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# Modeling, thermodynamic and techno-economic analysis of coal-to-liquids process with different entrained flow coal gasifiers



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#### HIGHLIGHTS

• Modeling of coal-to-liquids (CTL) process with different entrained flow gasifiers was conducted.

• Thermodynamic analysis of CTL process was presented.

• Locations and magnitudes of exergy inefficiencies were identified and quantified.

• Techno-economic and CO<sub>2</sub> emissions analysis of CTL process were conducted.

#### ARTICLE INFO

Keywords: Coal-to-liquids (CTL) process Coal gasification Process simulation Thermodynamic analysis Techno-economic analysis Fischer-Tropsch (FT) synthesis

#### ABSTRACT

For the coal-to-liquids (CTL) plant, the most important unit is gasification, which determines the composition of the crude syngas, and affects  $CO_2$  emissions and investment of the CTL process. This paper conducts a detailed plant-wide modeling of CTL process with different entrained flow gasifiers. The model is compared with the literature data. Three cases of CTL process with different entrained flow gasifiers (GSP, Shell and Texaco) are researched through thermodynamic, techno-economic and  $CO_2$  emissions analysis. Case GSP represents the CTL process with GSP gasifier, Case Shell represents that with Shell gasifier, and Case Texaco represents that with Texaco gasifier. For a typical CTL process, Case GSP can produce FT liquids of 277.49 t/h, Case Shell can produce 246.25 t/h, and Case Texaco can provide 232.93 t/h. The energy efficiencies of Case GSP, Shell and Texaco are 50.85%, 48.18% and 41.09%, respectively. The exergy efficiencies are 49.89%, 47.20% and 40.44%, respectively. The exergy inefficiencies of the subsystem are quantified. The economic performance and  $CO_2$  emissions of the three cases are also discussed.

#### 1. Introduction

The energy reserve in China is rich in coal, while scarcity in oil and gas. The proven reserves of coal in China are  $114.5 \times 10^9$  t, and in 2015 the percentages of energy production from coal, oil, and natural gas are 78.2%, 9.2%, and 5.3%, respectively [1]. In a long time, coal will be the dominant energy resource in China. As shown in Fig. 1, the consumption of gasoline and diesel in China has been growing rapidly [1]. The oil consumption is kept increasing, and more than half of oil is imported from abroad, so the development of alternative energy resources is required. The coal-to-liquids (CTL) process can produce diesel and gasoline from coal. The capacity of the biggest CTL plant is 4.0 Mt/y oil in

China [2], and the total capacity will grow continuously to 13 Mt/y by 2020 [3].

Gasifiers vary in cold gas efficiency, cost, processing capacity and adaptability of coal type, and this makes a big difference in the whole CTL process. There are mainly three types of gasifiers based on the solid feedstock movement, i.e., fixed bed, fluidized bed and entrained flow gasifiers. For the entrained flow gasifiers, there are two feeding options, slurry feeding and dry feeding. Recent studies on the CTL process with different gasifiers is shown in Table 1. Various of gasifiers are used (Shell, Texaco, BGL, etc.), and most studies focus on the plant configuration (liquid-only or co-production [4–8]), the integration with CCS [4–13] and hybrid feedstock (coal/biomass/natural gas [9–11,14–23]).

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AGR

ASU

ATR

BEOP

BFW

BOI

BOP

BTL.

CBGTL

CBTL

CCP

CCS

CoP

CTL. EG

FCI

FG

FT

FTI.

GT GTL

HP

IP

LFG

LHV

LRC

LTFT

MHX

O&M

OTL

PSA

sf

ST

STL

SWS

SCOT

Siemens-GSP GSP

NG

MDEA

LP

HRSG

LACCR

CEPCI CG

## Nomenclature

#### Abbreviations

light fuel gas

low pressure

low-rank coal

natural gas

lower heating values

low-temperature FT

methyldiethanolamine

operating and maintenance

pressure swing adsorption

Shell Claus off-gas treating

main heat exchanger

oil-to-liquid fuels

the scale factor

shale-to-liquids

sour water stripper

steam turbine

**GE-Texaco** Texaco

lature	<i>TCI</i> WGS	total capital investment water gas shift
ions	WUS	wastewater treatment
acid gas removal	Notations	
air separation unit		
autothermal reformer	a, b, c, d	the coefficients of specif
break-even oil price	С	cost
boiler feed water	$c_{ m p}$	the specific heat capacity
balance of indirect costs	$d_{\rm p}$	the diameter of the coal
balance of plant costs	$\dot{E_x}$	Exergy (kJ/kg)
biomass-to-liquids	H	Enthalpy (kJ/kg)
coal, biomass, and natural gas to liquids	n	the number of carbon ato
coal biomass to liquids	Р	Pressure (kPa)
combined cycle power plant	S	Entropy (kJ/kgK)
$CO_2$ capture and storage	$S_1, S_2$	the production capacity
Chemical Engineering Plant Cost Index		planning project
coal gasification	Т	Temperature (K)
ConocoPhillips	t <sub>n</sub>	number of trains
coal-to-liquids	x <sub>i</sub>	the mass fraction of com
ethylene glycol	Y	yield
fixed capital investment	$y_{ ext{ineff}}$	the ratio of the exergy inefficiencies
fuel gas	Z	the coefficient which de
Fischer-Tropsch	L	and CO <sub>2</sub>
FT liquids co Texaco	[CO]	the concentration of CO
gas turbine	[CO <sub>2</sub> ]	the concentration of CO
natural gas to liquids		
high pressure	Greek syn	10015
heat recovery steam generator		average officiency (0/)
intermediate pressure	$\eta_{\mathbf{x}}$	exergy efficiency (%)

TCI	total capital investment
WGS	water gas shift
WWT	wastewater treatment
Notations	
a, b, c, d	the coefficients of specific heat capacity
С	cost
cp	the specific heat capacity (kJ/kgK)
$d_{ m p}$	the diameter of the coal particle
$E_{\mathbf{x}}$	Exergy (kJ/kg)
Η	Enthalpy (kJ/kg)
n	the number of carbon atoms in the hydrocarbon molecules
Р	Pressure (kPa)
S	Entropy (kJ/kgK)
$S_1, S_2$	the production capacity of the benchmark project and the
	planning project
Т	Temperature (K)
t <sub>n</sub>	number of trains
x <sub>i</sub>	the mass fraction of component i
Y	yield
$y_{\text{ineff}}$	the ratio of the exergy inefficiencies to the total exergy inefficiencies
Ζ	the coefficient which depends on the concentration of CO and $CO_2$
[CO]	the concentration of CO
[CO <sub>2</sub> ]	the concentration of $CO_2$
Greek sym	ıbols
$\eta_{\mathbf{x}}$	exergy efficiency (%)
Φ	the coefficient which depends on the diameter of the coal
	particle
Subscripts	and superscripts
	······ 1 ···· 1 ···
0	reference state
0 daf	
	reference state
daf	reference state dry, ash free
daf dev	reference state dry, ash free devolatilization
daf dev e	reference state dry, ash free devolatilization electricity
daf dev e ex	reference state dry, ash free devolatilization electricity exergy
daf dev e ex in	reference state dry, ash free devolatilization electricity exergy input
daf dev e ex in ind	reference state dry, ash free devolatilization electricity exergy input indirect
daf dev e ex in ind ineff	reference state dry, ash free devolatilization electricity exergy input indirect exergy inefficiencies
daf dev e ex in ind ineff out	reference state dry, ash free devolatilization electricity exergy input indirect exergy inefficiencies output
daf dev e ex in ind ineff out ph	reference state dry, ash free devolatilization electricity exergy input indirect exergy inefficiencies output physical

Only a few authors considered the effect of gasifier type. The CTL plants in China mainly use three types of gasifiers, i.e., slurry gasifiers, dry powder gasifiers, and fixed bed gasifiers [24]. As the entrained flow gasifiers have four main advantages: (1) the ability to utilize any type of coal, (2) high coal throughput capacity particularly at high pressures, (3) product gas is free of tars, and (4) high carbon utilization due to high reaction rates, this study focuses on the entrained flow gasifiers, and three types of entrained flow gasifiers (GSP, Shell and Texaco) are systematically investigated to assess their performance in the CTL process.

the levelized annual capital charge rate

Exergy is defined as the maximum theoretical work obtainable from a system compared with the ambient environment. It is used to assess thermodynamic inefficiencies in the system by considering the magnitudes, locations, and types of exergy inefficiencies [27]. The exergy

analysis methodology has been applied in the coal gasification (CG) [28–30], biomass gasification [31–36], CTL process [37], GTL process [38], and BTL process [39-42]. Gräbner and Meyer [28] evaluated the gasification processes in terms of cold gas efficiency, syngas yield and exergy efficiency. CoP and Shell exhibited the highest exergy efficiencies for Pittsburgh #8 coal while Siemens (GSP) offered the highest efficiency for the South African coal. Liszka et al. [29] proposed a hydrogen production process through co-gasification of biomass and coal with CO<sub>2</sub> capture. The overall exergy efficiency of the coal-to-hydrogen system was 57%, and the highest exergy losses took place in the gasifier. Seyitoglu et al. [30] studied an integrated coal gasification system for hydrogen production and power generation, and the overall energy and exergy efficiencies of the entire system was 41% and 36.5%, respectively. Ptasinski et al. [31] used idealized gasifier model to

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