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# Thermo-economic design optimization of parabolic trough solar plants for industrial process heat applications with memetic algorithms



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R. Silva<sup>a,b,\*</sup>, M. Berenguel<sup>a,b</sup>, M. Pérez<sup>a,b</sup>, A. Fernández-Garcia<sup>c</sup>

<sup>a</sup> CIESOL Research Center on Solar Energy, UAL-CIEMAT Joint Center, University of Almería, Ctra. Sacramento s/n, Almería 04120, Spain
<sup>b</sup> Automatic Control, Electronics and Robotics Research Group, University of Almería, Ctra. Sacramento s/n, Almería E-04120, Spain
<sup>c</sup> Plataforma Solar de Almería-CIEMAT, Ctra. Senés, km 4, E04200 Tabernas, Almería, Spain

# HIGHLIGHTS

• A thermo-economic optimization of a parabolic-trough solar plant for industrial process heat applications is developed.

- An analysis of the influence of economic cost functions on optimal design point location is presented.
- A multi-objective optimization approach to the design routine is proposed.
- A sensitivity analysis of the optimal point location to economic, operational, and ambient conditions is developed.
- Design optimization of a parabolic trough plant for a reference industrial application is developed.

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# ABSTRACT

A thermo-economic design optimization of a parabolic trough solar plant for industrial processes with memetic algorithms is developed. The design domain variables considered in the optimization routine are the number of collectors in series, number of collector rows, row spacing, and storage volume. Life cycle savings, levelized cost of energy, and payback time objective functions are compared to study the influence on optimal design point location. Furthermore a multi-objective optimization approach is proposed to analyze the design problem from a multi-economic criteria point of view. An extensive set of optimization cases are performed to estimate the influence of fuel price trend, plant location, demand profile, operation conditions, solar field orientation, and radiation uncertainty on optimal design. The results allow quantifying as thermo-economic design optimization based on short term criteria as the payback time leads to smaller plants with higher solar field efficiencies and smaller solar fractions, while the consideration of optimization criteria based on long term performance of the plants, as life cycle savings based optimization, leads to the reverse conclusion. The role of plant location and future evolution of gas prices in the thermo-economic performance of the solar plant has been also analyzed. Thermo-economic optimization of a parabolic trough solar plant design for the reference industrial process heat application at a southern Mediterranean country considered in this work shows a levelized cost of energy of 5 c€/kW h.

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# 1. Introduction

# 1.1. State-of-the-art

Currently there is a worldwide pressure on fossil fuel consumption, due to the combined effects of the increasing primary energy demand, limitations in available sources, and the environmental awareness of anthropogenic carbon dioxide emissions impact on

\* Corresponding author at: CIESOL Research Center on Solar Energy, UAL-CIEMAT Joint Center, University of Almería, Ctra. Sacramento s/n, Almería 04120, Spain. Tel.: +34 950214083. global warming [1]. These factors constitute an important driving force behind a progressive introduction of clean and viable alternatives in all energy consuming sectors.

The industrial sector has been identified as a potential and still largely unexplored application for solar thermal, since it represents a significant part of total primary energy consumption [2,3]. In the past decades several solar industrial process heat plants were constructed, however, due to the unstable progression of oil prices, their market penetration has been slow and difficult. Nevertheless, recent oil prices, and improvements on the state-of-the-art of medium temperature collectors are bringing back the attention to this area, as shown by the recent studies done by [4–8]. Previous assessments conducted by [3] identified the most relevant

E-mail address: ricardosilva@ual.es (R. Silva).

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# Nomenclature

Α	solar field collector area, m <sup>2</sup>	$N_p$	number of collectors in parallel
$a_0$	coefficient of thermal efficiency curve	Ns	number of collectors in series
$a_1$	coefficient of thermal efficiency curve, W/m <sup>2</sup> K	Qaux	auxiliary power, W
$a_2$	coefficient of thermal efficiency curve, W/m <sup>2</sup> K <sup>2</sup>	$Q_i$	input irradiance power on the solar field, W
$\overline{A_a}$	absorber cross-sectional area, m <sup>2</sup>	$O_n$	industrial process demanded power, W
Ă,	collector aperture area. $m^2$	O <sub>u i</sub>	useful power from solar field ith segment. W
Aai	exterior area of storage <i>i</i> th segment, $m^2$	Ren	Revnolds number
Aa	solar field gross area, $m^2$	T <sub>a</sub>	ambient temperature. °C
h <sub>1</sub>	incidence angle modifier curve coefficient	T:	storage temperature of <i>i</i> th segment $^{\circ}$ C
$b_{2}$	incidence angle modifier curve coefficient	T <sub>e</sub>	fluid average temperature of the solar field ith segment
62 C	collector concentration ratio	1 ],1	°C
C-	collector cost per unit area $f/m^2$	Tim	solar field inlet temperature °C
$C_a$	fixed costs of the plant $\epsilon$	T.	solar field outlet temperature °C
C,	land cost per unit area $e/m^2$	$T_{OUL}$	process temperature °C
C .	storage specific heat capacity at constant pressure of <i>i</i> th		process return temperature °C
$C_{p,i}$	soment 1/kg K		storage overall heat transfer coefficient $W/m^2 K$
C	segment, J/Kg K	V	storage volume m <sup>3</sup>
$C_{pi}$	piping cost per unit length, $\epsilon/m$	V	Storage volume, in volume of the storage its fluid comment $m^3$
$C_{sp}$	solar plant total cost, $\in$	V <sub>i</sub>	volume of the storage full huid segment, in
$C_{\nu}$	storage cost per unit volume, $\epsilon/m^2$	v <sub>w</sub>	absorber tube water velocity, m/s
D	absorber diameter, m	X	design variables vector
EJJ	solar plant enciency	X	design domain
$E_{p1}$	electric power consumed by pump of solar circuit, W	W	collector aperture width, m
$E_{p2}$	electric power consumed by pump of load circuit, W	β	collector tracking angle, °
$E_t$	annual thermal energy produced by the plant, J	$\Delta p$	pressure differential, Pa
f	friction factor	$\Delta T_p$	process temperature differential, °C
$f_{bs}$	fraction of shaded area	3	absorber tube inner absolute roughness, m
$F_s$	solar fraction	$\eta_i$	efficiency of the solar field <i>i</i> th segment
g	gravitational acceleration, m/s <sup>2</sup>	$\theta$	incidence angle, °
$G_{b,n}$	normal direct irradiance, W/m <sup>2</sup>	$ ho_i$	density of the storage <i>i</i> th fluid segment, kg/m <sup>3</sup>
$K_d$	market discount rate	ν	piping design velocity, m/s
K <sub>fuel</sub>	annual cost of backup fuel, $\in$		
Kins	insurance tax	Abbreviations	
K <sub>inv</sub>	plant total investment, $\in$	AR	aspect ratio
Kosm	plant operational and maintenance costs, $\in$	CRF	capital recovery factor
$k_{ heta}$	incidence angle modifier	DNI	direct normal irradiance
Ľ	piping total length, m	F-W	Fast_West
$L_{C}$	collector length, m	CA	genetic algorithm
Ln	spacing between rows, m	IFA	International Energy Agency
LCCc	life cycle cost of a conventional fuel system only system.	LCOF	levelized cost of energy
	€	LCOL	life cycle savings
ICCs	life cycle cost of a solar plus auxiliary energy system $\epsilon$	LCS N C	North South
LCS	life cycle savings. €	11-3 TDD	norm-soum
m,	mass flow rate on load circuit kg/s		payback time
m.	mass flow rate on solar circuit $k\sigma/s$	TIC	tunical motoorological year
n	nlant lifetime years	I IVI Y	typical meteorological year
11	plant incline, years		

temperature ranges and industrial thermal demand consumers, concluding that a significant part of these demands are situated at temperature levels between 100 °C and 250 °C. At this temperature level standard stationary non-concentrating collectors present large thermal losses that reduce their efficiency, hence the use of tracking concentrating technology should be considered. Furthermore, industrial processes are frequently located on places where buildings are densely packed and there is small available area [4,8], so it is relevant that the collectors also allow rooftop installation. These requirements justify the recent developments of new concentrating collector designs that are modular and lightweight, such as small parabolic troughs [9–11]. Efforts have been made in the past to assess the potential of parabolic trough collectors for industrial applications. A study performed by [4] reported that parabolic trough collectors reached energy costs ranging from  $0.04 \in /kWh$  to  $0.08 \in /kWh$ , depending on the industrial process temperature, and considering favorable solar irradiance conditions. These values were substantially higher than typical thermal energy costs in industry, hence this technology was still not able to reach competitiveness without significant subsidies. Another study performed by [8] reaches similar conclusions and evaluates the subsidies intensity necessary to achieve competiveness with other energy sources, for typical investor profile requirements. In a general way, although all recent studies point in the same direction and identify a large potential for solar thermal energy in the industrial sector, further research efforts are still required to increase its economic performance, in order to be able to compete with cheaper fossil fuel energy sources without the need of public subsidies.

In this paper the design of a parabolic-trough solar plant for industrial process heat applications is optimized by thermohydraulic model simulation in order to improve its economic performance. Although there are well defined and established methods for designing low and high-temperature solar plants [1,35], there are at present few studies that address the particular Download English Version:

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