Contents lists available at ScienceDirect

### Applied Energy

journal homepage: www.elsevier.com/locate/apenergy

# Technological improvements in energetic efficiency and sustainability in existing combined-cycle gas turbine (CCGT) power plants

Antonio Colmenar-Santos<sup>a,\*</sup>, David Gómez-Camazón<sup>a</sup>, Enrique Rosales-Asensio<sup>b</sup>, Jorge-Juan Blanes-Peiró<sup>c</sup>

<sup>a</sup> Department of Electric, Electronic, Control, Telematic and Chemical Applied to Engineering, Technical School of Industrial Engineering, UNED, Juan del Rosal, 12 Ciudad Universitaria, 28040 Madrid, Spain

<sup>b</sup> Departamento de Física, Universidad de La Laguna, Avenida Astrofísico Francisco Sánchez, S/N, 38206 S/C de Tenerife, Spain

<sup>c</sup> Departamento de Ingeniería Eléctrica y de Sistemas y Automática, Escuela Técnica Superior de Ingenieros de Minas de LEÓN, Spain

#### HIGHLIGHTS

- CCGT partially regenerative with solar hybridization maintences the global efficiency like CCGT.
- Recuperation effectiveness is fundamental factor calculation of the regenerator.
- Emissions-fuel consumption decrease considerably with partial regeneration.
- Thermal efficiency obtained in new CCGT hybridized is higher than conventional solar technology.

#### G R A P H I C A L A B S T R A C T



#### ARTICLE INFO

Keywords: Combined cycle Gas turbine Regenerator Efficiency analisys Solar hybridization

#### ABSTRACT

Data from an existing combined-cycle gas turbine (CCGT) power plant are used to create a computer simulation to allow efficiency and emission calculations, simulation and assessing improvements that apply partial regeneration with solar hybridization. The proposed amendments to this triple-pressure steam-reheat combined cycle (CCC<sub>3PR</sub>) with 400 MW of net power incorporates a regenerator and thermal energy, from a source of renewable solar energy up to 50 MW, in order to reduce the energy loss in the gas turbine. The calculation and simulation models were created using Visual Basic code. Regeneration and solar hybridization were found to contribute to increasing efficiencies of around 2.25% to 3.29% depending on the loading point. The reduction of gas consumption was between 6.25% and 9.45% and the overall cycle efficiency loss is minimal due to hybridization. There was a loss of the net power of the new cycle but it is considerably lower if than heat from a renewable source is supplied to the cycle. This net power loss has an average value of 7.5% with regeneration only and of 1% with regeneration and hybridization. The reduction of fuel consumption is significant which could result in saving approximately 4 million €/year. Partial regeneration in the gas turbine and solar thermal power in the existing CCGTs provide an interesting possibility for reducing emissions (by 26,167 t/year). In conclusion, partial regeneration with solar hybridization provides an interesting and proven possibility to increase performance and efficiency whilst reducing emissions from the existing CCC<sub>3PR</sub>.

\* Corresponding author. E-mail address: acolmenar@ieec.uned.es (A. Colmenar-Santos).

https://doi.org/10.1016/j.apenergy.2018.03.191

Received 23 August 2017; Received in revised form 30 March 2018; Accepted 31 March 2018 0306-2619/ © 2018 Elsevier Ltd. All rights reserved.







#### Applied Energy 223 (2018) 30-51

Nomenclature		$\eta_{\rm cc}$	efficiency combined cycle, %
Symbols		Subscripts and acronyms	
APP	approach point, –	а	air
BP	low pressure, –	amb	ambient conditions
c <sub>P</sub>	specific heat, kJ/(kg·K)	AP	high pressure level
с	cost, €	atm	atmospheric pressure
dT	temperature difference, K	BP	low pressure level
e	exergy, kJ/kg	CCC	Combined cycle power plant
h	enthalpy, kJ/kg	CCC <sub>3PR</sub>	triple pressure HRSG with reheating
HP	high pressure, –	CCC <sub>3PR, 1</sub>	reg CCC <sub>3PR</sub> with regenerator
L	irreversibility, W	CCC <sub>3PR, 1</sub>	reg&HS CCC <sub>3PR, reg</sub> with solar hibridization
LEC	levelized cost. €	CCP	Parabolic cylindrical collector
'n	mass flow, kg/s	CComb	combustion chamber
m.	mass flow rair. kg/s	Comp	compressor
m <sub>c</sub>	mass flow exhaust gases, kg/s	Cond.	condensator
<i>т</i> т	mass flow steam IP. kg/s	CN	carnot factor
m , , p	mass flow steam AP kg/s	DSG	direct steam generation
m <sub>v,AP</sub> ṁpp	mass flow steam RP kg/s	in	inlet
<i>т</i> .	mass flow reheater steam kg/s	ext	extraction steam turbine
m.	mass flow extraction steam kg/s	exh	exhaust gases
n extrac.	pressure har	ECO	economizer
P I HV	lower heating value kI/kg	EV	1 <sup>a</sup> combustor chamber GT
DD DD	ninch point K	EVA	evaporator
Ò_ases	mass flow exhaust gases, kg/s	f	fuel
r.	compression ratio. –	F	dosing
+c S	entrony kJ/(kg·K)	FW	feedwater
т	temperature K	gen	generator
TAT	after turbine temperature. K	G	gas
TIT <sub>up pp</sub>	inlet turbine temperature, k	GT	gas turbine
T , pp m	steam turbine temperature BD_ID_AD_K	GT26	gas turbine Alstom GT26
<sup>1</sup> sal, BP,IP, AT	terminal difference temperatures K	HTF	heat transfer fluid
11	internal energy k I/kg	HRSG	heat recovery steam generator
u II	hast transfer coefficient $(WW^{-1}m^{-2})$	IP	intermediate pressure level
	Hat-transfer Coefficient, (WK - III )	ISCC	integrated solar combined cycle
UЛ w	power W	I FR	linear fresnel reflectors
vv	power,w	out	
Crook latt	arc	P	
Creek letters		Rh	reheater
0	regunerative mass fraction	Ref	reference
u	effectiveness of the reconcreter	rog	regenerator
e v	enectiveness of the regenerator, –	reg	regeneration
n n	specific fleat felation, –	Sal	steam cycle
n	eniciency, %	CEV	2ª compustor chamber CT
n Ilis,C	isentropic efficiency compressor, %	SE V CLI	2- combustor chamber G1
n Im,C	mechanic efficiency compressor, %	ST ST	superiodici
n I Im,T	mechanic efficiency turbine, %	JI TO	steall tululle
I m,bombas	, mechanic emciency pumps, %	IQ Tum <sup>L</sup>	lallik turbing
I] <sub>is,GT</sub>	isentropic efficiency compressor, %	TUTD V	tui Dille
I I <sub>m,GT</sub>	mecnanic efficiency gas turbine, %	V	steam
I] <sub>is,TV</sub>	isentropic efficiency steam turbine, %	VGV	variable geometry blades
I] <sub>m,TV</sub>	mechanic efficiency steam turbine, %	U	reference conditions

#### 1. Introduction

In the search of an efficient, economical and environmentally friendly energy, there is a clear shift towards renewable energy sources and decreasing emissions. This is an on-going process and the final solution has clearly not yet been reached [1,2].

Present day operating conditions of Combined-Cycle Gas Turbine (CCGT) power plants differ from the base load design conditions (approximately 400 MW), and therefore require performance studies and technological improvements at loading points others than the base load. This research considers practical improvements that can be made inside

the existing CCGT plants operating in Spain and how these improvements can be implemented on the system operation conditions achieving emissions and fuel consumptions reductions and improving the system global efficiency. These changes will be in-line with Horizon 2020 directive [1–3]. It is necessary to include novelty improvements to give a response to these clean energy needs inside the existing CCGTs. In this aspect, the improvement of partial regeneration in gas turbine is possible. It is vital to advance research and development projects that deal with the emerging technologies that are needed to achieve these goals. Solar energy is another alternative, because it presents a great number of advanced technological options, such as the solar thermal Download English Version:

## https://daneshyari.com/en/article/6680029

Download Persian Version:

https://daneshyari.com/article/6680029

Daneshyari.com