



Trigenerative micro compressed air energy storage: Concept and thermodynamic assessment



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HIGHLIGHTS

- The trigenerative-CAES concept is introduced.
- The thermodynamic feasibility of the trigenerative-CAES is assessed.
- The effects of the relevant parameter on the system performances are dissected.
- Technological issues on the trigenerative-CAES are highlighted.

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ABSTRACT

Energy storage is a cutting edge front for renewable and sustainable energy research. In fact, a massive exploitation of intermittent renewable sources, such as wind and sun, requires the introduction of effective mechanical energy storage systems.

In this paper we introduce the concept of a trigenerative energy storage based on a compressed air system. The plant in study is a simplified design of the adiabatic compressed air energy storage and accumulates mechanical and thermal (both hot and cold) energy at the same time. We envisage the possibility to realize a relatively small size trigenerative compressed air energy storage to be placed close to the energy demand, according to the distributed generation paradigm. Here, we describe the plant concept and we identify all the relevant parameters influencing its thermodynamic behavior. Their effects are dissected through an accurate thermodynamic model. The most relevant technological issues, such as the guidelines for a proper choice of the compressor, expander and heat exchangers are also addressed. Our results show that T-CAES may have an interesting potential as a distributed system that combines electricity storage with heat and cooling energy production. We also show that the performances are significantly influenced by some operating and design parameters, whose feasibility in real applications must be considered.

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1. Introduction

Balancing supply and demand of electricity is nowadays a key issue for many countries, due to the increasing penetration of intermittent renewable energy sources (RES) and of distributed generation (DG) [1,2]. Different approaches are possible to cope with this problem including, updating the power regulation strategy for DG plants, utilizing electrical boilers and heat pumps, modifying the consumer demand of energy, switching to electricity

based mobility, fast ramping conventional plant, and updating the electricity distribution infrastructure [1–3]. In this scenario, electricity storage certainly plays a key role especially for a large scale exploitation of intermittent RES, such as wind or solar power [2,4].

Despite only two working applications of compressed air energy storage (CAES) exist [3,5,6] these storage systems claims the greater economical feasibility [1,2], among all the technological alternatives for large scale electricity storage (e.g. pumped hydro and batteries), thanks to their relatively low investment cost per unit capacity [2]. Nevertheless, the assessment of the economic potential of such a technology is still an open research issue [1,2,4,7,8]. In a CAES the mechanical energy is stored by

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Nomenclature

\dot{C}_j	chilling power exchanged in the j -th re-heater	k_{air}	thermal conductivity of air
$\beta_c(t)$	compression stage pressure ratio	k_{iron}	thermal conductivity of structural material
β	ratio between maximum reservoir pressure and environmental pressure	k_{wool}	thermal conductivity of insulation material
δ	pressure loss in the heat exchangers and connecting pipes	M	mass of air contained in the volume
\dot{m}	air mass flow	N	rotating velocity
\dot{Q}_i	thermal power exchanged in the i -th inter-cooler	N_{IC}	number of inter-coolers
\dot{Q}_R	thermal power lost through the reservoir walls	N_{RH}	number of re-heaters
\dot{V}	volumetric flow rate	N_c	number of compression stages
η_c	compressor small stage efficiency	N_e	number of expansion stages
η_e	small stage efficiency for the expander	N_s	specific speed
η_p	small stage efficiency general	p_{env}	environmental pressure
η_{ad}	adiabatic efficiency	p_{max}	maximum reservoir pressure
η_{el}	electrical efficiency	p_{min}	minimum reservoir pressure
η_{ex}	second law efficiency	p_R	pressure of the air in the reservoir
η_{iso}	isothermal efficiency	Q_i	thermal energy exchanged at the i -th inter-cooler
γ	ratio between maximum and minimum reservoir pressure	Q	gas constant relative to air
\mathcal{T}	storage capacity	r_1	internal radius of the reservoir (see Fig. 2)
Nu_{ext}	Nusselt number relative to the air outside the reservoir	r_2	external radius of the structural part of reservoir (See Fig. 2)
Nu_{int}	Nusselt number relative to the air inside the reservoir	r_3	external radius of the reservoir (See Fig. 2)
Ra	Rayleigh number	S	flow area
Re	Reynolds number	T	air temperature
μ	compressor load coefficient	t	time
ν	air kinematic viscosity	T_{ri}	reservoir inlet temperature
ϕ	compressor flow coefficient	T_{ci}	compressor inlet temperature
ρ	air density	T_{co}	compressor outlet temperature
Θ	time interval between charge and discharge of the volume	T_{env}	environmental temperature
ε	compression transformation exponent	T_{ico_i}	water temperature at the outlet of the i -th inter-cooler
ζ	polytropic exponent	T_{rho_j}	temperature at the outlet of the j -th re-heater
A	heat exchange surface	T_R	air temperature in the reservoir
a	zeroth order coefficient of air constant pressure specific heat	T_{ti}	turbine inlet temperature
a^*	zeroth order coefficient of air constant volume specific heat	T_{to}	turbine outlet temperature
b	first order coefficient of the air specific heat	U	global heat exchange coefficient
B_c	exergy relative to a chilling energy flux	u_2	peripheral blade speed
B_t	exergy relative to thermal energy	V	storage volume
C_i	thermal energy exchanged at the i -th re-heater	W_c	compression electrical work
c_w	water specific heat	W_d	expansion electrical work
c_{p_a}	constant pressure specific heat for air	A-CAES	adiabatic-CAES
c_{v_a}	constant volume specific heat for air	CAES	compressed air energy storage
D	reference length scale	CHCP	combined heat cooling and power plant
d	hydraulic diameter	CHE	compact heat exchanger
d_2	peripheral rotor blade diameter	DG	distributed generation
d_s	specific diameter	HE	heat exchanger
h_{ext}	convective coefficient outside the reservoir	IC	inter-cooler
h_{int}	convective coefficient inside the reservoir	PCHE	printed circuit heat exchanger
h_{ri}	enthalpy of the air entering the reservoir	PFHE	plate-fin heat exchanger
H_s	isentropic enthalpy change across the compressor	PHE	plate heat exchanger
		RES	renewable energy sources
		RH	re-heater
		STHX	shell and tube heat exchanger
		T-CAES	trigenerative-CAES

compressing air from the environment into a high pressure reservoir, through a compressor driven by an electrical motor. When electricity is required from the CAES the air is expanded through a turbine. In case of Diabatic-CAES, air is heated through the combustion of a fossil fuel before expansion [6]. On the other hand, in Adiabatic-CAES (A-CAES), air heating is performed by recovering the heat in the inter-cooled compression and no additional fuel is required [9–13].

Most of the literature related to CAES is focused on utility-scale applications [1,4,7,14], that are very large plants located close to the energy production. Nevertheless, the development of small

scale A-CAES (micro-CAES) to be placed close to the energy demand is of great interest [15–17]. Such a solution allows a more tight coupling between the energy storage systems and the energy demand. Moreover, micro-CAES may act as trigenerative systems, which is to say combined heat, cooling, and power plants (CHCP) by recovering heat after air compression and cooling energy during or after the expansion phase [15,16]. Trigeneration is possible only placing the CAES close to the energy demand, given the technical difficulty to transfer thermal and chilling energy at large distances. Such a plant allows to conjugate the widely recognized advantages of distributed trigeneration (see for instance [18–20]) with those of

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