

# Reversible removal of SO<sub>2</sub> at low temperature by L-α-alanine supported on γ-Al<sub>2</sub>O<sub>3</sub>

Renpan Deng, Lishan Jia\*

Department of Chemical Engineering and Biochemical Engineering, College of Chemistry and Chemical Engineering, Xiamen University, Xiamen 361005, China

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## ABSTRACT

L-α-Alanine was supported on γ-Al<sub>2</sub>O<sub>3</sub> to remove SO<sub>2</sub> in this work. The effects of SO<sub>2</sub> concentration, water vapor and temperature on the removal of SO<sub>2</sub> were investigated. The experiment results showed that the activity of L-α-alanine on SO<sub>2</sub> removal increased significantly when supported on γ-Al<sub>2</sub>O<sub>3</sub>. SO<sub>2</sub> saturation capacity increased with increase SO<sub>2</sub> concentration, and kept about 57 mg/g when SO<sub>2</sub> concentration exceeded 1.7%. Water vapor promoted SO<sub>2</sub> removal and made SO<sub>2</sub> saturation capacity increase greatly. SO<sub>2</sub> saturation capacity decreased with increase in temperature, and room temperature was optimum. Raman spectroscopy analysis results revealed that SO<sub>2</sub> weakly adsorbed onto the adsorbent mainly due to the interaction of SO<sub>2</sub> and amino group via hydrogen bonds in the presence of water vapor. X-ray photoelectron spectroscopy (XPS) analysis results indicated that a small amount of SO<sub>2</sub> strongly adsorbed onto the adsorbent by forming aluminum sulfite. However, the strong chemical adsorption sites were saturated after the first adsorption and would no longer adsorb SO<sub>2</sub> afterwards. Ten continuous adsorption–desorption cycles showed that the adsorbent had an excellent regeneration performance.

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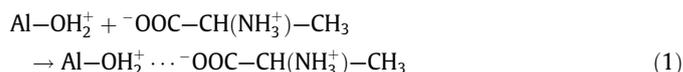
## 1. Introduction

Air pollution has been a serious problem for years and has drawn increasing attention all over the world. SO<sub>2</sub>, mainly emitted from fossil-fuel combustion, such as coals and oils, is one of major air pollutants, which have been linked with the formation of acid rain, urban smog and health hazards. Currently, flue gas desulfurization (FGD) is the most widely used techniques to control the emission of SO<sub>2</sub>. Several conventional processes, such as wet FGD, dry FGD, semidry FGD, have been adopted in industry far and wide [1,2]. However, these methods have some disadvantages, for example, a large amount of water is required and by-products such as calcium sulfate are produced and these need to be treated further. Also, the absorbents used are difficult to regenerate [3–5].

Adsorption of SO<sub>2</sub> over solid sorbents is currently employed to remove large amounts of potential hazardous waste as it is a relatively simple process and consumes less water [6]. Generally, the adsorption desulfurization process would not cause secondary pollution. Moreover, adsorbents are usually easy to regenerate. A variety of solid materials, such as lignite [7], activated carbon [8], activated carbon fibers [9,10], zeolites [11,12], and metals or metal oxides, for example, Cu or CaO supported on porous materials [13,14], have been researched for SO<sub>2</sub> removal for years. Among these adsorbents, activated carbon and activated carbon fibers have been used in commercial units, however, the high cost limited their application to some extent. Most of other sorbents are still

being at the phase of experimental research and have a long way to achieve industrial applications. Given this situation, it is urgently necessary to develop new sorbents of high efficiency, low cost, and excellent regeneration performance for FGD process.

Alkanolamines and amines, such as methyldiethanolamine and ethylenediamine [15,16], have been used for SO<sub>2</sub> removal for years. It has been demonstrated that the removal of SO<sub>2</sub> is related to amino groups in such materials. However, there are many difficulties in application of alkanolamines and amines due to their high volatility and toxicity. Amino acids have amino group, and are more environmentally friendly compared with alkanolamines and amines. Therefore, it could be a good choice to use amino acids as sorbent for SO<sub>2</sub> removal. In fact, there have been many reports about the interaction between amino acid and supports, for example, glycine supported on silica [17] and alanine supported on boehmite [18], etc. It was found that amino acid could support on various materials by different mechanisms, such as electrostatic adsorption, chemical adsorption or hydrogen-bond adsorption [19,20]. Garcia et al. studied the mechanism of L-α-alanine supported on γ-Al<sub>2</sub>O<sub>3</sub> by vibrational spectroscopy. They found that L-α-alanine interacted with γ-Al<sub>2</sub>O<sub>3</sub> by hydrogen-bonds [21], and the adsorption mechanism in the neutral immersed solutions is as follows:



Although there have been many related researches and reports, however, as far as we know, amino acids have not yet been applied as sorbents in the FGD process. In this work, we supported L-α-ala-

\* Corresponding author. Tel.: +86 592 2188283; fax: +86 592 2184822.

E-mail address: [jials@xmu.edu.cn](mailto:jials@xmu.edu.cn) (L. Jia).

nine on  $\gamma\text{-Al}_2\text{O}_3$  ( $\text{l-}\alpha\text{-alanine}/\gamma\text{-Al}_2\text{O}_3$ ) and investigated its  $\text{SO}_2$  adsorption property so as to develop a new renewable desulfurization adsorbent.

## 2. Materials and methods

### 2.1. Preparation of the adsorbents

In a typical immersed experiment [21], 1.0 g of  $\gamma\text{-Al}_2\text{O}_3$  (40–60 mesh, calcined at 600 °C for 4 h in a muffle furnace. Specific surface area is 190.6  $\text{m}^2/\text{g}$ ) was immersed in 50 mL of 0.6 mol/L  $\text{l-}\alpha\text{-alanine}$  solution and stirred at room temperature for 24 h. After the adsorption, the solid was separated by filtration, washed once with 50 mL of distilled water, and finally dried at 80 °C for 12 h. Under this condition,  $\text{l-}\alpha\text{-alanine}$  loading determined by formaldehyde titration was 5.0 wt.%.

### 2.2. $\text{SO}_2$ removal experiments

The  $\text{SO}_2$  removal experiments were performed in a glass-made jacketed fixed-bed reactor with 8 mm inside diameter, under isothermal conditions at required temperature. Approximately 0.3 g adsorbents were placed in the reactor to remove  $\text{SO}_2$  from simulated flue gas. The simulated flue gas was a mixture of  $\text{N}_2$ ,  $\text{O}_2$  and  $\text{SO}_2$  with the suitable concentration. Various simulated flue gas were introduced into the reactor after adding water vapor into the gas stream. Water vapor required for  $\text{SO}_2$  removal was generated in a pressure-controlled boiler made of stainless steel and equipped with electric heating coils. The steam lines were insulated with heating belt to prevent condensation within the line and keep the temperature. For comparison, experiments were also carried out using dry simulated flue gas without adding water vapor. The flow rate of the mixture gas was kept at 15 mL/min. The  $\text{SO}_2$  concentration changes at the outlet of the reactor were determined by iodine titration method (HJ/T 56-2000, a standard method of State Environmental Protection Administration of China). The amount of  $\text{SO}_2$  adsorption capacity is expressed as milligram  $\text{SO}_2$  per gram adsorbent (mg/g).

After saturation adsorption, the mixture gas was switched to  $\text{N}_2$  and the temperature increased to 120 °C at a rate of 20 °C/min. The adsorbent was regenerated in the reactor under an  $\text{N}_2$  flow at 120 °C until  $\text{SO}_2$  in vent was not determined. The  $\text{SO}_2$  concentration at outlet of the reactor was also determined by iodine titration method. The amount of desorbed  $\text{SO}_2$  is also expressed as milligram  $\text{SO}_2$  per gram adsorbent.

### 2.3. Specific Brunauer–Emmett–Teller (BET) surface areas

Specific surface areas of different adsorbents were calculated from nitrogen adsorption isotherms recorded at the temperature of liquid nitrogen on a Micromeritics Model ASAP 2000 (USA) using the Brunauer–Emmett–Teller (BET) equation.

### 2.4. Raman characterization

Confocal Raman microspectroscopy was conducted at room temperature with Renishaw UV–Vis Raman 1000 System, equipped with a CCD (charge couple device) detector and a Leica DMLM microscope. The line at 514.5 nm of an  $\text{Ar}^+$  laser was used for excitation. The laser power was reduced to  $\sim 1.0$  mW to ensure that the sample is not damaged by laser irradiation.

### 2.5. X-ray photoelectron spectroscopy (XPS) analysis

So as to analyze the S species that are strongly adsorbed on the adsorbents, electronic binding energies for S2p peaks of  $\text{l-}\alpha\text{-alanine}/\gamma\text{-Al}_2\text{O}_3$  after desorbing  $\text{SO}_2$  were measured by an X-ray photoelectron spectrometer. XPS analysis was performed on a PHI Quantum 2000 Scanning ESCA Microprobe with a monochromatized microfocused Al X-ray source. The binding energy was calibrated by C1s as reference energy (C1s = 284.6 eV).

## 3. Results and discussion

### 3.1. Activity of $\text{l-}\alpha\text{-alanine}/\gamma\text{-Al}_2\text{O}_3$ on $\text{SO}_2$ removal

Fig. 1 illustrates the activity of  $\text{l-}\alpha\text{-alanine}/\gamma\text{-Al}_2\text{O}_3$  on  $\text{SO}_2$  removal at 30 °C.  $\text{l-}\alpha\text{-alanine}$  crystal exhibited very low activity on  $\text{SO}_2$  removal, that is,  $\text{SO}_2$  saturation capacity was only 6.7 mg/g. However,  $\text{SO}_2$  saturation capacity increased about 8.5 times (57.2/6.7) when  $\text{l-}\alpha\text{-alanine}$  was supported on  $\gamma\text{-Al}_2\text{O}_3$ , and compared with  $\gamma\text{-Al}_2\text{O}_3$ ,  $\text{SO}_2$  saturation capacity increased about 2.4 times (57.2/23.4). This indicated that the activity of  $\text{l-}\alpha\text{-alanine}$  on  $\text{SO}_2$  removal increased significantly when supported on  $\gamma\text{-Al}_2\text{O}_3$ . Table 1 gives the pore characteristics of different adsorbents, which could explain the phenomenon. The very low activity on  $\text{SO}_2$  removal by  $\text{l-}\alpha\text{-alanine}$  crystal may be due to the much low specific surface area (only about 0.5  $\text{m}^2/\text{g}$ ). However, the specific surface area of the adsorbents increased about 260 times when  $\text{l-}\alpha\text{-alanine}$  was supported on  $\gamma\text{-Al}_2\text{O}_3$ . This could have greatly promoted the adsorption of  $\text{SO}_2$  and caused a significant increase in  $\text{SO}_2$  saturation capacity.

### 3.2. Effects of $\text{SO}_2$ concentration on $\text{SO}_2$ removal

Fig. 2 shows the effects of  $\text{SO}_2$  concentration on  $\text{SO}_2$  removal by  $\text{l-}\alpha\text{-alanine}/\gamma\text{-Al}_2\text{O}_3$  at 30 °C. The breakthrough time shortened with the increasing  $\text{SO}_2$  concentration, and the breakthrough times were no more than one hour when  $\text{SO}_2$  concentration was between 0.5% and 4.2%. This indicated the  $\text{SO}_2$  adsorption rate was relatively fast.  $\text{SO}_2$  saturation capacity increased with the increasing  $\text{SO}_2$  concentration, however, the saturation capacity kept stable at about 57 mg/g when  $\text{SO}_2$  concentration exceeded 1.7%.  $\text{SO}_2$  saturation capacity could still maintain at about 40 mg/g when  $\text{SO}_2$  concentration decreased to 0.5%, meaning that  $\text{l-}\alpha\text{-alanine}/\gamma\text{-Al}_2\text{O}_3$  could also be used to remove  $\text{SO}_2$  under relatively low  $\text{SO}_2$  concentration. The effects of  $\text{SO}_2$  concentration on  $\text{SO}_2$  removal may be due to dynamics and thermodynamics, that is, the concentration gradient between  $\text{SO}_2$  and the adsorbents increased with the increasing  $\text{SO}_2$

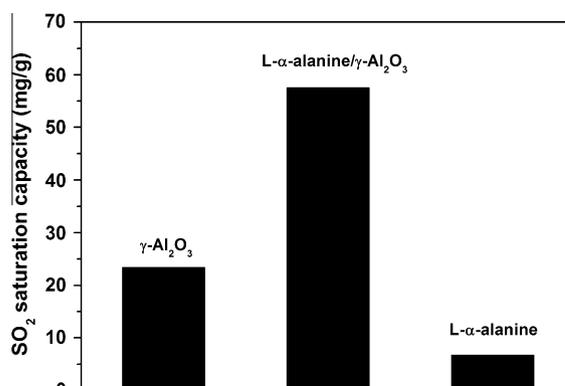


Fig. 1. Activity of  $\text{l-}\alpha\text{-alanine}/\gamma\text{-Al}_2\text{O}_3$  on  $\text{SO}_2$  removal at 30 °C gas composition (vol.%): 1.7%  $\text{SO}_2$ ; 5.0%  $\text{O}_2$ ; 20% water vapor; balance gas:  $\text{N}_2$ .

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