



# The separation of CO<sub>2</sub> from ambient air – A techno-economic assessment

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## HIGHLIGHTS

- Amines/imines are most promising adsorbing agents to separate CO<sub>2</sub> from ambient air.
- Energy demand results in 3.65 GJ/t<sub>CO2</sub> and a second law efficiency of up to 11.83%
- Costs of avoiding CO<sub>2</sub> emissions range from \$ 824 (wind)-1333/t<sub>CO2</sub> (natural gas)
- CO<sub>2</sub> separation from air is unable to economically compete with CCS.
- Separation from air will not play a vital role in the abatement of the CO<sub>2</sub> problem.

## ARTICLE INFO

### Keywords:

CO<sub>2</sub> separation from the atmosphere  
Techno-economic analysis  
Climate change  
Carbon capture and storage  
CO<sub>2</sub> abatement costs  
Polyethyleneimine adsorption

## ABSTRACT

This paper assesses the separation of CO<sub>2</sub> from ambient air from a technical and economic standpoint. Reducing CO<sub>2</sub> emissions and their sequestration from the atmosphere is vital to counteract ongoing climate change. The most promising technological options for CO<sub>2</sub> separation are first identified by reviewing the literature and comparing the most important technical and economic parameters. The results point to amines/imines as adsorbing agents to separate CO<sub>2</sub> from ambient air. A system layout is then designed and a technical analysis conducted by solving mass and energy balances for each component. An economic analysis is then performed by applying a specifically-developed model. The total energy demand of the system discussed here is calculated as 3.65 GJ/t<sub>CO2</sub>. This high energy demand mainly derives from the system-specific implementation of two compressors that compress air/CO<sub>2</sub> and overcome the pressure losses. The second-law efficiency calculated ranges of 7.52–11.83 %, depending on the option of heat integration. The costs of avoiding CO<sub>2</sub> emissions vary between \$ 824 and 1333/t<sub>CO2</sub>, depending on the energy source applied. The results of this work present higher values for energy demand and costs compared to other values stated in literature. The reasons for this deviation are often insufficient and overoptimistic assumptions in other literature on the one hand, but also relate to the specific system design investigated in this paper on the other. Further case studies reveal that enormous land requirements and investments would be needed to reduce potential CO<sub>2</sub> quantities in the atmosphere to contemporary levels. A comparison between CO<sub>2</sub> removal from the atmosphere and carbon capture and storage technology for coal power plants shows that this technology is not yet able to economically compete with carbon capture and storage. Furthermore, the impact of CO<sub>2</sub> separation on the production costs of industrial commodities like cement and steel demonstrates that CO<sub>2</sub> removal from the atmosphere is not yet a viable alternative to solving the climate change problem. In the long-term, CO<sub>2</sub> separation from ambient air may still play an important role in the sequestration of CO<sub>2</sub> from diluted and dispersed sources, as the technology has the potential for significant further development and optimization.

## 1. Introduction

Climate change is an all-encompassing challenge facing humanity. The consequences of climate change include, amongst other things, an increase in mean temperature and sea level, the frequent occurrence of

extreme weather events, changes in biodiversity and oceanic acidification. Climate change is result of the greenhouse effect: short-wavelength solar radiation enters the Earth's atmosphere and is partly reflected by surface. As the temperature of the radiation drops on its journey from the Sun to the Earth, its wavelength increases. The

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**Nomenclature***List of abbreviations*

CCS	carbon capture and storage
CCUS	carbon capture, utilization and storage
CNG	compressed natural gas
DNI	direct normal irradiation
LNG	liquid natural gas
MEA	monoethanolamine
PEI	polyethyleneimine
PtG	power-to-gas
PtL	power-to-liquids
PtX	power-to-x

*List of symbols*

$\Delta$	delta [–]
$A$	surface [m <sup>2</sup> ]
$A$	annuity [\$/a]
$B_1, B_2$	coefficients to account for additional costs [–]
$c_p$	specific heat capacity [J/mol/K]
$c_A$	abatement costs [\$/t <sub>CO2</sub> ]
$C_B$	utilities costs [\$/a]
$c_{PC}$	specific production costs [\$/t <sub>CO2</sub> ]
$C_{BM}$	component costs [\$/a] (for components that are not made of carbon steel for an operating pressure of 1 bar)
$C_{BM}^0$	component costs [\$/a] (for components that are made of carbon steel for an operating pressure of 1 bar)
$C_F$	manufacturing costs [\$/a]
$C_G$	overhead costs [\$/a]
$C_H$	auxiliaries costs [\$/a]
$C_L$	laboratory costs [\$/a]
$C_M$	material costs [\$/a]
$C_p$	staff manufacture costs [\$/a]
$C_p^0$	acquisition costs [\$/a]
$C_{PC}$	production costs [\$/a]
$C_R$	commodities costs [\$/a]
$C_{SV}$	taxes and insurances costs [\$/a]
$C_{UB}$	supervision and bureau staff costs [\$/a]
$C_W$	maintenance costs [\$/a]
$F_{CI}$	investment costs [\$/a]
$F_M, F_P, F_{BM}$	coefficients to account for additional costs [–]
$g$	specific Gibbs energy [J/mol]
$\Delta h_R$	specific enthalpy of reaction [J/mol]
$\dot{H}$	enthalpy flow [W]
$i$	interest rate [%]
$I_{2001}, I_{2012}$	Chemical Engineering Cost Plant Index for 2001 and 2012 [–]
$k$	heat transmission coefficient [W/m <sup>2</sup> /K]
$K_1, K_2, K_3$	component specific coefficients [–]
$m$	mass [kg]
$\dot{m}$	mass flow rate [kg/s]
$n$	polytropic exponent [–]
$\dot{n}$	molar flow rate [mol/s]

$p$	pressure [Pa]
$q$	thermal work [J/mol]
$r$	reaction rate [mol/m <sup>3</sup> /s]
$R$	ideal gas constant ( $R = 8.314$ J/mol/K)
$t$	deduction period [a]
$T$	temperature [°C or K]
$V$	volume [m <sup>3</sup> ]
$w$	specific work [J/mol]
$x$	sorbent loading [mmol/g]
$X$	sorbent working capacity [%]
$y_i$	concentration of component in the gas phase [–]
$z_i$	concentration of component in the liquid phase [–]
$Z$	capacity coefficient [–]
$\eta$	efficiency [–]
$\theta$	ratio of heat recovery [–]
$\tau$	abatement factor [–]
$\nu$	stoichiometric coefficient [–]

*List of indices*

0	standard conditions (1013 hPa, 0 °C)
<i>ads</i>	adsorption
<i>cond</i>	condensation
<i>CO2</i>	carbon dioxide
<i>C2H4</i>	ethylene
<i>des</i>	desorption
<i>el</i>	electric
<i>em</i>	emitted
<i>evap</i>	evaporation
<i>F</i>	fluid
<i>g</i>	gas phase
<i>H2O</i>	water/water vapor
<i>HE</i>	heat exchange
<i>i</i>	component i
<i>in</i>	inlet
<i>j</i>	variable j
<i>k</i>	count variable k
<i>l</i>	liquid phase
<i>min</i>	minimal
<i>NG</i>	natural gas
<i>out</i>	outlet
<i>poly</i>	polytropic
<i>product</i>	product
<i>PEI</i>	polyethyleneimine
<i>rev</i>	reversible
<i>s</i>	saturation
<i>sep</i>	separated
<i>sorbent</i>	sorbent
<i>system</i>	system
<i>t</i>	technical
<i>th</i>	thermal
<i>waste</i>	wasted
<i>W</i>	wall

infrared radiation reflected from the Earth's surface cannot completely pass through the "climate gas layer" in the troposphere, and so is reflected back to the Earth [1,2]. Therefore, the terrestrial temperature increases. The "climate gas layer" consists of water vapor as well as CO<sub>2</sub>, methane and nitrous oxide etc. Alongside natural emissions of these climate gases, anthropogenic emissions have led to increased amounts of these gases in the troposphere, which are the highest in at least the last 800000 years [3]. Current measurements show

approximately 1800 ppb of methane, 320 ppb of nitrous oxide and 407 ppm of CO<sub>2</sub> [3,4]. Although CO<sub>2</sub> has a global warming potential that is about 1/21 that of methane and about 1/310 that of nitrous oxide over 100 years [5], CO<sub>2</sub>, with a current anthropogenic emission of about 38 Gt/a [3], is responsible for about 60% of anthropogenic climate change [6]. As forecast in Pham et al. [6], a CO<sub>2</sub> concentration of 570 ppm can be expected by 2100 as a result of population growth and improving economic conditions. As approximately 1000 ppm could be

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