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Demulsification of heavy crude oil-in-water emulsions: A comparative study between microwave and thermal heating

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HIGHLIGHTS

- A comparative study of demulsification by microwave and oil bath heating.
- 16 Results were confirmed by steady state fluorescence spectrometry.
- The effect of a demulsifier on the oil-in-water (O/W) emulsion stability was studied.
- The effect of salt content on the O/W emulsion stability was evaluated.
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ABSTRACT

Oil-in-water (O/W) emulsions are works in an innovate manner by which otherwise highly viscous heavy and extra-heavy crude oils can be transported from producing sites to transforming sites through pipelines. In spite of the important reduction in viscosity and pressure drops, water must be removed from the crude oil before further process or refining. Hence, the present study discusses the demulsification of an O/W emulsion prepared with Mexican heavy crude oil. A comparative study was carried out between microwave and oil bath heating with regard to water separation time. The effect of a chemical demulsifier and salt content of the O/W emulsion's aqueous phase was also investigated. Microwave dielectric heating of O/W emulsions showed a greater degree of water separation in less time than conventional oil bath heating. Water separation of O/W emulsions increased with microwave power and salt content of the aqueous phase, and in the presence of a chemical demulsifier. Finally, the fluorescence emission spectra of the initial and treated O/W emulsions were in agreement with the water separation results and provide a quick and effective way to study the demulsification processes.

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50 1. Introduction

Currently, most of the recoverable petroleum in Mexico and in 51 52 many other countries is heavy crude oil with an API gravity equal to or lower than 20°. The complex composition of these crude oils 53 makes them difficult and expensive to produce and transport 54 through pipelines due to their low mobility and flow near ambient 55 56 temperature. Also, their high asphaltene and paraffin contents promote pipe clogging, pressure drops, and consequently a lower 57 production rate than lighter crude oils. Various well developed 58 59 strategies are used to facilitate the transport of heavy crudes, such 60 as dilution with organic solvents, lighter oils, or condensates; 61 heating (and by necessity, thermally isolating) pipelines; and the 62 use of flow improvers and drag reducing additives. Nevertheless,

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0016-2361/\$ - see front matter \odot 2013 Published by Elsevier Ltd. http://dx.doi.org/10.1016/j.fuel.2013.05.094 innovative approaches such as the formation of oil-in-water (O/ W) emulsions, known as inverse emulsions within the petroleum community, may contribute as an alternative technology to reduce crude oil's viscosity and increasing flow with only minor operational issues [1].

The formation of O/W emulsions, industrially known as the Orimulsion process [2–4], has proved to be a very reliable method because of its low cost and relative ease in industrial implementation. However, this approach, in which crude oil is transported as drops dispersed in a water continuous phase (20–30% w/w), requires emulsion breakage and water separation before further refining. While there has been fewer studies of O/W emulsions as found in the present article, it is worth mentioning that extensive studies exist on the demulsification of water-in-oil (W/O) emulsions, since emulsion of this type commonly forms during crude oil production and pipelining [5–7].

The presence of emulsions is a common feature in oil processing. Although the formation of emulsions of different types, such Q4 80

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as W/O, O/W, O/W/O y W/O/W, is possible, the first two are the most common. These are responsible for operational problems such as destabilization and deposition of asphaltenes and paraffin and clogging/blockage and subsequent pressure drops along transport pipes and during drying and desalination processes. In O/W emulsions, water is the continuous phase. This type of emulsion is favored since it effectively carries the otherwise viscous heavy and extra-heavy crude droplets in a far more fluid form through the transport pipes [8–12].

90 Microwave technology has gained great popularity in recent 91 years owing to its higher efficiency at speeding up most chemical 92 reactions [13]. However, there is still considerable controversy 93 about the action mechanism of microwave dielectric heating with respect to the enhancement of chemical reactions. Some authors 94 95 attribute such reaction and process acceleration under microwave 96 dielectric heating to the phenomenon known as "specific micro-97 wave effect." This is considered a nonthermal effect of microwaves 98 and generally associated with the selective absorption of energy by polar molecules [14-16]. Another hypothesis states that micro-99 wave effect is merely thermal [17,18]. 100

101 Much attention is focused on the microwave enhancement of 102 chemical reactions and breakage of W/O emulsions because micro-103 wave irradiation has demonstrated the ability to accelerate these 104 processes. Although the earlier studies concerning microwave 105 technology for emulsion separation were focused on O/W systems 106 or both O/W and W/O systems [9-12], microwave technology has rarely been considered as a demulsification process of O/W emul-107 108 sions because this kind of emulsion is an emerging technology for crude oil transportation [19]. Recently, the application of ionic 109 110 compounds in conjunction with microwave energy was studied 111 in the breaking of W/O emulsions [20,21].

This work discusses the demulsification of an O/W emulsion 112 113 prepared with a Mexican heavy crude oil and the use of a new ionic glycine-based demulsifier under microwave and oil bath heating. 114 115 The effects of salt content on the O/W emulsion's aqueous phase 116 and addition of chemical demulsifier to the water separation frac-117 tion were also studied. Finally, fluorescence emission spectra of 118 every initial and treated O/W emulsion were obtained in order to 119 gain further insight about the non-aggregated and aggregated 120 states of the heavy crude oil during the demulsification processes.

121 **2. Experimental section**

122 2.1. Materials and equipment

123 All reagents were purchased from Aldrich Chemical Co. Micro-124 wave experiments were conducted on a CEM Discover Synthesis 125 Unit (Monomode system) operating at 2450 MHz monitored by a PC. The Differential Scanning Calorimetry (DSC) was carried out 126 127 using a Shimadzu model DSC-60A. Karl Fischer titrator (model Or-128 ion AF-8) equipped with a double platinum electrode was em-129 during the water-content determination tests. ploved 130 Micrographs were taken in a Nikon Eclipse E800 optical micros-131 copy. Particle size determination was performed with a freshly 132 prepared emulsion using a counter and particle size analyzer 133 PPS-Accusizer 780. Zeta potentials of the nanoemulsions were esti-134 mated from electrophoretic mobility measurements using phase 135 analysis light scattering (PALS) in the Brookhaven ZetaPALS setup.

136 2.2. DSC measurements

137These assays were carried out under N2 at a flow rate of 20 mL/138min. Every emulsion was precisely weighed (ca. 10 mg) in an alu-139minum pan which was tightly sealed. The sample's cooling cycle140from 50 to -60 °C was scanned at a rate of -10 °C/min. Emulsion

characterization by DSC was performed twice on the same day that141emulsions were prepared.142

2.3. Fluorescence spectroscopy

The assays were performed on a RF-5301PC Shimadzu Spectro-144 fluorometer equipped with a 150 W Xe lamp and a cell tempera-145 ture controller. Emission spectra were recorded between 290 and 146 410 nm, with an excitation wavelength of λ_{exc} = 280 nm and a slit 147 width of 3 nm. From each emission spectrum, the slope (m) was 148 determined between 326 and 339 nm. This permits the study of 149 the microenvironment around the fluorophore molecules con-150 tained in the heavy crude oil and the effect of demulsifying agents 151 and heating processes [22]. Fixed wavelength data as well as emis-152 sion spectra were analyzed by means of the panorama software. 153 Appropriate blanks were employed to correct the measurements 154 for any light scattering contribution. 155

2.4. Crude oil characterization 156

The sample of heavy crude oil (HCO) utilized in this study was 157 provided by the Mexican Petroleum Company (PEMEX) from a 158 marine well drilled in the south of the Gulf of Mexico. The samples 159 were characterized by the following standard procedures: API 160 gravity (ASTM D-287), Kinematic viscosity (ASTM D-445), salt con-161 tent (ASTM D-3230), paraffin content (UOP-46), water content 162 (ASTM D-4006), and saturated, aromatics, resins, and asphaltenes 163 (ASTM D-2007) content. Total sulfur was determined in an Antex 164 9000S, employing the standard procedure ASTM D 5453-05: Stan-165 dard Test Method for Determination of Total Sulfur in Light Hydro-166 carbons, Motor Fuels and Oils by Ultraviolet Fluorescence [23]. The 167 cloud points for NPE in salty solutions were determined in accor-168 dance with the standard procedure ASTM D 2024-09. 169

2.5. Preparation of O/W emulsions

Synthetic seawater (total salt content 40.750 ppm, standard 171 method D-1995) was used to prepare O/W emulsions, using com-172 mercially available nonylphenol ethoxylate (ethoxyl content 173 15 mol, NPE) as surfactant. NPE was dissolved in 15 mL of seawater 174 of pH 8 at room temperature to prepare a 1200 ppm solution. This 175 was poured into a jacketed glass reactor with water recirculation at 176 65 °C. The propeller of the mixer was fixed in order to remain sub-177 merged in the aqueous phase. 35 g of HCO was then added to the 178 top of the glass reactor. The reactor and mixer with surfactant sea-179 water solution and HCO were incubated at 25 °C for 10 min. Emul-180 sification proceeded at 8000 rpm for 5 min using an IKA 181 Labortechnik homogenizer. The formation of an O/W emulsion 182 was corroborated by dispersing an emulsion drop in water, DSC 183 analysis, and optical microscopy. 184

2.6. Emulsion characterization

The initial O/W emulsion was characterized by DSC on the day of preparation. The water content and micrographs were taken before and after each test. The water content reported is the average of three measurements.

2.7. Microwave demulsification tests

The microwave demulsification tests were conducted using191sealed-vessels (10 mL) containing 3.0 g of the O/W emulsion. These192were separately irradiated from 2 to 60 min at 60 °C without stir-193ring at 60 °C. The reaction temperature was followed by an internal194fiber-optic (FO) temperature probe (ruby thermometer) protected195by a borosilicate immersion well directly inserted in the reaction196

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