work output is almost linear to the air flow rate.

2.2. Feasibility analysis for the heat exchangers

The detailed heat exchanging simulations are performed to check the feasibility and the results are shown in Table 2. The pinch temperature is set as 3 °C for every heat exchanger as the constraint. Therefore, the minimum temperature difference of the heat exchanger have to be larger than 3 °C. Finding pinch point is an important part in the procedure of the heat exchanging feasibility check. The hot stream is air and the cold stream is LNG for all heat exchangers. The cold LNG is vaporized via

99 Table 1 Specific work output by the air flow rate (kJ/kg-LNG). 100

Specific work output	Case 1	Case 2	Case 3	Case 4	Case 5
Air expander 1	30.23	34.01	37.79	41.57	45.35
Air expander 2	31.98	35.97	39.97	43.97	47.97
Air expander 3	33.27	37.42	41.58	45.74	49.90
Air expander 4	33.26	37.42	41.58	45.74	49.89
Total work output	128.74	144.82	160.92	177.02	193.11

108

Please cite this article as: I. Lee, et al., Data on conceptual design of cryogenic energy storage system combined with liquefied natural gas regasification process, Data in Brief (2017), http://dx. doi.org/10.1016/j.dib.2017.09.015

Download English Version:

https://daneshyari.com/en/article/6597360

Download Persian Version:

https://daneshyari.com/article/6597360

Daneshyari.com