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Performance analysis of internal-combustion-engine primed trigeneration systems for use in high-rise office buildings in Hong Kong $^{\diamond}$

K.F. Fong, C.K. Lee*

Division of Building Science and Technology, College of Science and Engineering, City University of Hong Kong, Tat Chee Avenue, Hong Kong

HIGHLIGHTS

- Internal-combustion-engine-primed trigeneration (ICEPT) systems were analyzed.
- Three types of fuels, namely diesel oil, natural gas and petrol gas, were considered.
- Dynamic performances studied for use in high-rise office building in Hong Kong.
- Diesel-oil-fueled system yielded the largest primary energy saving.
- Natural-gas-fueled one offered the lowest carbon dioxide emission.

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ABSTRACT

The energy and environmental merits of three types of internal-combustion-engine primed trigeneration (ICEPT) systems were investigated when compared with a conventional chilled water system powered by the grid electricity for use in a high-rise office building in Hong Kong. With the employment of the ICEPT systems, the year-round total electricity demand from the building was reduced by at most 10.4% for the natural-gas-fueled one. However, the saving in the total primary energy consumption (*PEC*) only ranged from 1.7% to 6.8% with the diesel-oil-fueled system being the best although for all the three types of ICEPT systems more than 70% of the energy from the fuel had been utilized. The huge difference in the coefficient of performance (*COP*) between the absorption chiller and the vapor-compression chiller was the main cause which impaired the benefit of recovering the waste heat to provide space cooling. The total carbon dioxide emission (*CDE*) varied widely with the types of fuels adopted with a maximum of 26.7% for the natural-gas-fueled system which was due to the lower carbon dioxide emission index of natural gas as compared to other fuel types. The overall ranking of the ICEPT systems depended on the weighing between energy and environmental merits.

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1. Introduction

With the increasing awareness on climate change, the urge for the reduction in carbon dioxide emission has become a major mission of the government in the developed country. One possible direction is the employment of more renewable energy sources such as solar, wind, tidal and geothermal in place of the conventional power plants which run on fossil fuels. However, the high initial cost of the renewable energy systems is the main obstacle. Another feasible way is to optimize the use of energy delivered

* Corresponding author.

E-mail address: a8304506@graduate.hku.hk (C.K. Lee).

http://dx.doi.org/10.1016/j.apenergy.2014.11.059 0306-2619/© 2014 Elsevier Ltd. All rights reserved. from the fossil fuels by designing more energy-efficient power systems. This can be achieved by utilizing the waste heat from the power systems for heating and/or spacing cooling of buildings through the use of heat-driven air-conditioning equipment, thus forming a trigeneration system. Fig. 1 shows the symbolic diagram of a trigeneration system. Fuel is supplied to a prime mover for generating electricity. Meanwhile, the waste heat delivered from the prime mover is recovered to provide space cooling and/or heating. With this design, usually more than 70% of the energy released from the fuels can be utilized.

Different kinds of prime movers may be used which include internal combustion engine, gas turbine, steam turbine, micro turbine and fuel cell. Studies have been made to investigate the thermodynamic performances of various designs of trigeneration systems [1-15] which mainly focus on the behavior of the trigeneration systems at different operating conditions. However, the

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Nomenclature

Α	area (m ²)	f	fuel
CDE	carbon dioxide emission (ton)	i	inlet
СОР	coefficient of performance	iw	iacket water
Cn	specific heat at constant pressure (kl/kg K)	0	outlet
ÉUF	energy utilization factor		
GEE	generator electrical efficiency	Abbraviations	
H	enthalpy (kI)	Abov	absorption shiller control valvo
I HV¢	lower heat value of fuel (kI/kg)		absorption chiller cooling water nump
m h	mass flow rate (kg/s)	ADCWF	absorption chiller primary chilled water pump
P	pressure (kPa)	ADPCIIVP	absorption chiller printary chilled water pump
PEC	primary energy consumption (MW h)	ADSCIIVP	absorption chiner secondary chined water pullip
Ó.	heat nower utilized by the absorption chiller (kW)	AC	alf-conditioning
	heat power utilized for space heating (kW)	AVVEV	auxiliary water cooling valve
Qheat	heat energy loss from engine casing per cycle (kl)		dissel anning fueled by dissel sil
Qenv	heat energy transferred to jacket water per cycle (kl)	DEDO	diesel engine fueled by diesel oli
Qjac rns	engine speed (1/s)	EEHX	engine exhaust neat exchanger
т	temperature (K)	EEHXV	engine exhaust heat exchanger valve
$\frac{1}{T}$	average temperature (K)	EJHX	engine jacket neat exchanger
1	overall heat transfer value between engine casing and	EJWP	engine jacket water pump
Ortenv	the environment (kW/K)	EZ	external zone
IIΔ	overall heat transfer value between cylinder and en	GENG	gas engine fueled by natural gas
UAjac	gipe include (kW/K)	GEPG	gas engine fueled by petrol gas
V	gille Jacket (KW/K) volume (m^3)	ICEPT	internal-combustion-engine primed trigeneration
V 147	pot work output per cucle (kl)	IZ	internal zone
vv _{net}	aloctrigity output from the prime mover (1/1/1)	LL	lift lobby
VV out	electricity output from the prime mover (kw)	RHWP	regenerative hot water pump
		SAC	supply air cooling coil
Symbols		SACV	supply air cooling coil valve
ϕ	angular displacement of crankshaft during the con-	SAF	supply air fan
	stant-pressure combustion of the Diesel cycle (degree)	SAH	supply air heating coil
γ	ratio of specific heat	SAHV	supply air heating coil valve
σ	Stefan–Boltzmann constant (= 5.669×10^{-11} kW/	SHHX	space heating heat exchanger
	$m^2 K^4$)	SHHXV	space heating heat exchanger valve
		SHWP	space heating water pump
Subscripts		VCCWP	vapor-compression chiller cooling water pump
1, 2, 3, 4	state points in the $P-V$ diagram of the engine cycles	VCPChWF	vapor-compression chiller primary chilled water
cas	engine casing		pump
cyl	cylinder	VCSChWF	vapor-compression chiller secondary chilled water
env	environmental or ambient condition		pump

building demand profiles for space cooling and heating can vary widely throughout the year. Hence, to evaluate more precisely the economic and/or energy merits of the trigeneration systems, year-round system performance analyzes are also conducted [16–20] (although comparatively fewer) which indicate that the benefit of applying trigeneration systems depends readily on the building type, the climate and the local cost levels of various types of energy. In particular, published works on the application of trigeneration systems to sub-tropical regions in which the air-conditioning load is cooling-dominated are rare. The main challenge is that the cooling demand can be low outside the peak-load season but at the same time the heating demand is still minimal which is not favorable for a trigeneration system.

Al-Sulaiman et al. [21] reviewed the characteristics of various kinds of trigeneration systems with different prime movers. They remarked that the internal-combustion-engine primed trigeneration (ICEPT) systems were among the most common and wellestablished types. Angrisani et al. [22] also highlighted the benefits of ICEPT systems for use in small- or medium-capacity applications. For the thermally-driven cooling devices, they may be absorption chiller, adsorption chiller, desiccant cooling system, etc. Fong et al. [23] commented that the absorption chiller performed the best in a solar cooling system when applied to a subtropical region like Hong Kong due to its higher coefficient of performance (*COP*) and the humid climate in summer. Hence, it can be expected that the combined use of the ICEPT system and the absorption chiller should offer satisfactory performance.



Fig. 1. Symbolic diagram of a trigeneration system.

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