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The impact of intake air temperature on performance and exhaust emissions of a diesel methanol dual fuel engine

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HIGHLIGHTS

- The intake air temperature affecting the dual fuel engine performance was investigated.
- Emissions from DMDF engine affected by the intake temperature were examined.
- 16 DMDF indicated thermal efficiency affected by intake air temperature was studied.
- Increasing intake air temperature can reduce all of gaseous emissions but NO_x.
- Increasing intake air temperature will worsen PM emissions.

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ABSTRACT

To better understand how the intake air temperature and methanol fumigation affect the performance and emissions of diesel engine, a parametric study concerned with methanol mass fraction and intake air temperature was conducted. In this study, methanol port injection was used for preparing homogenous charge for diesel methanol dual fuel operation on a 6-cylinder turbocharged intercooler heavy duty (HD) diesel engine. The testing work was operated at a constant load and constant engine speed of 1500 r/min. The experimental results show that there was a strong coupling between the intake air temperature and the methanol fraction to performance and emissions of the engine. At dual fuel operation mode, decreasing intake air temperature reduced the indicated thermal efficiency and exhaust gas temperature and the trend was more evidently as methanol energy fraction increased. Decreasing of intake air temperature also prolonged the ignition delay, which caused a later combustion phasing and smaller peak cylinder pressure. By the induction of methanol, NO_x, NO and smoke emissions decreased markedly, while NO₂, CO, total hydrocarbon (THC), formaldehyde and methanol emissions increased. However, increasing the intake air temperature would inhibit the NO₂, THC, CO, formaldehyde and methanol emissions and increase NO, NO_x and soot emissions. The effect of intake air temperature and methanol fraction on emissions is more remarkably at a larger methanol fraction (30% or more) and higher intake air temperatures such as 60-70 °C.

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37 1. Introduction

The increasing energy demand, depleting oil reserves and environmental pollution problems associated with the use of fossil

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http://dx.doi.org/10.1016/j.fuel.2015.08.073 0016-2361/© 2015 Elsevier Ltd. All rights reserved. fuels have sparked renewed interest to find out clean alternative fuels [1–4]. Alcohols such as methanol, ethanol and butanol are competitive alternative fuels due to their liquid nature, high oxygen contents, high octane number and their production from renewable biomass [4]. Among all these alcohol fuels, methanol is one of the most promising fuels as it can be easily synthesized from abundant source such as coal, nature gas and biomass, especially in the methanol adequate country such as Canada, China [1]. Methanol has been used in combustion engines since their invention. Although methanol is known to be excellent fuels for spark ignition engines due to its high octane ratings, lean flammability limits, increased thermal efficiency and low exhaust emissions. It does not carry a similar attraction when its use in diesel engines,

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Abbreviations: HD, heavy duty; THC, total hydrocarbon; NO_x, nitrogen oxides; PM, particulate matter; DMCC, diesel/methanol compound combustion; DMDF, diesel methanol dual fuel; HC, hydrocarbon; CO, carbon monoxide; NO₂, nitrogen dioxide; HCCI, homogeneous charge, compression ignition; SMD, Sauter Mean Diameter; NO, nitrogen monoxide; TDC, top dead center; ECU, electronic control unit; AVL, Anstalt für Verbrennungskraftmaschinen List; FTIR, fourier transform infrared spectroscopy; PID, proportion integration differentiation; SR_m, substitution ratio; AFR, air fuel ratio; LHV, low heat value; SR, substitution ratio.

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although methanol has many advantages as a diesel engine fuel, including lower nitrogen oxides (NO_X) forming potential, negligible particulates (PM) emissions, lack of sulfur and sulfur compounds, and easy refueling [5]. This is because there are difficulties in the ignition of air–fuel mixtures when methanol is used in diesel engines, mainly due to its low cetane number, high latent heat of vaporization and long ignition delay [3–5].

Typically there are several methods have been investigated to overcome ignition problems associated with methanol used in diesel engines. Adding ignition improvers to methanol has helped to increase the methanol fuel's cetane rating by adding compounds to the fuel, which auto-ignite very easily in unmodified diesel engines. These compounds which are typically nitrates are called ignition accelerators of improvers. However, they can be expensive and their toxicities in the raw fuel or as a component of the engine exhaust are not known [6,7]. To avoid the use of ignition improvers, investigators have utilized dual fueling, one of the progress is by diesel methanol emulsions [8-16] and the other by using two fuels simultaneously as inducting the methanol with a separate methanol fuel injector [17-23]. Both of these techniques have their advantages and drawbacks. Stabilized emulsions require use of surfactants and have a limitation of blending rate, while dual injection equipment increases cost of fuel injection systems considerably.

97 However, the fumigation methanol seems to be more potential 98 for it can allow the large amount of injected methanol to vary 99 depending on actual requirements, which could achieve advanced 100 combustion mode [24] and flexible switch between duel fuel mode 101 and neat diesel operation [19], additionally minor modification for 102 the engine as well. Moreover, since the methanol is mixed in the 103 intake air it is possible to increase the power output from diesels by use of methanol diesel dual fuel [19,22]. Many investigations 104 105 have been carried out related to performance and emissions with 106 methanol fumigated diesel engine. Yao et al. [19] investigated 107 the effect of diesel/methanol compound combustion (DMCC) on 108 diesel engine combustion and emissions. The experimental results 109 reported that smoke number, nitrogen oxides reduced as carbon 110 monoxide and unburned hydrocarbon emissions increased with 111 fumigation of methanol fuel. Wei et al. [23] and Masimalai [25] 112 investigated a higher premixed methanol fraction (more than 70 113 percent methanol in the fuel energy share) in a six cylinder diesel engine and single cylinder engine respectively. Both found an 114 increase of hydrocarbon (HC) and carbon monoxide (CO) and 115 116 decrease in NO_X and particulate. It also found an increasing of nitrogen dioxide (NO_2) and formaldehyde emissions by the use of 117 118 methanol fumigation. Investigations regarding fuel deliver timing 119 reported by Liu et al. [22] and Liu et al. [17] respectively, they 120 found that advancing the fuel delivery angle would inhibit the 121 HC, CO, and smoke emissions but promote NO_X emissions. Liu 122 et al. [26] investigated the effect of injection pressure on combus-123 tion and emissions of the diesel methanol dual fuel, as the diesel injection pressure increases, CO and HC emissions are decreased, 124 however, CO₂ and NO₂ emissions are slightly increased. An investi-125 126 gation by Cheung et al. [20] found that by the use of a diesel oxi-127 dization catalyst the emission of HC and CO got to the same level 128 of neat diesel operation.

129 Methanol has higher latent heat of vaporization than that of diesel (about 1100 kJ/kg versus 250 kJ/kg) and a lower calorific 130 value (about 20.1 MJ/kg versus 42.8 MJ/kg) [27,28], which means 131 132 methanol needs a much higher (about 9.37) evaporation heat for 133 a given energy output. Reduction of charge temperature leads to 134 lower the temperature in the cylinder at the time of diesel fuel 135 injection thereby prolongs ignition delay. Meanwhile, reduction 136 of the charge temperature also increases the intake air mass, and 137 methanol with high oxygen content gets a much leaner A/F (air/-138 fuel) ratio (about 6.4 versus 15), which caused a leaner combustion

[2]. Usually intake air temperature was used to modify the ignition 139 timing of homogeneous charge, compression ignition (HCCI) com-140 bustion [29], or to extend the lambda limitation for the diesel 141 engine. For dual fuel operation, effect of intake air temperature 142 on diesel methane dual fuel has been concerned widely interests. 143 Experiment investigations operated by Adb-alla et al. [30] and 144 kumar and Raj [31] found that higher intake air temperature 145 increases the exhaust NO_x but reduces the unburned hydrocarbon 146 and carbon monoxide emissions. Simulation work bv 147 Papagiannakis [32] also got a similar result. For diesel dual fuel, 148 previous studies were mainly dealt with effect of intake air tem-149 perature on combustion and emissions characteristics in a single 150 cylinder, air cooled, naturally aspirated methanol fumigated diesel 151 engine. Varde [33] found that decreasing inlet charge temperature 152 reduced peak cylinder pressure and increased ignition delay period 153 at a given methanol energy fraction. Experiment and simulation 154 work by Su et al. found that ambient temperature shows greatly 155 effect on the spray and atomization of diesel fuel. The increasing 156 of ambient temperature would improve the activation of diesel 157 fuel, accelerating the diesel fuel evaporation, change the SMD 158 distribution and spray tip penetration [34]. For a given level of 159 methanol energy, reducing inlet charge temperature reduced NO_X 160 levels. The effect was more significant at lower temperatures rang-161 ing from 0 °C to -5 °C. Another investigation was made by Yilmaz 162 [13] about the effects of intake air preheat on diesel methanol 163 blends. Nadir found that preheating the intake air tended to reduce 164 the production of CO and HC, while slightly increasing nitrogen 165 monoxide (NO) emission. 166

In previous study, intake air temperature shows significantly 167 impacts on combustion and emission characteristics of diesel 168 methanol dual fuel engines. However, the experiments are oper-169 ated at low level of intake charge temperature and firm methanol 170 energy fraction. The coupling effect of intake charge temperature 171 and methanol mass fraction has not been investigated. Actually, 172 in our tests either on bench or in fields, we found that intake 173 charge temperature had great impacts to the emission and fuel 174 consumption. The effect was different at varied methanol mass 175 fraction. To gain a better understanding of how the intake air tem-176 perature and methanol fumigation affect the performance and 177 emissions of diesel engine, further investigation concerned with 178 a higher mass fraction of methanol and larger intake air tempera-179 ture range is needed. In this study, an experimental study was 180 undertaken to investigate engine performance and emission char-181 acteristics versus substitution ratio at various intake air tempera-182 ture. The testing diesel engine was operated at a constant load 183 and engine speed. Performance and emission characteristic at var-184 ious ratios of methanol substitution at different intake air temper-185 ature were investigated. 186

2. Experiment setup and procedure

2.1. Research engine

Experiments were conducted on a Weichai WP-series diesel 189 engine, which is a typical turbo charged common rail 6 cylinder 190 heavy duty diesel engine with a displacement of 1.621 l/cylinder. 191 The engine specifications are listed in Table 1. Fig. 1 shows a 192 schematic of the engine, which has been converted for dual fuel 193 operation. For this study methanol was premixed with a methanol 194 low pressure common rail and methanol injector, which was 195 depicted in Fig. 1. Methanol was injected into intake manifolds 196 with a pressure of 0.42 MPa. The methanol injection was controlled 197 by a dedicated electronic control unit (ECU). 198 199

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The properties of diesel and methanol fuel are shown in Table 2. The diesel fuel used in this study contained sulfur less than

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