

Available online at www.sciencedirect.com



International Journal of HEAT and MASS TRANSFER

International Journal of Heat and Mass Transfer 48 (2005) 2351-2359

www.elsevier.com/locate/ijhmt

Evaporating heat transfer and pressure drop of hydrocarbon refrigerants in 9.52 and 12.70 mm smooth tube

H.S. Lee^a, J.I. Yoon^{b,*}, J.D. Kim^c, Pradeep Bansal^d

^a Department of Refrigeration and Air-Conditioning Engineering, College of Engineering, Pukyong National University, San 100,

Yongdang-dong, Nam-gu, Pusan 608-739, Korea

^b College of Engineering, School of Mechanical Engineering, Pukyong National University, San 100, Yongdang-dong,

Nam-gu, Pusan 608-739, Korea

^c Department of Refrigeration and Air-Conditioning, Tongmyong College, Pusan 608-740, Korea ^d Department of Mechanical Engineering, The University of Auckland, Private bag 92019 Auckland, New Zealand

> Received 12 July 2004; received in revised form 25 January 2005 Available online 17 March 2005

Abstract

Experimental results of heat transfer characteristic and pressure gradients of hydrocarbon refrigerants R-290, R-600a, R-1270 and HCFC refrigerant R-22 during evaporating inside horizontal double pipe heat exchangers are presented. The test sections have one tube diameter of 12.70 mm with 0.86 mm wall thickness, another tube diameter of 9.52 mm with 0.76 mm wall thickness was used for this study. The local evaporating heat transfer coefficients of hydrocarbon refrigerants were higher than those of R-22. The average evaporating heat transfer coefficient increased as the mass flux increased. It is showed the higher values in hydrocarbon refrigerants than R-22. Comparing the heat transfer coefficient of experimental results with that of other correlations, the obtained results from the experiments had coincided with most of the Kandlikar's correlation. Hydrocarbon refrigerants have higher pressure drop than R-22 in 12.7 mm and 9.52 mm. This results form the study can be used in the case of designing heat transfer exchangers using hydrocarbons as the refrigerant for the air-conditioning systems. © 2005 Elsevier Ltd. All rights reserved.

Keywords: Hydrocarbon refrigerant; Evaporation; Heat transfer coefficient; Pressure drop; Natural refrigerant

1. Introduction

Due to the environmental problems by CFCs and HCFCs, the development of new alternative refrigerants with the high efficient machine which can reduce energy consumption has been becoming an urgent issue [1,2].

^{*} Corresponding author. Tel.: +82 51 620 1506; fax: +82 51 620 1500.

E-mail address: yoonji@pknu.ac.kr (J.I. Yoon).

HFCs or non-azeotropic refrigerant mixtures [3] has been being regarded as alternative refrigerants. However, HFC's can make acids and toxic substances when they are resolved in a compound into their forming elements by sunlight [4], and though, they have zero ODP (ozone depletion potential), but they have high GWP (global warming potential). Besides of that fact, it is hard to treat non-azeotropic refrigerant mixtures efficiently and is difficult to reproduce the primary constant composition due to its variation caused by leakage for repairing. So, new alternative refrigerants having no

^{0017-9310/\$ -} see front matter @ 2005 Elsevier Ltd. All rights reserved. doi:10.1016/j.ijheatmasstransfer.2005.01.012

Nomencl	ature
---------	-------

BO	boiling number, q/Gi_{lg}	Subscri	inte	
	specific heat at constant pressure (kJ/kg K)	avg	average	
C_p CO	convection number, $((1-x)/x)^{0.8} (\rho_v/\rho_1)^{0.5}$	CBD	convective boiling dominant	
d	diameter (m) $((1 - x)/x) = (p_v/p_1)$	e	evaporator	
$F_{\rm fl}$	fluid dependent parameter		equivalent	
$\frac{\Gamma_{\mathrm{fl}}}{G}$	mass velocity (kg/m ² s)	eq :	inner	
b h	heat transfer coefficient (kW/m ² K)	1 	inlet	
n i		in 1		
	enthalpy (kJ/kg)	l loc	liquid local	
$\frac{l_{ m lg}}{k}$	latent heat of vaporization (J/kg)			
	thermal conductivity (kW/m K)	NBD	nucleate boiling dominant	
т	mass flow rate (kg/h)	0	outer	
п	number of local tube	out	outlet	
q	heat flux (kW/m ²)	r	refrigerant	
Q	heat capacity (kW)	tp	two phase	
Re	Reynold number, $\rho u D/\mu$	V	vapor	
S	suppression factor	W	source water	
Т	temperature (K)			
x	quality			
Greek symbols				
Δ	difference			
μ	dynamic viscosity (Pa s)			
ho	density (kg/m ³)			

poisonous characteristics, no flammability and should be similar to conventional refrigerant in terms of thermodynamic property are required.

Under these circumstances, additional and active studies regarding the so-called "natural refrigerants" have been under way. Especially HC's refrigerants are examined positively as an alternative refrigerant for (H)CFC because it is easily available and its GWP and ODP are almost close to zero. But, the developed countries like US and Japan have not adapted them except for Europe due to flammability of HC's. However, according to James [5], in case of the household refrigerators, the possibility of explosion by flammability can be negligible since the HC's charge quantity is about half of general CFC refrigerant's one. Besides, if some simple safety device (e.g. ventilation system or leakage detector) is installed, it can overcome that problem in the large size air-conditioning and refrigerating system. But, the researches for performance of the refrigeration and airconditioning systems using the HC's as a refrigerant are not enough, especially, the study on characteristics of evaporating heat transfer is the one of those.

Kandlikar [6] introduced a general correlation about fluid boiling in the vertical-horizontal tube. Kwon [7] experimented regarding the characteristics of evaporating heat transfer using R-290, R-410A and compared with those of R-22. According to his report, evaporating heat transfer coefficient of R-290 was higher than that of R-22 or R-410A, but the research on evaporating heat transfer of natural refrigerants is still ridiculously rare.

In this scenarios, the purpose of this paper is to obtain basic data for the purpose of designing the evaporator that uses HC's refrigerants and is to compare experimentally, the evaporating heat transfer characteristic and the pressure drop of R-1270 (propylene), R-290 (propane), R-600a (iso-butane) taking R-22 as base at the smooth tube.

2. Experimental apparatus and method

2.1. Experimental apparatus

Fig. 1 shows the schematic of the experimental apparatus including basic air-conditioning and refrigerating system consisted of compressor, condenser, expansion valve, evaporator and peripheral device. The system also consists of two main flow loops: a refrigerant loop and heat source water for evaporating or condensing loop. In the test section of the experiment, the evaporator is a double-tube type heat exchanger divided into three sections, which are inner tube, outer tube and annular section.

The heat exchanger (test section) is shown in Fig. 2. The inner diameter of the inner tube (copper) is 10.92 mm, 8 mm, and outer and inner diameters of the outer tube (copper) are 19.94 and 22.22 mm respectively. Download English Version:

https://daneshyari.com/en/article/663154

Download Persian Version:

https://daneshyari.com/article/663154

Daneshyari.com