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Degradation of flexural strength in reinforced concrete members caused by steel corrosion



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HIGHLIGHTS

- Strength degradation model in RC members with corroded steel bars was proposed.
- The proposed model reflects the bond performance degradation due to corrosion.
- The area loss of steel bars was also considered in the analysis model.
- The concept of average expansion pressure was introduced into the analysis model.
- The proposed non-linear analysis model was validated by various test results.

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ABSTRACT

The volume expansion of reinforcements due to corrosion produces tensile stresses on the surrounding concrete, leading to radial cracks in the concrete cover and to significant reduction in the serviceability performance and durability of reinforced concrete members. In this study, a flexural strength assessment model of reinforced concrete (RC) members with corroded bars has been developed, which is an extension of the steel–concrete bond strength models based on the thick-walled cylinder theory. This model simulates the degradation of flexural strength in RC members according to the corrosion rate and flexural cracks, and is in good agreement with available experimental data.

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1. Introduction

The high pH in the pore solution of concrete protects the embedded steel in reinforced concrete structures against corrosion in moderate environments [1–3]. However, once the thin passive film protecting the steel against corrosion is damaged by concrete carbonation or chlorides, the corrosion mechanism is initiated

[1–3]. Corrosion products generated on the periphery of reinforcing bars cause two to six times the volume expansion compared to the amount of steel consumed by corrosion [1–5]. This results in radial cracks in the concrete around the reinforcing bars or the delamination of the cover concrete [3–7]. Furthermore, the loss of the effective cross-sectional area of reinforcing bars due to corrosion and the reduction of the bond strength due to the damage to the rebar ribs directly degrade the flexural strength of reinforced concrete members [2,3,8–25]. Previous studies have proposed various analysis models for the relationship between the corrosion rate and the bond strength [8,9,22,24,25]. Most of the existing models are based on the two-dimensional thick-walled cylinder model (TWCM). Although this approach can easily model the splitting cracking on concrete along the longitudinal direction over the reinforcing bars due to their volume expansion, the effect of cracking perpendicular to the member axis caused by the service

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Nomenclature

| | | | |
|------------|--|--------------------------|---|
| A_{cef} | area of effective embedment zone of the concrete | T_s | tensile force in reinforcement |
| A_s | sectional area of non-corroded tensile reinforcement | t_r | thickness of rust layer |
| A'_s | sectional area of compressive reinforcement | u | radial displacement |
| A_v | sectional area of transverse reinforcement | x | corrosion penetration depth |
| A_x | sectional area of corroded tensile reinforcement | x_{cr} | corrosion penetration depth at cover cracking |
| b | beam width | α | volume ratio of corrosion products to initial steel |
| C | clear cover thickness | α_1 | stress-block factor |
| c | neutral axis depth | α_c | face angle of concrete crushing plane |
| C_c | compressive force in concrete | β | angle of inclined cracking |
| c_e | effective depth of concrete cover | β_1 | stress-block factor |
| C_s | compressive force in reinforcing bars | γ | angle between the direction of P_x and the inclined crack- ing |
| d | depth to the tensile reinforcement | ε_1 | concrete strain corresponding to the tensile stress $0.15f_t$ |
| d' | depth to the compressive reinforcement | ε_c | compressive strain in concrete |
| d_0 | core diameter of deformed bar | ε_{co} | concrete strain corresponding to concrete compressive strength |
| d_b | diameter of non-corroded bar | ε_{cr} | cracking strain corresponding to concrete tensile strength (f_t/E_c) |
| d_x | diameter of corroded bar | ε_r | flexural cracking strain corresponding to modulus of rupture |
| E_c | elastic modulus of concrete | ε_s | tensile strain in reinforcing bar |
| E_s | elastic modulus of steel | ε'_s | compressive strain in reinforcing bar |
| f | friction coefficient of crushed concrete | ε_u | concrete strain corresponding to zero tensile stress in concrete |
| f_c | compressive stress of concrete | ε_y | yield strain of steel bar |
| f_{ck} | compressive strength of concrete | ε_α | largest tensile strain in the effective embedment zone |
| f_r | modulus of rupture | ε_β | smallest tensile strain in the effective embedment zone |
| f_s | tensile stress in reinforcement | ε_θ | tangential tensile strain |
| f_t | concrete tensile strength | $\varepsilon_{\theta c}$ | tangential tensile strain at $r = R_o$ (surface cracking) |
| f_y | yield strength of steel bar | θ | angle of octahedral shear stress (angle of similarity) |
| f_{p_x} | friction force on the bearing face | λ | parameter to calculate the failure condition of concrete under multiaxial stress state |
| h_x | rib height of corroded steel bar | μ | friction coefficient between steel and concrete |
| I_1 | invariants of the stress tensor | ρ_{ef} | tensile reinforcement ratio in the effective embedment zone |
| J_2 | invariants of the deviatoric stress tensor | ρ_v | stirrup ratio in splitting plane ($A_v/c_e s_v$) |
| J_3 | invariants of the deviatoric stress tensor | Σ_0 | perimeter of the corroded rebar (πd_x) |
| K_1 | coefficient that characterizes bond properties of steel bar | σ_1 | principal stress in the direction 1 |
| K_2 | coefficient to account for strain gradient | σ_2 | principal stress in the direction 2 |
| K_{sv} | coefficient to account for stirrup confinement | σ_3 | principal stress in the direction 3 |
| l_d | development length of tensile reinforcement | σ_c | average radial compressive stress |
| l_r | rib spacing | σ_m | octahedral stress |
| M_n | flexural strength | σ_θ | tangential tensile stress |
| P_{avg} | average corrosion pressure over the length of crack ele- ment | τ | average shear stress |
| P_c | confining stress in uncracked concrete | τ_{avg} | average bond strength over the length of crack element |
| P_{corr} | corrosion pressure due to expansion of corrosion prod- ucts | τ_{bu} | bond strength of corroded reinforcing bar considering corrosion pressure effect |
| P_{crx} | average radial force | τ_{crx} | bond strength of corroded reinforcing bar without cor- rosion pressure effect |
| p_x | pressure in front of the bar rib | τ_{total} | bond strength of corroded reinforcing bar considering stirrup confining effect |
| r | radius from the center of steel bar | φ | rib face angle of deformed bar |
| R_c | radius at the crack tip | | |
| R_i | initial radius of steel bar | | |
| R_o | radius at the surface of concrete | | |
| R_u | radial distance at which the hoop strains reach ε_u | | |
| s | maximum spacing between longitudinal reinforcing bars | | |
| s_m | average spacing of flexural cracks | | |
| s_v | stirrup spacing | | |
| T_c | tensile force in concrete | | |

loads, such as the flexural cracking, is not taken into account. Therefore, this study incorporates the concept of average corrosion pressure into the bond strength analysis model so that it is possible to include the effect of flexural cracking on the concrete volume pressure in a simple but reasonable way. This modified bond strength model was implemented into a non-linear flexural strength analysis of the reinforced concrete members with corroded bars.

2. Estimation of radial pressure due to corrosion

2.1. Compatibility and constitutive relationships

Fig. 1(a) shows an idealized TWCM consisted of a reinforcing bar embedded in concrete. According to the theory of elasticity [26], the deformation-strain relationship $[u(r)-\varepsilon_\theta(r)]$ can be expressed in the polar coordinate system as follows:

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