Building and Environment 82 (2014) 490-501

Contents lists available at ScienceDirect

Building and Environment

journal homepage: www.elsevier.com/locate/buildenv

Practical approaches to determine ventilation rate for offices while considering physical and chemical variables for building material emissions

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A R T I C L E I N F O

Article history: Received 18 June 2014 Received in revised form 6 September 2014 Accepted 19 September 2014 Available online 28 September 2014

Keywords: Volatile organic compounds Recirculation Intermittent Distribution Reaction Health-relevant pollutant

ABSTRACT

Indoor air pollutants in offices can be attributed to various sources, including building materials, consumer products, and exhalation from occupants. The required ventilation rate for offices can be determined by estimating the majority of emissions originated from building materials, as an additional determinant factor for ventilation rate, with the assumption of constant ventilation with 100% outdoor air, uniform indoor mixing, and no chemical reactions. In this paper, the validity of these assumptions was investigated by incorporating the effects of various physical and chemical factors in determining material emissions and ventilation rates. Three physical factors investigated were recirculation ventilation, intermittent ventilation and pollutant distribution. Simplified methods using correction factors were proposed to revise the ventilation rate and validated by emission modeling and CFD method. In addition, three chemical factors were discussed. First, 28 building materials were selected from the NRC database and each was subject to determining the ventilation rate. As a result, 28 leading pollutants that are likely to determine the ventilation rate were obtained. Because most of the leading pollutants are reactants rather than products of indoor air reactions, it was concluded that the current ventilation rate determining methods should still be applicable. Additionally, a correction method was proposed for a reaction product such as formaldehyde. Second, the methods to revise ventilation rate based on temperature variation and pollutant concentration in outdoor air were proposed. This study showed that ventilation rate for offices could be determined based on building material emissions in more realistic ventilation and environmental conditions.

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1. Introduction

The indoor environment is susceptible to contaminants and usually more polluted than outdoor air due to indoor sources such as humans, open fires, building materials, consumer products, indoor activities, and so on [1–4]. It is widely reported that indoor pollution can adversely affect human health, comfort and productivity, and even be the cause of excessive morbidity and mortality [5,6]. Although outdoor air also contains contaminants, usually at lower concentrations [7,8], that are originated from traffic exhaust, industry, etc. [9,10], ventilation with outdoor air is still the basic means to remove pollutants emitted from various indoor sources, thereby reducing their concentrations in occupied spaces and achieving better indoor air quality [11,12]. However, because of

* Corresponding author. *E-mail address:* weiye_hvac@outlook.com (W. Ye). transient nature of indoor air quality partly due to the everchanging emission sources and indoor air chemistry, as well as the increasing demand of efficient use of energy, setting an adequate ventilation rate for buildings is still in question.

Throughout the history of ventilation, ventilation rate is prevailingly stated as the term of minimum air change rate (ACH) per person for at least two reasons. First, it is reasonable and convenient to determine ventilation rate based on the number of occupants since the health of the occupants is the objective of ventilation in most cases [4,13,14]. Second, humans were considered as the main source for indoor pollution ever since Yaglou et al.'s experiments on the relationship between occupants, perceived indoor air quality and ventilation rates [15,16]. Consequently, the issue of how much the air change rate per person is appropriate at different times has become important worldwide. For instance, the ACH per occupant, which is termed as the conventional method, in indoor air quality standards or regulations for







Nomenclature		q_n	eigenvalues in Eq. (4) (m^{-1})
		Q	airflow rate of the room $(m^3 \cdot h^{-1})$
		R	The ratio of total flow rate to the original ventilation
Symbols			rate (dimensionless)
A_1, A_2	independent and empirical parameters in Eqs. (17) and	Ra	ventilation rate required per unit area $(L_1 s^{-1} \cdot m^{-2})$
	(18)	R_{bz}	the breathing zone ventilation rate $(L \cdot s^{-1})$
A _i	exposed surface area of the <i>i</i> -th building material (m^2)	R_p	ventilation rate required per person $(L \cdot s^{-1} \cdot person^{-1})$
A_d	indoor surface area for the ozone deposition (m ²)	S_j	total counts of the <i>j</i> -th pollutants that determines
A_z	the net occupiable floor area of the ventilation zone		ventilation rate (dimensionless)
$C_{0,i,j}$	(m^2)	S _{total}	total combinations of the material/reference pair
	initial material-phase emittable concentration for the		(dimensionless)
	<i>j</i> -th pollutant in the <i>i</i> -th building material (μ g·m ⁻³)	Т	temperature (K)
$C_{i,j,\infty}(t)$	material-phase concentration for the <i>j</i> -th pollutant at	$t_{A,n}$	duration of the <i>n</i> -th non-ventilation period in
	the top of the <i>i</i> -th building material when emissions		intermittent ventilation (h)
	reach steady-state (µg·m ^{−3})	$t_{\mathrm{B},n}$	duration of the <i>n</i> -th ventilation period in intermittent
CR _j	characteristic frequency of the <i>j</i> -th leading pollutants		ventilation (h)
	(fractional)	v_d	ozone deposition velocity $(m \cdot h^{-1})$
D _{i.i}	material-phase diffusion coefficient of the <i>j</i> -th	V	room volume (m ³)
	pollutant emitted from <i>i</i> -th building material $(m^2 \cdot s^{-1})$	V_{bz}	volume of the breathing zone (m ³)
E _{bz}	pollutant distribution effectiveness coefficient	$V_{bz,x}$	volume of the <i>x</i> -th tiny space in the breathing zone
	(dimensionless)		(m ³)
E _{i.i}	steady-state hourly emission rate for the <i>j</i> -th pollutant	Х	correction factor of temperature effect on emission
\overline{E}_{ABn}	in the <i>i</i> -th building material ($\mu g \cdot h^{-1}$)		rate of chemical pollutant in building materials
	the average pollutant hourly emission rate of the <i>n</i> -th		(dimensionless)
-710,11	periodic cycle in intermittent ventilation ($ug \cdot h^{-1}$)	Xlead	correction factor of temperature effect on emission
f	the duration time for one ventilation period (in		rate of the known leading pollutant (dimensionless)
J	intermittent ventilation) divided by the cycle time	v	pollutant concentration limit in indoor air quality
	(fractional)	5	reference ($\mu g \cdot m^{-3}$)
h	convective mass transfer coefficient $(m \cdot s^{-1})$	y_{hzx}	gas-phase concentration for the <i>j</i> -th pollutant in the <i>x</i> -
H H	a lumped variable in Eq. (4) $H = h_{\rm e}/D_{\rm e}K_{\rm e}$ (m ⁻¹)	0 02,11	th tiny space of the breathing zone $(\mu g \cdot m^{-3})$
K	material/air partition coefficient for the <i>i</i> -th pollutant	\overline{y}_{Bn}	average gas-phase pollutant concentration of the <i>n</i> -th
Nij	emitted from <i>i</i> -th building material (dimensionless)	J D,N	ventilation period in intermittent ventilation ($ug \cdot m^{-3}$)
Ι.	thickness of the <i>i</i> -th building material (m)	Vd	formaldehyde vield (dimensionless)
L_l M	formaldehyde emission rate from building materials	$\mathbf{v}_{i}(t)$	gas-phase concentration for the <i>i</i> -th pollutant at time <i>t</i>
111	$(\mu \alpha, h^{-1})$	<i>y</i> ₁ (<i>v</i>)	$(\mu\sigma \cdot m^{-3})$
• h	(µg·n)	$\overline{\mathbf{V}}$: to a	average pollutant concentration within the breathing
$M_j^{\mathcal{S}}(t)$	the hourly emission rate of the <i>j</i> -th pollutant from all	J J,DZ	zone (ug.m ^{-3})
	the building materials at time $t (\mu g \cdot h^{-1})$	<u></u> /	average pollutant concentration within the breathing
MW_f	molecular weight of formaldehyde $(g \cdot mol^{-1})$	$y_{j,bz}$	average politicant concentration within the breathing
MW _{ozone}	molecular weight of ozone $(g \cdot mol^{-1})$		zone with the revised ventilation rate ($\mu g \cdot m^{-3}$)
п	summation index (dimensionless)	$y_{j,pred}$	theoretical steady-state gas-phase concentration for
Ν	ventilation rate of the room (h^{-1})	0	the <i>j</i> -th pollutant ($\mu g \cdot m^{-3}$)
N _b	pre-determined required ventilation rate for diluting	y_{ozone}^{o}	outdoor ozone concentration ($\mu g \cdot m^{-3}$)
	building material emissions (h^{-1})	A1.1 ·	
N _c	revised required ventilation rate based on chemical	Abbrevia	tions
	reactions (h^{-1})	ACH	air change rate per hour
N _d	revised required ventilation rate based on pollutant	ASHRAE	American Society of Heating, Refrigerating and Air-
	distribution effectiveness (h^{-1})		Conditioning Engineers
Ni	revised required ventilation rate for intermittent	CFD	computational fluid dynamics
	ventilation (h^{-1})	HVAC	heating, ventilation and air conditioning
Ni	required ventilation rate for the <i>j</i> -th VOC (h^{-1})	IAQ	indoor air quality
N _q	revised required ventilation rate based on outdoor air	VOC	volatile organic compound
	quality (h^{-1})	TVOC	total volatile organic compounds
Nr	revised required ventilation rate for recirculated		
	ventilation (h ⁻¹)	Greeks	
N _T	revised required ventilation rate for temperature	α	the ratio of pollutant concentration in outdoor air
	variation (h^{-1})		(supply air) to the concentration limit in indoor air
Р	formaldehyde production rate ($\mu g \cdot h^{-1}$), which is		quality reference (dimensionless)
	defined as $P = v_{1}^{0} \dots v_{d} v_{d} A_{d} \left(\frac{MW_{f}}{MW_{f}} \right)$	η	outdoor air fraction in the supply air (fractional)
ת	$\frac{1}{\sqrt{2}} = \frac{1}{\sqrt{2}} \frac{1}{$		
Γ_Z	number of people in the ventilation zone (person)		

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