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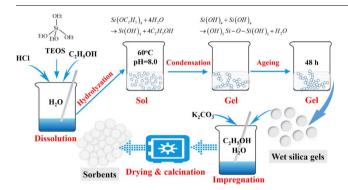
# Facile synthesis of silica aerogel supported K<sub>2</sub>CO<sub>3</sub> sorbents with enhanced CO<sub>2</sub> capture capacity for ultra-dilute flue gas treatment



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#### GRAPHICAL ABSTRACT



## ARTICLE INFO

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#### ABSTRACT

Silica aerogel supported  $K_2CO_3$  sorbents with different  $K_2CO_3$  loadings were synthesized by sol-gel and wet impregnation processes. The sorbents were characterized by  $N_2$  adsorption-desorption, X-ray diffraction (XRD), and field emission scanning electron microscopy (FESEM) techniques.  $CO_2$  capture performances of the sorbents were tested in a simulated ultra-dilute flue gas stream of  $1.0\%CO_2$  and  $2.0\%H_2O$  at 20 °C, using a fixed-bed reactor coupled with an online infrared gas analyzer. Sorbent regeneration performances of the samples were evaluated in a pure  $N_2$  atmosphere at 200 °C with a heating rate of 10 °C/min.  $CO_2$  capture capacity and  $K_2CO_3$  utilization efficiency increased first and then decreased with the increase in  $K_2CO_3$  loading. The desired sorbent with 20 wt%  $K_2CO_3$  was screened for investigating the effects of acid impurities. The presence of 500 ppm  $SO_2$  and 500 ppm NO in the simulated flue gas stream was found to adversely affect the  $CO_2$  capture, sorbent regeneration and multiple cyclic performances. Detailed mechanisms of the irreversible sorbent deactivation process were discussed.  $SO_2$  could be chemically absorbed by  $K_2CO_3$  under a moist condition to form byproduct of  $K_2SO_3H_2O$ , and the byproduct was stable and would be accumulated in the sorbent during the repeated cycles. This further attenuated the physical properties and  $K_2CO_3$  utilization efficiency of the sorbent. These results would lay a solid foundation for further application of the sorbent in ultra-dilute flue gas treatment.

#### 1. Introduction

Massive CO<sub>2</sub> emitting from fuel combustion process is considered as

the major contributor to global warming and climate change. Post-combustion CO<sub>2</sub> capture, oxy-fuel combustion technology, and the integrated gasification combined cycle and carbon capture and storage

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Table 1
A summary of CO<sub>2</sub> capture capacities of several silica aerogel supported sorbents reported in literatures.

Sorbents	Raw materials	Synthesis method	Testing conditions	CO <sub>2</sub> capture capacity (mmol CO <sub>2</sub> /g sorbent)	Refs.
A-SCD-acetone <sup>a</sup> A-SCD-ethanol A-SCD-methanol A-SCD- isopropanol	APTES, TEOS, EtOH, H <sub>2</sub> O, acetone, ethanol, methanol, isopropanol	One-step sol-gel process and SCD <sup>b</sup>	Fixed-bed reactor, 25–75 °C, 1%CO $_2$ + 1% H $_2$ O, 300 mL/min	5.55 4.46 3.96 4.24	[18]
AH-RFSA <sup>c</sup>	Resorcinol, formaldehyde APTES, $H_2O$	Hydrothermal sol-gel process	Fixed-bed reactor, 30–50 °C, $1\%CO_2$ (+1% $H_2O$ ), $300 \text{ mL/min}$	3.57 (4.43)	[19]
AHSA d	APTES, TEOS, EtOH, H <sub>2</sub> O	One-step sol-gel process and SCD	Fixed-bed reactor, 50 °C, 1%CO <sub>2</sub> , 300–700 mL/min	2.42-3.04	[20]
AMSA <sup>e</sup>	APTES, TEOS, EtOH, HCl, $\rm H_2O$	One-step sol-gel process and SCD	Quartz tubular reactor, 25–50 °C, $10\%CO_2$ (+ $10\%H_2O$ )	1.19–1.95 (3.81–6.97)	[21]
M-APTMS <sup>f</sup> T-APTMS <sup>g</sup>	TMOS, EtOH, HCl, $\rm H_2O$	Two-step hydrolysis-condensation process	Adsorption column, 20 °C, 0.25%CO <sub>2</sub> + 30% RH, 0–2 L/min	1.40 1.62	[22]
P-30-85 <sup>h</sup> W-30-80 <sup>i</sup>	TEPA, methanol, n-hexane, NaIO <sub>4</sub> , RuO <sub>2</sub> :2H <sub>2</sub> O, PA <sup>j</sup>	Solvent evaporative precipitation, wet impregnation	Electro-microbalance, 75 °C, 100%CO <sub>2</sub> , 100 mL/min	1.6-6.1 0.9-5.8	[23]
SA-I-40-90 k SA-O-50-85 l	TEPA, PA	Wet impregnation	Electro-microbalance, 75 °C, 100%CO <sub>2</sub> , 100 mL/min	2.3-6.1 1.3-3.5	[24]
$SiO_2$ $SiO_2$ -5%PEI $SiO_2$ -15%PEI $SiO_2$ -2%APTMS	Sodium silicate solution, acetic acid, TEOS, APTMS, EtOH, PEI	Hydrolyzation and polycondensation, wet impregnation	TGA, 50 °C, 100%CO <sub>2</sub> , 50 mL/min	0.21 0.88 1.16 0.67	[25]
FS-DETA-0-40 <sup>m</sup> K <sub>2</sub> CO <sub>3</sub> /SG <sup>n</sup>	Silica gel, DETA, methanol Silica gel, K <sub>2</sub> CO <sub>3</sub> , H <sub>2</sub> O	Wet impregnation Wet impregnation	TGA, 25 °C, 100%CO <sub>2</sub> , 60 mL/min TGA, 60 °C, 15%CO <sub>2</sub> + 15%H <sub>2</sub> O, 500 mL/min (fluidized-bed reactor, 1.8 m <sup>3</sup> /h)	0.56-0.92 Carbonation conversion of 34.5% (18.8%)	[26] [11]
K <sub>2</sub> CO <sub>3</sub> /SG	Silica gel, K <sub>2</sub> CO <sub>3</sub> , H <sub>2</sub> O	Wet impregnation	Fixed-bed reactor, 20 °C, 0.5%CO <sub>2</sub> + 1·.8H <sub>2</sub> O, 0.05 m <sup>3</sup> /h	0.15	[27]
K <sub>2</sub> CO <sub>3</sub> /SG	Silica gel, K <sub>2</sub> CO <sub>3</sub> , ethanol	Wet impregnation	TGA, 20–60 °C, $1.0\%\text{CO}_2 + 2.0\%\text{H}_2\text{O}$ , 500 mL/min	0.53	[28]

<sup>&</sup>lt;sup>a</sup> A-SCD-acetone = amine hybrid silica aerogel synthesized using acetone for solvent exchange.

(IGCC) are regarded as potential strategies for  $\rm CO_2$  emission reduction [1–3]. Amongst these mitigation technologies, post-combustion  $\rm CO_2$  capture through chemical absorption shows particular promise for large-scale application [4–6].

Chemical absorption of  $\mathrm{CO}_2$  using dry regenerable potassium-based sorbents is suitable for fossil fuel sector with broad prospects, considering the advantages of high storage capacity, facile regeneration, low cost and energy consumption, and high availability [6–10]. Although considerable efforts have been spent on further improving the  $\mathrm{CO}_2$  capture capacities and global reaction rates of potassium-based sorbents, high cost of the supporting materials and sorbent deactivation in acid impurities could be the two major challenges to overcome before cosmically commercial applications [11–17].

To achieve a cost-effective  $CO_2$  capture process, low-cost silica aerogel materials with open pore structure, high porosity and high surface area have been extensively employed as excellent supports for synthesizing solid  $CO_2$  sorbents [18–29]. Table 1 summarizes the  $CO_2$  capture capacities of several silica aerogel supported amine or  $K_2CO_3$  sorbents. Amine functionalization has been widely accepted as a promising route to improve  $CO_2$  capture capacity of silica aerogel. It was found that  $CO_2$  uptakes of the investigated amine-modified silica aerogel sorbents were comparable to or even greater than some commercially available sorbents (higher than 2.0 mmol  $CO_2/g$  sorbent) [18–21,23,24]. Particularly, a novel amine-modified  $SiO_2$  aerogel

sorbent (AMSA) synthesized by sol-gel process with supercritical drying (SCD) technique possessed an extremely high CO2 storage capacity of 6.97 mmol CO<sub>2</sub>/g sorbent [21]. Reports concerning the modification of silica aerogel with K<sub>2</sub>CO<sub>3</sub> for enhanced CO<sub>2</sub> capture capacity are limited. Compared to amine-functionalized silica aerogel sorbents, K2CO3modified silica aerogel (K2CO3/SG) prepared by one-step wet impregnation method presented rather poor CO2 capture performances, as indicated by the low carbonation conversion (34.5% in TGA and 18.8% in fluidized-bed reactor) and CO2 uptake (0.15 mmol CO2/g sorbent) [11,27]. Microscopic structure blockage in silica aerogel support and non-uniform distribution of K<sub>2</sub>CO<sub>3</sub> thereon were observed during the one-step wet impregnation procedure using deionized water as solvent, and these were responsible for the weak CO<sub>2</sub> capture performances. Overall capture capacity could be enhanced to 0.53 mmol CO<sub>2</sub>/g sorbent, when ethanol was used as solvent in the one-step wet impregnation process [28]. Whereas, the K2CO3 utilization efficiencies of the K<sub>2</sub>CO<sub>3</sub>/SG sorbents prepared by the one-step wet impregnation method using deionized water and ethanol as solvents are only 5.5% and 35.6%, which are far from those reported for K<sub>2</sub>CO<sub>3</sub>/Al<sub>2</sub>O<sub>3</sub> sorbents (>90%) [14,15,30,31]. Hence, there is still room for improvement in CO2 capture capacity and K2CO3 utilization of the K2CO3-modified silica aerogel sorbents by further optimizing the synthesis method.

Deactivation in the presence of potential impurities such as SO<sub>2</sub> and NOx could be another issue for CO<sub>2</sub> solid sorbents. To date, there are

<sup>&</sup>lt;sup>b</sup> SCD = supercritical drying.

<sup>&</sup>lt;sup>c</sup> AH-RFSA = amine hybrid resorcinol-formaldehyde/silica.

<sup>&</sup>lt;sup>d</sup> AHSA = amine hybrid silsesquioxane aerogel.

 $<sup>^{\</sup>rm e}$  AMSA = amine-modified SiO $_2$  aerogel.

f M-APTMS = ((3-aminopropyl)trimethoxysilane.

<sup>&</sup>lt;sup>g</sup> T-APTMS = (3-trimethoxysilylpropyl)diethylenetriamine.

h P-30-85 = TEPA modified silica aerogel synthesized by precipitation method with amine loading in the 30-85 wt% range.

i W-30-80 = TEPA modified silica aerogel synthesized by wet impregnation method with amine loading in the 30-80 wt% range.

<sup>&</sup>lt;sup>j</sup> PA = particulate aerogel.

<sup>&</sup>lt;sup>k</sup> SA-I-40-90 = TEPA impregnated hydrophilic silica aerogel with amine loading in the 40-90 wt% range.

<sup>&</sup>lt;sup>1</sup> SA-O-50-85 = TEPA impregnated hydrophobic silica aerogel with amine loading in the 50–85 wt% range.

<sup>&</sup>lt;sup>m</sup> FS-DETA-0-40 = DETA impregnated commercial silica gel with amine loading in the 0-40 wt% range.

 $<sup>^{</sup>n}$  K<sub>2</sub>CO<sub>3</sub>/SG = K<sub>2</sub>CO<sub>3</sub> modified commercial silica gel.

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