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## Parametric study of recuperative VOC oxidation reactor with porous media

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#### Abstract

Numerical study of volatile organic compounds (VOC) oxidation reactor consisting of two coaxial tubes, filled with inert porous media is performed. Influence of incoming gas flux, adiabatic temperature of gas combustion, reaction rate constant, diameter of porous body particles, reactor size and heat losses on maximal temperature of reactor, recuperation efficiency, combustion front position is investigated. It is shown that maximum temperature and recuperation efficiency of reactor has extremum in the field of incoming gas flow rate and porous body particle size parameters (for simulated configuration of reactor maximum corresponds to  $U_G \sim 2$  m/s and  $d_0 \sim 6$  mm). Numerical simulation shows non-monotonous character of maximal temperature and recuperation efficiency dependence from side heat losses of reactor. The obtained results can be used for construction optimization of practical VOC oxidation reactors. © 2006 Elsevier Ltd. All rights reserved.

Keywords: Filtration combustion (FC); Heat recuperation; Heat regeneration; Porous media; Volatile organic compounds (VOC); Oxidizer

### 1. Introduction

Air purification from Volatile Organic Compounds (VOC) remains actual problem facing chemical, nutrition, mining and other industries [1,2]. The widely spread VOCs - phenol, formaldehyde, acetone, benzole and other may be contained in ventilation gases of mines, paint shops, plastic extruder shops, in technological flue gases, etc. In many cases VOCs concentration is less than combustion lean limit concentration, but enough for self-sustained combustion in inert porous media. Combustion in inert porous media or filtration combustion (FC) provides effective heat recirculation and consequently low energy costs of the process [3-6]. In the case of sufficiently high concentration of VOCs ( $\sim 1 \text{ mass}\%$ ) the combustion process may be sustained due to the heat content of the pollutants and does not demand any additional fuels. In experiments by Takeno and Sato [7] in steady reactor with complicated heat recuperation methane-air mixture combustion was realized at equivalence ratio as low as  $\Phi = 0.026$  (which is 20 times lower than lean limit combustion concentration for methane-air mixture). In the work [3,4] the regenerative porous media reactor was utilized for lean methane combustion. The stable combustion was achieved at equivalence ratio  $\Phi = 0.15$ .

One of the principal features of FC is internal heat recirculation in the combustion wave, due to heat exchange between gas and solid in the preheat zone of the combustion wave. Practical systems designed for the low calorific fuels combustion utilize schemes of external heat recirculation in addition to the internal one. These are heat recuperation by means of counter-flow heat exchange between incoming and exhaust gases and heat regeneration due to periodical reverse of flow direction. Both schemes are investigated in laboratory installations [3,4,8–10] and found their application in industrial VOCs oxidizers, produced by Thermatrix [10], ReEco-Stroem [11] and other companies. Physical aspects of the FC in inert porous media are discussed in [4,7,12,13] and other papers.

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#### Nomenclature

$a, a_0$	Arrhenius preexponential factor $(m^3/(mol s))$	$T_0$	initial temperature of the system (K)
$C_{\rm r}$	efficiency of recuperation (dimensionless)	$U_{\mathbf{G}}$	superficial gas velocity (m/s)
$C_1$	dimensionless losses from sidewall of reactor	u V	gas velocity vector (m/s)
$c_p$	heat capacity of gas $(J/(Kg K))$	$X_i$	molar fraction of <i>i</i> th component
$c_{\rm s}$	heat capacity of porous carcass $(J/(kg K))$	$Y_i$	mass fraction of <i>i</i> th component
D	gas diffusivity tensor (m <sup>2</sup> /s)	$z_1, z_2$	internal tube or reactor length (m)
<b>D</b> <sub>d</sub>	dispersion diffusivity tensor (m <sup>2</sup> /s)	$z_{f}$	combustion front position (m)
$D_{\rm p}, D_{\rm t}$	longitudinal and transverse component of dis-	~ -	
_	persion diffusivity tensor	Greek .	symbols
$D_{\rm g}$	gas diffusivity coefficient, approximated by	α	heat exchange coefficient $(W/(m^2 K))$
	nitrogen properties (m <sup>2</sup> /s)	$\alpha_{\rm vol}$	volumetric heat exchange coefficient $(W/(m^3 K))$
$d_0$	diameter of porous carcass particle (m)	3	emissivity of the porous carcass
$d_1$	internal tube diameter (m)	ho	density (kg/m <sup>3</sup> )
$d_2$	reactor diameter (m)	$\dot{ ho}_i$	mass generation rate of <i>i</i> th component due
G	gas mass flow rate (kg/s)		chemical reactions (kg/s)
$h_i$	mass enthalpy of <i>i</i> th chemical component	Λ	heat conductivity tensor (W/(m K))
$\Delta h$	gas mixture heat of combustion (J/kg)	λ	conductivity or effective conductivity of porous
Ι	unit matrix		carcass (W/(m K))
k	reaction rate $(m^3/(mol s))$	$\mu$	gas viscosity coefficient, approximated by nitro-
$k_0, k_1$	filtration permeabilities		gen properties (Pa s)
M	average molecular weight of gas (kg/mol)	$\sigma$	Stefan–Boltzmann constant $(5.67 \times 10^{-8} \text{ W/})$
т	porosity		$(m^2 K^4))$
р	pressure (Pa)	τ	unit vector with components $\tau_z$ , $\tau_r$
$p_0$	outlet pressure (Pa)	$\Phi$	fuel/air equivalence ratio
$Q_{ m r}$	heat flux via internal tube wall (W)	$\Omega$	surface of internal tube or reactor sidewall
$Q_1$	heat losses from side wall of reactor (W)		
R	absolute gas constant	Subscri	ipts
r	radius (m)	1	relates to internal tube
S	internal tube cross section (m <sup>2</sup> )	2	relates to reactor sidewall
Т	temperature (K)	g	gas
$T_{\rm ad}$	adiabatic temperature of combustion, $\Delta T_{ad} =$	i	<i>i</i> th component of gas
	$T_{\mathrm{ad}} - T_0 \left(\mathrm{K}\right)$	S	solid

Though such type of reactors are under investigation and have a practical utilization, there is lack of obtainable publications concerned with detailed parametric study of these devices. The combined regenerator-recuperator scheme of VOC oxidizer was investigated in [14] numerically. Important parameters – maximal temperature of reactor,  $NO_x$ emission, effective ranges of gas flow rate and VOC concentration are compared for different types of reactor. It was shown that recuperative-regenerative scheme let one expand the range of operational flow rate and VOC concentration compared to stationary recuperative reactor.

Parametric study of filtration combustion reactor with electro heating elements was presented in [15]. The influence of gas flow rate, electrical heating elements position and power, and thermal isolation on maximal temperature in the system, unburned VOC concentration was investigated.

In this article numerical study of the steady-state recuperative (coaxial tubes type) reactor is performed. The influence of incoming gas flow rate, heat losses via side wall and other parameters on temperature and VOC burning out is under investigation. Reactor recuperation efficiency and combustion front position were under consideration too. The chemical kinetics of the VOC oxidation is modeled by one-step Brutto model for methane combustion.

#### 2. Problem statement

The system under investigation consists of two coaxial tubes, filled with ceramic particles – packed bed (Fig. 1). The reactor walls width is assumed to be zero in the model. The heat losses via side walls may be varied according to Newtonian law (7). At initial time instant porous body (Fig. 1, (4)) was preheated in order to ignite the gas mixture. VOC containing gas (Fig. 1, (1)) enters through central tube, heats up due to the heat exchange with porous body (Fig. 1, (4)) turns-around and goes out through the gap between internal tube and reactor body (Fig. 1, (2)). At certain temperature the VOC oxidation starts and xcombustion products heat up porous media and via it the incoming fresh gas mixture.

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