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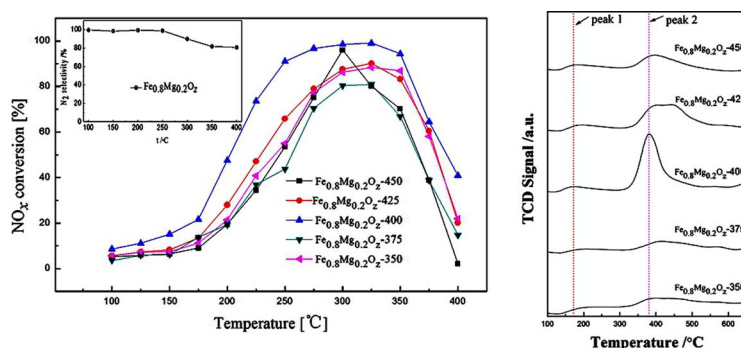
# Influence of calcination temperature on $\text{Fe}_{0.8}\text{Mg}_{0.2}\text{O}_x$ catalyst for selective catalytic reduction of $\text{NO}_x$ with $\text{NH}_3$

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## GRAPHICAL ABSTRACT

$\text{Fe}_{0.8}\text{Mg}_{0.2}\text{O}_x$  catalyst calcined at 400 °C showed the best catalytic performance and excellent  $\text{N}_2$  selectivity. More than 90%  $\text{NO}_x$  conversion could be achieved in a wide temperature range of 250–350 °C. Calcination temperature significantly affected the total amount of the surface acidity. The surface acidity (mainly Brønsted acid sites in  $\text{Fe}_{0.8}\text{Mg}_{0.2}\text{O}_x$ -400 catalyst) played an important role in SCR reaction.



## ARTICLE INFO

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## ABSTRACT

A series of  $\text{Fe}_{0.8}\text{Mg}_{0.2}\text{O}_x$  catalysts for selective catalytic reduction (SCR) of  $\text{NO}_x$  with  $\text{NH}_3$  were prepared via coprecipitation method with microwave thermal assistant at different calcination temperature. The influence of calcination temperature on the catalytic performance, microstructure properties, surface elements and acidity over  $\text{Fe}_{0.8}\text{Mg}_{0.2}\text{O}_x$ -T catalysts was investigated by various characterization methods.  $\text{Fe}_{0.8}\text{Mg}_{0.2}\text{O}_x$  catalyst calcined at 400 °C showed the highest  $\text{NO}_x$  conversion and excellent  $\text{N}_2$  selectivity. More than 90%  $\text{NO}_x$  conversion could be achieved in a wide temperature range of 250–350 °C.  $\text{Fe}_{0.8}\text{Mg}_{0.2}\text{O}_x$ -400 with large surface area and pore volume obtained a high purity  $\gamma\text{-Fe}_2\text{O}_3$  crystalline phase with the calcination temperature of 400 °C. Meanwhile, Magnesium had strong interaction with  $\gamma\text{-Fe}_2\text{O}_3$  and existed in either highly dispersed or amorphous phase. Surface oxygen concentration and acidity (mainly Brønsted acid sites in  $\text{Fe}_{0.8}\text{Mg}_{0.2}\text{O}_x$ -T catalysts) played an important role in SCR reaction. The results implied that the higher surface area, pore volume, strong interaction, superior surface acidity and redox ability contributed to the excellent SCR catalytic performance of  $\text{Fe}_{0.8}\text{Mg}_{0.2}\text{O}_x$  catalyst calcined at 400 °C.

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## 1. Introduction

Nitrogen oxides (NO<sub>x</sub>, mainly NO and NO<sub>2</sub>) are one of the most primary pollutants that have caused nitric acid rain, photochemical smog, ozonosphere hole, etc., and seriously impact on human health [1,2]. The removal of NO<sub>x</sub> has become an important environmental issue due to the severe air pollution and the more and more rigorous emission standards. NO<sub>x</sub> are mainly from the emission of fossil-fuel power station and automotive exhaust [3,4]. NH<sub>3</sub>-SCR [5] has been proved to be the most efficient mature technology with acceptable cost [6] reliably applied in coal-power station to limit the emission of NO<sub>x</sub> [7]. The selection of catalyst is vital for the operation of denitrification system. Although vanadium-titanium catalysts [8–11] with a temperature window of 300–400 °C [12] have been widely used as the common commercial catalysts in eliminating NO<sub>x</sub>, several inevitable disadvantages such as the toxicity of vanadium pentoxide, the low selectivity at high temperature and the high conversion of SO<sub>2</sub> to SO<sub>3</sub> with increasing vanadium loadings have restricted the further application of these catalysts [13,14]. Nowadays, the increasingly stringent regulations of NO<sub>x</sub> emission and vanadium-titanium as hazardous waste make iron-based catalysts comprehensively concerned by the researchers. It is of great significance to study on iron-based catalysts with advantages such as low manufacturing cost, wide material sources, favorable SCR activity and N<sub>2</sub> selectivity, etc. [15–17]. Recently, it is reported that iron-based catalysts, such as Ce-Fe/WMH [18], Mn-Fe/TiO<sub>2</sub> [19], WO<sub>3</sub>/Fe<sub>2</sub>O<sub>3</sub> [20], Fe/WO<sub>3</sub>-ZrO<sub>2</sub> [21], Fe-Ti [22,23], Fe/TiO<sub>2</sub> [24], Fe/Ce-Ti [25,26], Fe-Ce-W [27,28], etc., show excellent SCR activity and N<sub>2</sub> selectivity. In these researches, γ-Fe<sub>2</sub>O<sub>3</sub> exhibited potential low-temperature de-NO<sub>x</sub> SCR performance [29]. Maghemite (γ-Fe<sub>2</sub>O<sub>3</sub>) widely used for the production of catalysts [30] is reported to be in a metastable state with a lower activation energy than α-Fe<sub>2</sub>O<sub>3</sub>, which makes the Lewis acid sites on the surface easily react with H atoms in NH<sub>3</sub>. Casanova [31] found that SCR activity correlated directly with the Fe loading of the catalyst at medium and low temperature. Cao [32] reported that the increase of surface area and pore volume of the catalyst due to the addition of Fe and strengthening of the Brönsted and Lewis acid sites were responsible for the increase of SCR activity. Specifically, the presence of Fe could significantly improve the SO<sub>2</sub> resistance of the sorbent [33]. Schill [34] found that the presence of Fe in V/TiO<sub>2</sub> catalyst could increase the surface area and surface acid sites. Liu [35] studied on Co-Ce-Ti catalyst with the excellent low-temperature activity and broadened temperature window, which could be attributed to the improvement of the physico-chemical properties and acceleration of the reactions in L-H and E-R mechanisms. The characterization results by Zhu [36] manifested that Co-Fe/TiO<sub>2</sub> owned more adsorption capacity of the reactants and Cu-Fe/TiO<sub>2</sub> had better redox ability. Further researches proved that the calcination temperature had an important influence on the valence state of species, as well as the dispersion extent of active phase and the crystal phase structure of support [37]. The appropriate calcination temperature was important for the DeNO<sub>x</sub> activity of the catalysts [38]. The SCR activities in different temperature range over various catalysts were influenced by the calcination temperature in varying degree. CeO<sub>2</sub>-ZrO<sub>2</sub>-WO<sub>3</sub> [39] catalyst calcinated at 600 °C showed the best NO<sub>x</sub> conversion and excellent N<sub>2</sub> selectivity with a wide temperature window from 250 to 500 °C. Nearly 100% NO conversion of Sm-Mn-0.1 catalyst was obtained at 65–200 °C after calcinating at 450 °C [40]. Generally speaking, agglomeration caused by high calcination temperature would lead to the decrease in activity of the catalysts. Obvious decreases were observed for CeO<sub>2</sub>-ZrO<sub>2</sub>-WO<sub>3</sub> catalyst [39] calcinated above 600 °C and Sm-Mn-0.1 catalyst [40] calcinated at 450 °C. CeMoO<sub>x</sub> catalyst calcinated at 600 °C and 700 °C led to drops of NO<sub>x</sub> conversion [41]. But not all the activities were decreased with increasing calcination temperature. For example, high DeNO<sub>x</sub> activity to N<sub>2</sub> of Ag(2) catalyst was attained with a high calcination temperature [42]. Recently, research showed that Fe<sub>0.8</sub>Mg<sub>0.2</sub>O<sub>x</sub> catalyst exhibited potential in converting NO<sub>x</sub>

to N<sub>2</sub> with NH<sub>3</sub>, but there are few researches about the influence of calcination temperature on Fe<sub>0.8</sub>Mg<sub>0.2</sub>O<sub>x</sub> catalyst [43]. Therefore, the objective of this paper is to investigate the SCR activities of Fe<sub>0.8</sub>Mg<sub>0.2</sub>O<sub>x</sub> catalysts calcinated at different temperatures and reveal the effect of calcination temperature on the physical and chemical properties of the catalysts such as crystalline phase, BET surface area, pore diameter distribution, micro-morphology, chemical states of the elements and surface acidity etc. by XRD, N<sub>2</sub>-adsorption-desorption, SEM, EDS, XPS and NH<sub>3</sub>-TPD.

## 2. Experimental

### 2.1. Preparation of catalyst

The iron-magnesium mixed oxide catalysts were prepared via the co-precipitation method with microwave thermal treatment. FeSO<sub>4</sub>·7H<sub>2</sub>O and Mg(NO<sub>3</sub>)<sub>2</sub>·6H<sub>2</sub>O (analytically pure, provided by Tianjin Kermel Chemical Reagent Co., Ltd) were used as the precursors. 2 mol/L NH<sub>3</sub>·H<sub>2</sub>O solution was used as a precipitator. A certain amount of FeSO<sub>4</sub>·7H<sub>2</sub>O and Mg(NO<sub>3</sub>)<sub>2</sub>·6H<sub>2</sub>O were dissolved in deionized water and stirred for 1 h at room temperature to get a fully dissolved solution. The solution was slowly titrated into NH<sub>3</sub>·H<sub>2</sub>O solution under stirring until pH of the synthesis solution became 9–10. The precipitate was filtered and washed by deionized water until pH of filter liquor was about 7 to remove foreign ions. Then the solid product was impregnated with 1 mol/L Na<sub>2</sub>CO<sub>3</sub> solution and disposed by microwave thermal treatment. The intermediate was washed by deionized water and then dried at 105 °C, which was followed by calcination at 350–450 °C for 5 h in air atmosphere. The samples were crushed and sieved into 40–60 mesh (0.28–0.45 mm) for test. The catalysts prepared were denoted as Fe<sub>0.8</sub>Mg<sub>0.2</sub>O<sub>x</sub>-T, where 0.2 was the molar ratio of Mg/(Mg + Fe) in the catalysts, and T was the calcination temperature, which equaled to 350, 375, 400, 425, 450 °C, respectively.

### 2.2. Catalytic activity test

The catalytic performances of Fe<sub>0.8</sub>Mg<sub>0.2</sub>O<sub>x</sub>-T catalysts for selective catalytic reduction with ammonia were investigated in a quartz fixed-bed reactor at ambient pressure. 4 mL catalyst (about 2.5 g) was used and the reactant gas was simulated as 0.1 vol.% NO, 0.1 vol.% NH<sub>3</sub>, 3.5 vol.% O<sub>2</sub> and balanced N<sub>2</sub>. The total gas flow rate was 2 L/min and the gas hourly space velocity (GHSV) was about 30,000 h<sup>-1</sup>. The concentrations of NO and NO<sub>2</sub> in the inlet and outlet were analyzed by MGA5 Flue Gas Analyzer (York Instrument, MRU, Germany), and the concentration of N<sub>2</sub>O and NH<sub>3</sub> was monitored by Finland FTIR flue gas analyzer GASMET DX400. To avoid the impact of ammonia on the analyzer, phosphoric acid solution was installed before the analyzer to absorb the ammonia. Data were collected from 100 °C to 400 °C with an increment of 25 °C. NO<sub>x</sub> conversion and N<sub>2</sub> selectivity were calculated according to Eqs. (1) and (2) respectively.

$$\eta = \frac{C(\text{NO}_x)_{\text{in}} - C(\text{NO}_x)_{\text{out}}}{C(\text{NO}_x)_{\text{in}}} \times 100\% \quad (1)$$

$$S_{\text{N}_2} = \frac{C(\text{NO}_x)_{\text{in}} + C(\text{NH}_3)_{\text{in}} - 2C(\text{N}_2\text{O})_{\text{out}}}{C(\text{NO}_x)_{\text{in}} + C(\text{NH}_3)_{\text{in}}} \times 100\% \quad (2)$$

where  $C(\text{NO}_x)_{\text{in}}$  and  $C(\text{NO}_x)_{\text{out}}$  were denoted as the concentrations of NO<sub>x</sub> in the inlet and outlet of the reactor, while  $C(\text{NH}_3)_{\text{in}}$  and  $C(\text{N}_2\text{O})_{\text{out}}$  meant the concentrations of NH<sub>3</sub> in the inlet and N<sub>2</sub>O in the outlet, μL/L. NO<sub>x</sub> represented the sum of NO and NO<sub>2</sub>.

### 2.3. Catalyst characterization

The X-ray Diffraction was performed on a Rigaku D/max 2500 PC diffractometer with Cu Kα radiation, 50 kV × 150 mA. The data of the 2θ from 10° to 90° were collected at 4°/min with the step size 0.1°. N<sub>2</sub>-

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