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57 The most common fatty esters contained in biodiesel are those 58 of palmitic acid, stearic acid, oleic acid, linoleic acid, and linolenic

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0016-2361/\$ - see front matter @ 2013 Elsevier Ltd. All rights reserved. http://dx.doi.org/10.1016/j.fuel.2013.04.031 acid. This holds for biodiesel feedstock, such as soybean, sunflower,59and rapeseed. However some tropical oils, such as coconut oil or60babassu oil contain significant amounts of shorter chain saturated61acids, such as lauric acid, myristic acid, caprylic acid, and capric62acid [1,2]. Saturated fatty esters possess higher CN and better oxi-63dative stability than their unsaturated counterparts. Using thermal64efficiency data, it was originally suggested that ethyl esters of65

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66 monounsaturated or short-chain saturated fatty acids should make 67 good alternative fuels and that they should be evaluated in long-68 term engine tests [3]. If saturated fatty acids are preferred due to 69 their greater oxidative stability, esters of decanoic acid appear 70 advantageous because they offer a compromise between cold flow 71 and cetane number. Moreover, by having accurate knowledge of 72 the influence of the molecular structure on the properties deter-73 mined, the modification of the fatty ester composition can be applied for improving biodiesel fuel properties. Important fuel 74 75 properties of biodiesel that are influenced by the fatty acid profile 76 and, in turn, by the structural features of the various fatty esters in-77 clude ignition quality, heat of combustion, cold flow, oxidative sta-78 bility, exhaust emissions, lubricity, viscosity and density. Fuel 79 density affects the mass of fuel injected into the combustion cham-80 ber and thus, the air-fuel ratio. This is because fuel injection 81 pumps fuel by volume not by mass and a denser fuel contains a 82 greater mass in the same volume. Thus, the changes in the fuel 83 density will influence engine output power due to a different mass 84 of fuel injected [4]. Isobaric thermal expansion and compressibility, characterize how temperature and pressure affect density. As 85 86 the propagation of sound is an adiabatic process, the acoustic 87 method gives the most reliable values of the adiabatic compress-88 ibility [5]. The interest in this material constant has been increased 89 in the last years due to the development of the common rail system 90 in the diesel engines. In the common rail engines, the fuel is in-91 jected into the combustion chamber under pressure up to 92 250 MPa. The injection is very rapid, thus approximately adiabatic. 93 Therefore, the adiabatic compressibility is particularly useful in the 94 estimation of the fuel injection timing [6–8].

95 In the present paper, we report experimental speeds of sound in 96 ethyl laurate and ethyl myristate measured within the tempera-97 tures from 293 to 318 K and at pressures from 0.1 MPa to 98 101 MPa, as well densities and heat capacities measured under 99 atmospheric pressure in the temperature range from 283 to 353 K 100 and 286 to 341 K, respectively. The densities and isobaric heat 101 capacities at pressures up to 100 MPa were calculated from experi-102 mental data according to the suggestion of Davis and Gordon [9]. To 103 this end, a slightly modified procedure of Sun et al. [10] was applied. 104 We aimed this work mainly at comparison of effects of pressure and 105 temperature on density, adiabatic compressibility, and isobaric 106 thermal expansion of ethyl laurate and ethyl myristate. Furthermore, we tried to find out whether the differences in the material 107 constants of the studied fuels are significant from the practical point 108 109 of view. Data similar to those reported in this work have been used in calculations of other thermodynamic parameters, in simulations, 110 111 and as a reference material for tests of performance characteristics 112 of diesel engines [6-8,11-14].

113 **2. Experimental section**

114 2.1. Materials

Ethyl laurate from Aldrich, minimum 0.98 (GC) mass fraction purity, and ethyl myristate from Aldrich, 0.99 (GC) mass fraction purity have been used in this work. The content of the main component was checked by gas chromatograph and was found to be 0.995 mass fraction.

120 2.2. Ultrasonic speed measurements

The speed of sound in liquids under test has been measured at atmospheric and higher pressures using two measuring sets designed and constructed in our laboratory [15,16]. Two measuring vessels of the same acoustic path and construction have been used, one of them designed for measurements under atmospheric pressure, the other one for measurements under elevated pressures. 126 The measuring set applies the pulse-echo-overlap principle. In 127 the acoustic cell, a single transmitting-receiving ceramic trans-128 ducer operating at 2 MHz frequency was applied together with 129 and an acoustic mirror. The pressure was applied by a hand-oper-130 ated hydraulic press connected with the chamber by a system of 131 high-pressure capillary tubes and valves. The pressure was stabi-132 lized to within 0.03 MPa and was measured with a strain gauge 133 measuring system (Hottinger Baldwin System P3MD) with accuracy 134 better than 0.15%. During the measurements, the temperature is 135 stabilized within the limits of ±0.01 K by a Haake DC 30 tempera-136 ture controller, and measured using an Ertco Hart 850 platinum 137 resistance thermometer (traceable to a NIST standard) with an 138 uncertainty of ±0.05 K and resolution of 0.001 K. 139

The uncertainty of the speed of sound measurements was estimated to be 0.03% at atmospheric pressure, 0.04% under pressures up to 60 MPa and 0.05% under pressures from 60 MPa to 101 MPa. Other details of the high-pressure device and the method of the speed of sound measurements can be found in a previous papers [15,16].

2.3. Density measurements

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The densities at atmospheric pressure were measured using a 147 vibrating tube densimeter Anton Paar DMA 5000. The uncertainty 148 of the density measurements was 0.05 kg m^{-3} , whereas the repeatability was estimated to be better than 0.005 kg m^{-3} .

2.4. Specific heat capacity measurements

The specific isobaric heat capacity was measured by a high sen-
sitivity differential scanning calorimeter Micro DSC III, manufac-
tured by Setaram and based on the Tian-Calvet principle. The
uncertainty of the isobaric heat capacity measurements was
±0.15%. More details of the measurement procedure can be found
in [17].152
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3. Measurement results

The ultrasonic speeds in compressed liquids were measured at temperatures from 293 to 318 K in about 5 K steps and under pressures up 101 MPa. The experimental values are listed in Table 1. The densities were measured under atmospheric pressure in the temperature range from 283 to 353 K in 5 K steps. The experimental values are collected in Table 2. The specific isobaric heat capacities were measured at atmospheric pressure and at temperatures from 286 to 341 K in about 0.02 K steps. In this way, ca. 3400 experimental points have been collected for each liquid. Therefore the values of isobaric specific heat capacity every 5 K are collected in Table 3.

The dependencies of the speed of sound, density, and isobaric specific heat capacity on temperature at atmospheric pressure were approximated by the following polynomials of the type:

$$y = \sum_{j=0}^{2} b_j T^j,\tag{1}$$

176 where y, is the speed of sound; u_0 , density; ρ , or isobaric specific heat capacity; C_p , at atmospheric pressure p_0 ; b_j are the polynomial 177 coefficients ($b_i = c_i$ for the speed of sound, $b_i = \rho_i$ for the density, and 178 $b_i = h_i$ for the isobaric specific heat capacity) calculated by the least 179 squares method. The backward stepwise rejection procedure was 180 used to reduce the number of non-zero coefficients. The coefficients 181 and standard deviations from the regression lines are given in Table 182 4. The standard deviations are much smaller than the measure-183 ments accuracy. 184

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