#### Fuel 140 (2015) 453-461

Contents lists available at ScienceDirect

## Fuel

journal homepage: www.elsevier.com/locate/fuel

# Innovative low temperature regenerable zinc based mixed oxide sorbents for synthesis gas desulfurization



Vincent Girard <sup>a,b</sup>, David Chiche <sup>a,\*</sup>, Arnaud Baudot <sup>a</sup>, Delphine Bazer-Bachi <sup>a</sup>, Isabelle Clémençon <sup>a</sup>, Florent Moreau <sup>a</sup>, Christophe Geantet <sup>b</sup>

<sup>a</sup> IFP Energies nouvelles, Rond-point de l'échangeur de Solaize, BP 3, 69360 Solaize, France <sup>b</sup> Institut de Recherches sur la Catalyse et l'Environnement de Lyon (IRCELYON), UMR5256 CNRS – Université Lyon I, 2 avenue Albert Einstein, 69626 Villeurbanne cedex, France

### HIGHLIGHTS

• ZnO and MoO<sub>3</sub> based materials have been studied as regenerable sulfur sorbents.

- Composite oxides show regeneration temperature up to 300 °C lower than ZnO sorbents.
- Transitional phases formations were evidenced through in situ XRD.

• Regeneration of sulfided mixed oxide is shown to exhibit synergetic effects.

Synergetic effects result from exothermic oxidative reactions of molybdenum phases.

#### ARTICLE INFO

Article history: Received 4 June 2014 Received in revised form 18 September 2014 Accepted 23 September 2014 Available online 7 October 2014

Keywords: Desulfurization Synthesis gas Purification Sorbents regeneration

#### ABSTRACT

Zinc oxide-based materials are commonly used for the final desulfurization of synthesis gas in IGCC and Fischer-Tropsch based XTL processes. The formation of large amount of solid waste is the major issue of this process. In-situ oxidative regeneration is a promising way to reduce this waste formation and enhance desulfurization process efficiency and economics. However, previous studies showed that one of the major drawbacks of oxidative regeneration of sulfided oxides relies in the high operating temperature range required to overcome the formation of inhibitory sulfate phases. A preliminary work of the authors focused on single oxides identified that regeneration temperature of zinc oxide-based sorbent could be reduced through the addition of molybdenum oxide. Two composites oxides - a single oxides mixture (ZnO and  $MoO_3$ ) and a mixed oxide (ZnMoO<sub>4</sub>) – were synthesized and characterized. Their sulfidation and oxidative regeneration properties were investigated through thermogravimetry and in-situ characterizations. Sulfidation of the single oxides mixture was shown to be similar to the combination of the sulfidation of both independent single oxides. Mixed oxide sulfidation leads to ZnMoO<sub>4</sub> phase demixing into ZnS, MoS<sub>2</sub> and ZnMoO<sub>3</sub>. The oxidative regenerations of the sulfided single oxide mixtures and mixed oxide are initiated, respectively, at 350 °C and 300 °C. These temperatures are 250 °C and 300 °C lower than the regeneration temperature of a pure ZnS. For the sulfided mixed oxide regeneration is even complete at 500 °C under isothermal conditions. Regeneration of sulfided oxides mixture and mixed oxide was thus shown to exhibit synergetic effects, resulting from exothermic oxidative reactions of molybdenum phases. Heat energy released during these reactions is assumed to enhance ZnS oxidation kinetics at a temperature lower than the previously measured one.

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### 1. Introduction

Integrated Gasification Combined Cycles (IGCC) power generation processes and Fischer–Tropsch based XTL processes (XTL for X = Biomass, Coal, or Gas To Liquids) constitute efficient and

\* Corresponding author. Tel.: +33 4 37 70 22 89. *E-mail address:* david.chiche@ifpen.fr (D. Chiche). cleaner alternative technologies for future energy production [1–3]. Both technologies are based on a first step of feed gasification into a synthesis gas or syngas, composed mainly of a mixture of CO and H<sub>2</sub> [4]. In IGCC processes, the syngas is burnt into a gas turbine to produce electrical energy. In the XTL processes, the syngas is converted into hydrocarbon fuel *via* the Fischer–Tropsch reaction [5–7]. Hydrogen sulfide constitutes one of the main impurities of synthesis gases [8]. This compound mixed to H<sub>2</sub>, is responsible



for the corrosion of the industrial units [9], especially the combustion turbine blades used in the IGCC. On another hand, it is also a poison of Fischer-Tropsch catalysts (cobalt-, iron-, and ruthenium-based) because of its irreversible chemisorption on their active sites [10-12]. Therefore, the sulfur content specifications in syngas are very drastic for such industrial units, below 10 ppmv for IGCC [13,14] and 0.05 ppmv for XTL [15,16]. Syngas bulk desulfurization is commonly conducted by chemical or physical solvents [17,18], though these technologies do not allow to achieve complete H<sub>2</sub>S removal. Indeed, expected H<sub>2</sub>S syngas content at solvent-based acid gas removal systems outlet (in the range 0.1-1 mol. ppm) remains higher than sulfur syngas content tolerated at Fischer–Tropsch process inlet [8,11]. Therefore deep desulfurization of syngas is generally achieved with solid sorbents based on metal oxides which can irreversibly react with H<sub>2</sub>S according to the following generic reaction:

#### $Me_xO_y(s) + yH_2S(g) \rightarrow Me_xS_y(s) + yH_2O(g)$

Because of the important and various initial amounts of  $H_2S$  (1–10,000 ppm) [19], the drastic sulfur specifications required, and the large syngas flow rates to be treated (around 100 kg s<sup>-1</sup> for an IGCC power plant) [20], the use of metal oxides based sorbents imposes either huge amounts of solids with large reactor or the use of small reactors and frequent changes of solid sorbent. In both cases, the large amount of solid waste produced is the major disadvantage of the sorbent-based syngas desulfurization, and may also alter process operation, efficiency, and economics. The *in-situ* regeneration of the sulfided sorbent, back to the oxide phase, during the process is an identified solution to improve desulfurization processes.

The optimization of such regenerable H<sub>2</sub>S sorbent should be guided by two main targets: (1) offering irreversible sulfidation reaction when in contact with H<sub>2</sub>S in order to minimize to the lowest possible level the  $H_2S$  concentration in the syngas, and (2) being able to get back to the oxide state when in contact with  $O_2$ at the lowest possible temperature. The sulfidation and oxidative regeneration properties of single oxides were studied in the literature through thermochemical calculations [21–24]. It could be concluded from these studies that the single oxide sulfidation reaction was strongly affected by the syngas reductive atmosphere. Under these conditions, ZnO can be reduced into Zn which volatilized above 600 °C [25], reductions of CuO [26], Fe<sub>x</sub>O<sub>y</sub> [27] and Mn<sub>x</sub>O<sub>y</sub> [28] are faster than the related sulfidation reactions. Moreover, the sulfidation of Cu or Fe and the reduced manganese oxide are kinetically limited [26,27,29]. The sulfidation equilibrium of CeO<sub>2</sub> in reductive atmosphere seems to be favorable and leads to the formation of  $Ce_2O_2S$  [30].

However, the formation and thermal stability of refractory sulfate phases in oxidative regeneration conditions were pointed out as the main issues of this regeneration process [24,31–33]. Indeed sulfate formation leads to a decrease of the sorbent reactivity and durability [29,34,35], and detrimental particles sintering is favored at the high regeneration temperature required for sulfate decomposition [36]. Furthermore, the high temperatures required for the sulfate decomposition will affect the overall thermal efficiency of the process and will impose the use of refractory alloys to manufacture the industrial reactors [20].

In order to overcome the limitations of single oxide-based sorbents, "composite oxide sorbents" such as for example zinc ferrite (ZnFe<sub>2</sub>O<sub>4</sub>) [37], zinc titanate (Zn<sub>x</sub>Ti<sub>y</sub>O<sub>x+2y</sub>) [38], or copper chromite (CuO–CrO<sub>2</sub>) [39] were developed through a series of incremental improvements in order to stabilize the long-term performance of H<sub>2</sub>S sorbent [40], optimize the operating conditions of the process [41], and decrease the regeneration temperature below 500 °C [41–44].

In a previous work [45], a global approach was proposed to study the physical and chemical phenomena involved during both sulfidation and regeneration steps of single oxides and corresponding sulfides by a confrontation between thermochemical calculations and experimental approaches. Some single oxides were thus identified to design a low temperature regenerable H<sub>2</sub>S sorbent. In particular, zinc oxide was shown to exhibit high sulfidation ability and restricted sulfate formation upon the ZnS surface particles during the oxidative regeneration process, in comparison to other sulfides of transition metal such as copper, manganese or iron. MoO<sub>3</sub> shown attractive properties, as the oxidative regeneration of the sulfided MoO<sub>3</sub> occurs through fast, highly exothermic and complete reaction below 500 °C.

Regarding the distinct properties of these two metal oxides, we focus in this paper on the reactivity of two different zinc and molybdenum based materials: a ZnO and MoO<sub>3</sub> single oxides physical mixture and the ZnMoO<sub>4</sub> mixed oxide. The objectives of this work are to evaluate the difference between the two materials and to identify potential synergetic effects between zinc and molybdenum phases, to study the physical and chemical phenomenon involved in sulfidation and oxidative regeneration reactions of these materials, and to validate the global approach previously proposed.

#### 2. Materials and methods

#### 2.1. Oxide materials syntheses

The single oxides mixture,  $ZnO-MoO_3$  was obtained by physical milling of  $MoO_3$  and ZnO materials. ZnO material was synthesized from thermal decomposition of precursor at 500 °C for 2 h. The precursor was  $(ZnCO_3)_2 \cdot (Zn(OH)_2)_3$  (Aldrich, purity > 58% Zn).  $MoO_3$  precursor was obtained from a chemical supplier, and was used as received after material characterizations.

Mixed oxide  $ZnMoO_4$  material was synthesized by successive calcinations steps at 450 °C and 500 °C and physical milling of the previous  $ZnO-MoO_3$  single oxides mixture.

#### 2.2. Thermogravimetry measurements

The sulfidation of the composite oxides was followed by thermogravimetric analysis (TGA) at 350 °C and atmospheric pressure, using a commercial magnetic suspension balance (Rubotherm). The feed was composed of 0.9% H<sub>2</sub>S diluted in H<sub>2</sub> with a constant flow (10.8 NL h<sup>-1</sup>). Oxide samples were firstly heated under a Helium flow up to 350 °C, and then the inlet valve was switched to the H<sub>2</sub>S-H<sub>2</sub> mixture under isothermal conditions. Sulfidation step had been conducted for 12 h.

Oxidative regeneration reaction of the sulfided sorbents were followed by TGA-DSC (Netzsch STA-449C Jupiter). Experiments with linear temperature variation were conducted by heating sulfided samples in an oxidative gas mixture  $(5\% O_2 \text{ in } N_2)$  at 5 °C/min from 49 °C to 625 °C. Isothermal experiments were also conducted on sulfided samples, which were first heated at 5 °C/min to 500 °C under N<sub>2</sub>, and then treated at 500 °C by an oxidative gas mixture (5% O<sub>2</sub> in N<sub>2</sub>) for 2 h. This gas mixture composition was chosen to limit sulfate formation [45]. In both kinds of experiments, gas flow rate was set to 9 NL h<sup>-1</sup>. The exhaust gases were analyzed by mass spectrometry (Netzsch QMS-430C Aeolos).

#### 2.3. Materials characterizations

Materials crystalline phases were characterized by X-ray diffraction (XRD) using a PANalytical X'Pert PRO diffractometer operating with Cu K $\alpha$  radiation ( $\lambda$  = 1.54182 Å). Materials textural Download English Version:

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