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A feasible way to handle the heat management of direct carbon solid oxide fuel cells



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HIGHLIGHTS

- A novel system is proposed to handle the heat management of DC-SOFC.
- Three operation strategies are presented for different operation conditions.
- Power density and efficiency of the proposed system could reach 8100 W m^{-2} and 60%.
- Effects of some important parameters on system performance are revealed.

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ABSTRACT

A novel integrated system consisting of an external heat source, a direct carbon solid oxide fuel cell (DC-SOFC), a vacuum thermionic generator (VTIG) and a regenerator is proposed to handle the heat management of the DC-SOFC. The electrochemical/chemical reactions, ionic/electronic charge transport, mass/momentum transport and heat transfer are fully considered in the 2D tubular DC-SOFC model, which shows that the overall heat released in the cell is always different from the heat required by the internal Boudouard reaction. Three different operation strategies of the proposed system are presented, and accordingly, analytical expressions for the overall power output and efficiency for the proposed system are specified. The results show that the VTIG could effectively recover the waste heat for additional power production at a large operating current density, and the maximum power density and efficiency of the proposed system could reach more than 8100 W m⁻² and 60% at 30,000 A m⁻² and 1173 K, respectively. The effects of the operating current density, the operating temperature and work function of the VTIG on the performance of the proposed system are discussed through comprehensive parametric studies.

1. Introduction

Despite the tendency in decreasing the reliance on fossil fuels and the development of alternative renewable energy technologies due to energy crisis and relative environmental problems, solid carbon remains a main resource in the coming decades because of its abundant storage and low price [1]. However, the utilization of solid carbon in conventional thermal plants for electricity generation is low-efficient due to the limitation Carnot cycle and complex intermediate processes [2]. In addition, the pollution from thermal plants cause various environmental problems, *e.g.* acid rains and global warming. Therefore, an alternative high-efficient and clean energy conversion device for electricity generation from solid carbon is urgently needed, such as solid oxide fuel cells (SOFCs) [3,4].

An SOFC is a whole solid-state device with a dense electrolyte sandwiched between two porous electrodes. As one of the most attractive energy conversion devices, SOFCs can directly convert gaseous fuels, such as H_2 and CO, into electricity through electrochemical reactions. The fuel flexibility characteristic of SOFCs also allows the utilization of other fuels, such as methane and solid carbon [5,6]. Solid carbon is an attractive fuel since it has a high volumetric energy density compared with gaseous fuels. Moreover, solid carbon is cheap and abundant, bringing huge economic advantages in exploring new markets [7–9]. However, the large particle size of solid carbon limits its direct contact with the triple phase boundaries (TPBs) in porous anode, resulting in a low output power density of direct carbon solid oxide fuel

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Nomenclature Abbreviation DC-SOFC direct-carbon solid oxide fuel cell SOFC solid oxide fuel cell TPB triple phase boundary VTIG vacuum thermionic generator YS7 vttrium stabilized zirconium Roman plate area ratio between VTIG and DC-SOFC а effective area of DC-SOFC, m² A Richardson-Dushmann constant, A m⁻² K⁻² A_0 area of VTIG anode, m² A_a area of VTIG cathode, m² A_c permeability coefficient, m² B_0 molar concentration of carbon dioxide, mol·m⁻³ $c_{\rm CO_2}$ constant-pressure heat capacity, C_p D_i^{eff} effective diffusivity of species *i*, $m^2 \cdot s^{-1}$ charge of an electron, C е activation energy, J mol⁻¹ Eacv equilibrium potential, V Ε $E_{\rm CO}^0$ standard equilibrium potential for carbon monoxide oxidization, V equilibrium Nernst potential, V E_{eq} E_{rb} activation energy of Boudouard reaction, J·mol⁻¹ F Faraday constant, 96,485 C·mol⁻¹ i current density, A·m⁻² i_L lowest working current density for VTIG, A·m⁻² exchange current density, A·m⁻² i. thermal neutral current density, A·m⁻² i_{tn} electrical current, A Ι Ia reverse electric current from VTIG anode, A I_c reverse electric current from VTIG cathode, A net thermionic electric current in VTIG, A ITIG thermal neutral current, A Itn net thermionic electric current density of VTIG, A·m⁻² j_{tig} Boltzmann constant, J K⁻¹ k_b kinetic coefficient of Boudouard reaction, $\ensuremath{s^{-1}}$ k_{rb} number of electrons transferred per electrochemical ren action flux of mass transport, kg·m⁻³·s⁻¹ Ni (partial) pressure, Pa р local CO gas partial pressure, Pa $p_{\rm CO}^L$ local CO₂ gas partial pressure, Pa $p_{\rm CO_2}^{\,\scriptscriptstyle L}$ local O2 gas partial pressure, Pa $p_{O_2}^{L}$ Р electricity power output, W PSOFC electricity power output by DC-SOFC, W electricity power output by VTIG, W P_{TIG} electricity power density, W·m⁻² P^* maximum electricity power density of DC-SOFC, $W {\cdot}m^{-2}$ P_{max}^*

P [*] _{cond}	electricity power density of DC-SOFC. $W m^{-2}$	
P_{TIC}^*	electricity power density of VTIG. $W \cdot m^{-2}$	
Q	heat, W	
\tilde{O}_h	heat absorption by Boudouard reaction. W	
Q,	heat released by electrochemical reaction, W	
Q_{SOFC}	heat rejection of DC-SOFC	
R	gas constant, 8.314 J·mol ^{-1} ·K ^{-1}	
R_{rb}	reaction rate of Boudouard reaction, $mol \cdot m^{-3} \cdot s^{-1}$	
Т	operating temperature, K	
T_2	VTIG anode temperature, K	
u	velocity field, $m^{3} s^{-1}$	
U	output voltage of VTIG, V	
V	operating voltage, V	
y_i	molar fraction of component i	
Greek letters		
α	charge transfer coefficient	
$\beta_{\rm H2}$	electrochemical kinetics parameter for H ₂	
ε	porosity	
ε_0	effective thermal emissivity	
η	electrical efficiency	
η_{SOFC}	electrical efficiency of DC-SOFC	
η_{TIG}	electrical efficiency of VTIG	
η_{act}	activation polarization, V	
η_{ohmic}	Ohmic polarization, V	
κ	permeability, m ²	
λ	thermal conductivity, $W \cdot m^{-1} K^{-1}$	
λ_{eff}	effective thermal conductivity, $W \cdot m^{-1} K^{-1}$	
μ	dynamic viscosity of fluid, Pa·s	
ρ	fluid density, kg·m ^{−3}	
σ	Stefan-Boltzmann constant, W m ⁻² K ⁻⁴	
$\sigma^{e\!f\!f}$	effective conductivity, S m^{-1}	
τ	tortuosity	
Ø	potential, V	
Φ_a	work function of the VTIG anode, eV	
Φ_c	work function of the VTIG cathode, eV	
Subscripts		
1		

an	anode
ca	cathode
со	carbon monoxide
H_2	hydrogen
1	ionic phase
S	electronic phase
<i>Superscri</i> µ 0 eff L	parameter at equilibrium conditions effective local

cells (DC-SOFCs). To overcome this problem, *in situ* solid carbon gasification has been proposed. Through *in situ* gasification, solid carbon is converted to gaseous fuel (*e.g.* CO) before the electrochemical reaction, which keeps the high volumetric energy density of solid carbon and expands the electrochemical reaction area simultaneously. A number of studies have been conducted to further improve the performance of DC-SOFC by adopting catalysts for faster carbon gasification kinetics [10–13]. Moreover, it has been found that DC-SOFCs can co-generate fuel and electricity power, which further increases their economic advantage [14–18]. The thermal effect in DC-SOFC has been also studied

to examine its potential for combined heat, gaseous fuel and electricity power generation [19]. It was found that the DC-SOFC requires heat input at a small current density due to the endothermic carbon gasification reaction, while the cell releases waste heat at a large operating current density. Initial studies combining conventional Stirling cycle and Otto heat engine with the DC-SOFC for its performance improvement have been conducted [20,21]. However, a system combining DC-SOFC with more novel and advanced heat-to-electricity conversion device is still needed to examine the potential performance improvement. Download English Version:

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