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Effect of MoO₃ on the heat resistant performances of nickel based MCM-41 methanation catalysts

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HIGHLIGHTS

• Several Ni-Mo based MCM-41 catalysts were prepared by the impregnation method.

15 • The Ni–Mo catalysts showed excellent performances of resistance sintering.

• The addition of MoO₃ can enhance the interaction between the nickel and the support.

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ABSTRACT

Several Ni–Mo based catalysts with Mo content from 1 wt% to 7 wt% were prepared by the impregnation method with MCM-41 as the support. The effect of Mo content on the activity of the catalyst was investigated for syngas methanation in a fixed-bed reactor. The addition of MoO₃ could obviously improve catalytic activity of Ni/M catalyst at low temperature of 250 $^{\circ}$ C with the CO conversion and the CH₄ selectivity from about 20%, 16% to 100%, about 80%, respectively. Ni-3%Mo/M catalyst showed the best activity with a CO conversion of 100% and a CH₄ selectivity of 94% at 350 °C under 1.0 MPa and 12000 ml/g/h with a 3:1 molar ratio of H₂ to CO. Compared with Ni/M catalyst, Ni-Mo/M catalysts showed higher resistance to sintering and no decrease in the catalytic activity after calcination at 700 ° C for 2 h. In the 100 h stability test under atmospheric pressure, the CO conversion and the CH₄ selectivity obtained on Ni-3%Mo/M catalyst maintained at about 100% and 89%, respectively, suggesting an excellent catalytic stability of this catalyst. The catalysts were characterized by N2 adsorption-desorption, CO chemisorptions, TEM, SEM-EDS, ICP, XRD, H2-TPR and XPS, and the results showed that electron transfer from MoO₃ to metal nickel was the main cause of activity improvement of Ni-Mo/M catalysts at low reaction temperature of 250 °C. The addition of MoO₃ could obviously improve the heat resistant performance of Ni/M catalyst. The results of TPR, SEM-EDS and XRD showed that the addition of MoO₃ could enhance the interaction between metal nickel and the support in the way of Ni-Mo alloy, which inhibited the catalyst sintering.

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52 **1. Introduction**

53 As a high efficient and clean energy, substitute natural gas (SNG) has attracted increasing attention duo to continuous rising 54 55 prices and exhaustion of natural gas [1]. Generally, SNG is produced via gasification of coal [2] and biomass [3], which produces 56 syngas (the mixture of H₂ and CO), followed by subsequent CO 57 methanation process (CO + $3H_2 \rightarrow CH_4 + H_2O$; $\Delta H_{298K} = -206.1$ 58 KJ/mol), which is a highly exothermic and thermodynamically fea-59 sible reaction. Since some metals such as Ni, Ru, Fe and Co, were 60 61 discovered by Sabatier and Senderens that they could catalyze the methanation reaction in 1902 [4], many methanation catalysts 62

0016-2361/\$ - see front matter @ 2013 Published by Elsevier Ltd. http://dx.doi.org/10.1016/j.fuel.2013.07.102 have been developed. However, Ni based catalysts are still the most favorable choice for the production of SNG due to its relatively high catalytic activity and suitable price [5]. But the syngas methanation reaction is highly exothermic, which easily leads to sintering of active metal and/or the support [6]. The support can significantly affect the dispersion of the active metal and the stability of the catalyst. Thus, the choice of a suitable support is important for the preparation of the catalyst.

Since the invention of MCM-41 mesoporous molecular sieves by the Mobil company, transition metal supported MCM-41 catalysts have been extensively studied duo to excellent properties, such as high specific surface area, regular pore structure of nanometer size and adjustable heteroatom content [7]. The nickel based MCM-41 catalyst with high metal loading and good dispersion of active metal could be prepared by the incipient wetness impregnation method with a nickel precursor solution [8]. Wojcieszak et al. [9]

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reported that the nickel based MCM-41 catalyst showed good activity in the hydrogenation of benzene, which prepared via a wet impregnation method. In our previous work [10], the nickel based MCM-41 catalyst showed good activity in the production of SNG via syngas methanation, but poor thermal stability, which was easily sintered after high temperature calcination. Therefore, it is still a challenge to develop metanation catalysts with both high activity and good thermal stability against sintering.

87 In recent years, bimetallic catalysts have attracted worldwide 88 attention. The interaction between the two metals may provide 89 pathways to higher activity and better anti-sintering performance 90 [11,12]. One explanation for the synergetic interaction between the two metals is physical promotion provided by one of the metals. 91 92 The other one is electron transfer from one of the metal (or metal 93 oxide) sites to the second metal [13]. As an important catalytic pro-94 moter. Mo can improve the dispersion of active metal and the 95 activity of the catalyst in many situations. The addition of Mo could 96 significantly promote the activity, the sulfur resistance and the 97 anti-sintering performance of Ni-based catalyst [14,15]. The sulfur resistance of Mo is a potential advantage for industrial application 98 99 due to copious amounts of sulfur in the syngas used in commercial 100 operation [16].

101 The Ni–Mo bimetallic supported catalysts with Ni as the main 102 active component and Mo as the promoter [14,15] were widely 103 investigated. The accession of Mo could promote the reduction of 104 NiO, which improved catalytic activity of the nickel catalyst. For 105 bimetallic catalysts, the synergetic interaction between the two 106 metals has been explained either by physical promotion provided 107 by Mo species or by electron transfer from MoO_x sites to the other 108 metal [17–19]. The coverage of active metal sites by MoO_x species 109 at high metal loadings also needs to be taken into account as a 110 third interaction mechanism [17,19,20]. However, the effect of Mo on the heat resistant performance on the nickel based MCM-111 112 41 catalyst, which was used to produce SNG via syngas methana-113 tion, was scarcely investigated.

114 In this paper, several Ni-Mo catalysts with Mo content from 1 115 to 7 wt% were prepared via an impregnation method by adding 116 MoO₃ into the nickel based MCM-41 catalysts and the catalytic 117 behavior of the catalyst for the production of SNG via syngas 118 methanation with a 3:1 molar ratio of H₂ to CO was investigated 119 and discussed. The effect of Mo on the structure and catalytic activ-120 ity of the catalyst was studied by various characterization means, such as X-ray diffraction (XRD), nitrogen adsorption-desorption 121 122 measurements, inductive coupled plasma emission spectrometer (ICP), CO chemisorptions, transmission electron microscopy 123 124 (TEM), scanning electron microscopy-energy dispersive spectrom-125 eter (SEM-EDS), H₂ temperature-program reduction (H₂-TPR) and 126 X-ray photoelectron spectra (XPS).

127 2. Experimental

128 2.1. Catalyst preparation

129 2.2.1. MCM-41 preparation

MCM-41 materials were synthesized to the procedure of Liu 130 131 et al. [21]. Cetyltrimethyl ammonium bromide (CTABr, C₁₆H₃₃ (CH₃)₃NBr, 99% pure, Merck) and tetraethylorthosilicate (TEOS, 132 133 $C_8H_{20}O_4Si$, 99% pure, Merck) were used as the surfactant and the 134 silica source, respectively. The surfactant (CTABr) was dissolved 135 in the deionized water with vigorously stirring at 40 °C. Then the 136 silica source (TEOS) was slowly added into the solution and the 137 PH value of the solution was adjusted to 11. The resulting gel with 138 a molar composition of TEOS:CTABr:NaOH:H₂O of 1:0.12:0.2:100, 139 was aged at room temperature for 2 h under vigorously stirring, 140 transferred into an autoclave and crystallized statically at 120 °C

for 24 h. After being cooled to room temperature, the resulting solid was centrifuged, washed with deionized water and dried at $100 \degree C$ overnight. The MCM-41 support was obtained by calcination in air (6 h at 550 °C, heating rate = 1°C min⁻¹) to remove the template. 141

2.2.2. Ni-Mo/MCM-41 catalyst preparation

The Mo based MCM-41 catalysts with different Mo content (1° 147 wt%, 3°wt%, 5°wt%, 7°wt%) were prepared by the incipient wetness 148 impregnation with $(NH_4)_6Mo_7O_{24}\cdot 4H_2O$ (99% pure, Merck) as the 149 molybdenum precursor and MCM-41 as the support under vacuum 150 overnight [22]. After impregnation, the samples were dried at 120 ° 151 C for 12 h and calcined in air at 550 °C for 4 h (heating rate = 1 ° 152 C min⁻¹). The Ni–Mo based MCM-41 catalysts were prepared by 153 the same procedure with Ni(NO₃)₂·6H₂O (99% pure, Merck) as 154 the nickel precursor and the Mo based MCM-41 catalyst as the sup-155 port and calcined in air at 550 °C for 4 h (heating rate = 1 °C min⁻¹). 156 The nickel content of all the catalysts was 10 wt%. The catalysts 157 were designated as Ni-xMo/M, in which x represented the molyb-158 denum weight content. For comparison, the nickel based MCM-41 159 catalyst with 10 wt% nickel content was also prepared by the same 160 procedure and MCM-41 as the support. And the catalyst was des-161 ignated as Ni/M. 162

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2.2. Evaluation of catalyst performance

The evaluation of Ni/M and Ni-Mo/M catalysts for syngas 168 methanation was carried out in a continuous flow fixed-bed reac-169 tor with a stainless steel tube (length: 40 cm, inner diameter: 170 10 mm). 500 mg catalyst (sieve fraction 100 mesh) was filled in 171 the tubular reactor and reduced in situ at 500 °C (except for special 172 instruction) for 2 h in a continuous flow of pure H_2 (50 ml/min). 173 Ultimately, it was tested over a temperature range of 250-650 °C 174 and a pressure range of atmospheric pressure to 1.0 MPa. The 175 mixed reactant gas consisted of $H_2/CO/N_2$ with a molar ratio of 176 3:1:1, in which N₂ was added as an internal standard gas for GC 177 analysis. The weight space velocity was selected to be 12000 ml/ 178 g/h. The outlet gases were cooled by a cold water trap and analyzed 179 on-line by the gas chromatograph (Techcomp, GC7890T) with a 180 TDX-01 column using the thermal conductivity detector. To calcu-181 late the CO conversion and the CH₄ selectivity, the outlet gases 182 were collected after half an hour of steady-state operation at each 183 temperature. The calculation formulas were described as follows: 184 185

CO conversion :
$$X_{CO}(\%)$$

$$=$$
 (moles of CO reacted) \times 100/(moles of CO supplied) (1)

$$CH_4$$
 selectivity : $S_{CH4}(\%)$

$$=$$
 (moles of CH₄ prepared) \times 100/(moles of CO reacted) (2) 190

$$CH_4 \text{ yield}: Y_{CH4}(\%) = X_{CO} \times S_{CH4}/100$$
 (3) 19

2.3. Characterization

The porous structure of the catalyst was investigated using an ASAP 2020 (Micromeritics) instrument and the pore size distribution was calculated by the Barret-Joyner-Hallender (BJH) method using the desorption branch. XRD patterns were recorded on a Rigaku D-MAX2500-PC using Cu K α radiation ($\lambda = 1.54056$) at 199 50 kV and 100 mA. The metal compositions of the samples were analyzed by ICP. H₂–TPR experiment was carried out on a TP- 201

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