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# Applied Energy

journal homepage: www.elsevier.com/locate/apenergy

# Optimization and multi-time scale modeling of pilot solar driven polygeneration system based on organic Rankine cycle

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## HIGHLIGHTS

- The field test of pilot distributed solar driven ORC-based CCHP system is presented.
- A multi-time scale simulation mechanism is developed.
- The objective and functionality of each time-scale simulation with appropriate time step is identified.
- A model-guided optimized system is achieved with sequential configuration.

### ARTICLE INFO

Keywords: Combined cooling, heating, and power Organic Rankine cycle Pilot system Solar thermal energy Simulation Time scale

### ABSTRACT

Pilot-scale distributed polygeneration system driven by solar energy and its effective simulation mechanism provides promising solutions for the technology promotion and implementation, as the emerging of smart grid concepts. In this regard, this study aims to preliminary test such a system based on organic Rankine cycle with the power output of 200 kW, which is combined with cooling and heating cycle. The developed pilot system is proven to sustain the power thermal efficiency of 10% with R123 and a self-made expansion valve. Targeting a whole optimized system in practical application, a multi-time scale mechanism is proposed and consists of long-, mid- and short-term simulation with yearly, hourly and second time step, respectively. The functionality of the concept is proven by showing the model-guided optimal sequential system with hexamethyldisiloxane working fluid. It achieves a high performance ratio, efficient cost, and less land occupation, corresponding to 67.61%, \$0.12 million and 3774.2 m<sup>2</sup>, respectively, under the long-term simulation. Rated operation decisions are correspondingly determined and present acceptable supply-and-demand matching performance at the level of midterm modeling, with the payback time of 7.41 years. Furthermore, the system dynamic behavior is analyzed in two typical sunny and cloudy days to understand and compare its running states. The short-term model shows a steady thermal efficiency of 9.6% within 15,000 s and capture a smaller period of safety state only within 6000 s under the sunny day condition. Although the peak irradiance in the cloudy day is higher than that in the sunny day, the performance degrades dramatically due to the irradiance fluctuation. It is expected that the proposed mechanism can be extended in analyzing operational security and control strategy.

### 1. Introduction

Due to the increasing global demand for energy, as well as the strict emissions targets, popularization and application of renewable energy systems is an urgent goal for all over the world to pursue. According to Renewable Energy Policy Network for the 21st Century, new investment in renewable energy from 2015 to 2016 continued to be dominated by solar, which accounted for roughly 47% of total investments in 2016 [1]. Its strong growth gave a clear indication of accounting for all of the increase in global renewable energy penetration, with solar technology as the backbone of the highly decarbonized energy system. China proposes an ambitious renewable penetration objective in 2050 with over 60% of China's total energy consumption and with 2700 GW solar units [2]. To access this goal, a first batch of concentrated solar power (CSP) demonstration projects have been officially released with an installed capacity of 1.35 GW, constituting 64% among the total CSP in the world. However, these projects locate in the sparsely populated western region of China with rich radiation resources, and commonly belong to centralized power generation system.

As the emerging of smart grid concept, societal-scale infrastructures such as eco-industrial parks [3] and smart buildings are rapidly expanded [4]. For such infrastructures, diversification of energy products

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https://doi.org/10.1016/j.apenergy.2018.03.118







Received 31 December 2017; Received in revised form 11 March 2018; Accepted 27 March 2018 0306-2619/ © 2018 Elsevier Ltd. All rights reserved.

Nomenclature q			the index for each objective, –
		$\dot{q}_i''$	net heat flux per unit area, W/m <sup>2</sup>
Acronym	S	$R_k$	net cash inflow during period k, \$
		R	coefficient, –
ACH	absorption chiller	S(t)	energy storage balance, kWh
CCP	combined cooling and heating	t	time, s
CCHP	combined cooling, heating and power	Т	temperature. °C
CHP	combined cooling and heating	$\frac{1}{T}$	average temperature
Cond OI		1	tomporature difference °C
Cond_Or			intermed an energy L
CPC	compound parabolic collector	U	internal energy, J
EIC	evacuated tube collector	$U_0$	overall heat transfer coefficient, W/m <sup>2</sup> . <sup>o</sup> C
HS	heating storage	$U_L^{ m abs}$	thermal loss coefficient of absorber, –
e-CPS	energy-cyber-physical	ν	specific volume, m <sup>3</sup> /kg
ICE	internal-combustion engine	$v_{\rm bf}$	bulk fluid velocity, m/s
NPV	net present value	V	volume, m <sup>3</sup>
PTC	parabolic trough collector	<i></i>	volumetric flow, m <sup>3</sup> /s
DBT	payhack time	, Ŵ	power kW
		**	power, kw
P_011		X	axiai distance, in
P_ORC	working fluid pump		
PS	parallel system	Greek symbols	
SS	sequential system		
VG	vapor generator	α	heating price and electricity price ratio
WHR	waste heat recovery	β	cooling price and electricity price ratio
	made near recovery	, F	effectiveness
Symbole		c	numn internal isontronic officiency
Synwois		<sup>c</sup> over,pp	officiency
	2	η	eniciency
Α	area, m <sup>2</sup>	ρ	density, kg/m <sup>°</sup>
$A_i$	circumferential area of segment "i", m <sup>2</sup>	$\overline{\rho_i}$	fluid density of fluid in each heat exchanger segments, kg/
а	coefficient, –		m <sup>3</sup>
Ь	coefficient, –	$\varphi$	incident angle, –
с	specific heat capacity, J/kg	φ	level fraction
C	geometric concentration ratio –	Λ	difference
cor	corrected	2	thermal conductivity
01	diameter, -	<i>n</i>	load cover factor
D	diameter, m	Ŷ	Ioau cover factor
$d_i$	inner diameter of tubes, m		
$d_o$	outer diameter of tubes, m	Subscripts	S
des	design condition		
Ε	total energy in volume, J	а	aperture of PTC
F	objective, –	abs	absorber of PTC
E.	dirt degree of collector's mirrors. –	cd	condenser
FF	filling factor _	em	electromechanical
C II	$M_{m}^{2}$	exp	expender
GP CT	solar infaulance, w/m	ov	avbaust or outlat
GI	gas turdine	ex	
g(t)	generated energy, kWh	eva	evaporator
h	specific enthalpy, J/kg	t	fluid
$h_i$	specific enthalpy of fluid in each heat exchanger segment,	HE	heat exchanger
	J/kg	heat_sur	surplus heat from condenser
hr	hour. –	hf	hot fluid
i	the number of points on the Pareto frontier –	hs	heat source
L	hourly solar beam radiation $W/m^2$	i	inside fluid of HE
	investment cost ¢	id	inside dirt of HE
IC II	investment cost, \$	in	internal
K	incident angle modifier, –	· ·	
k	the order of each variable	inc	state energy incentives
l(t)	load, kWh	1	liquid
M	total mass in volume, kg	lm	logarithm mean
$M_i$	the mass of fluid in each heat exchanger segment, kg	max	the maximum
<i>m</i>	mass flow rate, kg/s	mech	mechanical
N	the number of segments	net	gross mechanical output
n .	rotate speed	opt 0°	collector's optical efficiency for zero incident angle
IL N	rotation append, -	0	outside fluid of HE
N <sub>rot</sub>	rotating speed, rpm	o d	outside dist
Р	pressure, Pa	ua	
р	the index for each point on the Pareto front, -	pin	pinch point
PR	overall efficiency of solar energy, -	pp	pump
Ż	heat power, W	ref	reference
$\overline{\dot{Q}_i}$	heat power of fluid in each segment, W	S	swept

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