



# Behaviour of hexagonal concrete-encased CFST columns subjected to cyclic bending



Dan-Yang Ma<sup>a</sup>, Lin-Hai Han<sup>a,\*</sup>, Xiaodong Ji<sup>a</sup>, Wei-Biao Yang<sup>b</sup>

<sup>a</sup> Department of Civil Engineering, Tsinghua University, Beijing 100084, PR China

<sup>b</sup> Beijing Institute of Architectural Design, Beijing 100045, PR China

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## ABSTRACT

The hexagonal concrete-encased CFST column consists of a CFST (concrete-filled steel tube) core and a hexagonal-shaped reinforced concrete (RC) encasement. This paper presents the finite element (FE) analysis of hexagonal concrete-encased CFST columns subjected to axial compressive forces and cyclic bending moments. High-fidelity finite element analysis (FEA) model is established and validated by comparison with the test data in terms of failure mode and hysteretic curves. From the FEA model, the hysteretic response of the composite columns, the contact stress between the steel tube and concrete, and the strength contribution of different components during the full range of loading are illustrated. Parametric analysis is conducted to investigate the influences of various parameters on force-displacement envelope curves of the hexagonal concrete-encased CFST columns. The parameters include the material strength, confinement factor of CFST section, stirrup characteristic value, area ratio of CFST core to RC encasement, and axial force ratio. Finally, simplified methods are proposed to predict the flexural strength of hexagonal concrete-encased CFST columns. The predictions from simplified methods showed good agreement with the experimental and analytical results.

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## Notation

$A$	Cross-sectional area of concrete-encased CFST	$M_{CFST}$	Flexural strength of CFST component
$A_{core}$	Cross-sectional area of CFST core	$M_u$	Flexural strength
$A_{e,out}$	Equivalent area of outer concrete	$M_{uc}$	Predicted flexural strength
$B$	Side length	$M_{ue}$	Measured flexural strength
$D$	Distance to the middle axis	$n$	Axial force ratio
$E_s$	Modulus of elasticity of steel	$N_0$	Constant axial load
$E_c$	Modulus of elasticity of concrete	$N_u$	Compressive strength
$f_c'$	cylinder strength of core concrete	$P$	Lateral load
$f_{c,core}$	Prismatic strength of core concrete	$P_{uc}$	Predicted ultimate strength
$f_{c,out}$	Prismatic strength of outer concrete	$P_{ue}$	Measured ultimate strength
$f_{cu,core}$	Cube strength of core concrete	$s$	Stirrup spacing
$f_{cu,out}$	Cube strength of outer concrete	$t$	Steel tube thickness of CFST
$f_{ys}$	Yield strength of steel tube	$\alpha$	Area ratio of CFST core
$f_{yl}$	Yield strength of longitudinal rebar	$\alpha_s$	Steel ratio of CFST core
$f_{yh}$	Yield strength of stirrup	$\beta$	Factor of equivalent rectangular stress block
$M_{RC}$	Flexural strength of the RC encasement component	$\Delta$	Displacement
		$\Delta_y$	Yield displacement
		$\Delta_u$	Ultimate displacement
		$\theta$	Drift ratio
		$\theta_u$	Ultimate drift ratio
		$\lambda_v$	Stirrup characteristic value
		$\rho_v$	Volumetric stirrup ratio
		$\rho_s$	Longitudinal rebar ratio
		$\xi$	Confinement factor for CFST section

\* Corresponding author.

E-mail address: lhhan@tsinghua.edu.cn (L.-H. Han).

## 1. Introduction

CFST consists of the steel tube filled with concrete. CFST members with hexagonal cross section are used in some high-rise buildings for their aesthetic performance, where the members act as mega columns in the mega frame-core wall systems [1]. Moreover, the hexagonal shape makes the column easier to be connected with beams and the core wall. In the past, the performance of hexagonal CFST column members under axial compression and bending has been investigated by Xu et al. [1]. The CFST component is found to have increased compressive strength and ductility.

The concrete-encased CFST column consists of an inner CFST component and an outer reinforced concrete encasement component. The steel tube can provide confinement to the core concrete, and the reinforced concrete encasement can provide fire protection and corrosion protection. Because of these benefits, the concrete-encased CFST column has been increasingly used in high-rise buildings and bridges in China [2], such as Baoli Square of Shanghai, Jialing River Bridge and Labajin Bridge. The cross sections of the concrete-encased CFST column are usually circle, square, and rectangular for an easy beam-to-column connection. Han et al. [3] conducted experimental tests on concrete-encased CFST columns with aforementioned cross section. Ji et al. [4,5] reported a series of experiments on the seismic performance of concrete-encased CFST columns with square section. Both sets of tests indicate that concrete-encased CFST columns have favorable ductility and energy dissipation. Qian et al. [6] presented an analytical study on the cyclic behaviour of concrete-encased CFST columns with square section. In some complicated structures like China Zun, the highest building in Beijing, the column is not only connected to beams and shear wall in the longitudinal direction or transverse direction, but also in the diagonal direction. In such a circumstance, the hexagonal column section is convenient to be connected to beams and shear wall. The concrete-encased CFST column with a hexagonal section is designed to be applied in that circumstance. However, the research on the hexagonal concrete-encased CFST columns is very limited. The whole response of the hysteretic curve, the contact stress between steel tube and concrete, and the strength contribution of different components of the hexagonal concrete-encased CFST column have yet to be clearly understood.

To this end, the main objectives of this research are thus threefold: (1) To develop a high-fidelity finite element analysis (FEA) model that can accurately represent the cyclic behaviour of the hexagonal concrete-encased CFST column; (2) To conduct full-range analysis of the hexagonal concrete-encased CFST column, for estimating the contact stress between steel tube and concrete, and the strength contribution of different

components; and (3) To establish a simplified model for the flexural strength prediction of the hexagonal concrete-encased CFST column.

## 2. FEA model

A FEA model was developed using ABAQUS/Standard module [7] to represent the specimen of hexagonal concrete encased CFST column in Xu [8]. Using the symmetry, a quarter model was considered.

The schematic view of the FEA model of the hexagonal concrete-encased CFST is shown in Fig. 1. This type of cross section is chosen to be a 'standard' hexagonal shape in this study. The dual-axisymmetric cross section has an equal side length ( $B$ ) for each edge of CFST core, two interior angles of  $90^\circ$  ( $\theta_1$ ) and four interior angles of  $135^\circ$  ( $\theta_2$ ).

### 2.1. Material properties

The concrete damaged plasticity model was used to simulate the behaviour of the concrete under cyclic loading. The concrete section was divided into three regions according to different levels of confinement, as shown in Fig. 1(a). The uniaxial compressive strain-stress relation of the core concrete, outer stirrup-confined concrete and concrete cover were simulated by the constitute models proposed by Han et al. [9], Han and An [10] and Attard and Setunge [11], respectively. Note that there is no specific constitute model for the core concrete of the hexagonal CFST. The axial compressive behaviour of the hexagonal CFST [1] and rectangular CFST [12] was compared by experimental tests. Both sets of CFST columns for comparison had similar confinement factor  $\xi$  ( $= \frac{\alpha_s f_{ys}}{f_{ck,core}}$ ) and compressive strength of core concrete  $f_{cu,core}$ . The experimental results are shown in Fig. 2. The hexagonal CFST specimens were named by 'C', and the rectangular CFST specimens by 'rc'. It can be concluded that the axial strain-force relationship curves of two different sections are similar, which means the uniaxial compressive model of core concrete for the rectangular CFST can be used for the hexagonal CFST. The uniaxial compressive model of core concrete for the rectangular CFST is used for the core concrete with the hexagonal section. The uniaxial tensile model suggested by Shen et al. [13] is used for those types of concrete. The elastic modulus  $E_c$  and Poisson's ratio of concrete are taken as  $4730\sqrt{f'_c}$  and 0.2 respectively according to ACI318-11 [14], where  $f'_c$  is cylinder compressive strength in MPa.

The longitudinal rebars are simulated using Clough model [15]. The steel tube and stirrups are simulated using combined hardening model as shown in Fig. 3. The Clough model is used for the reason that

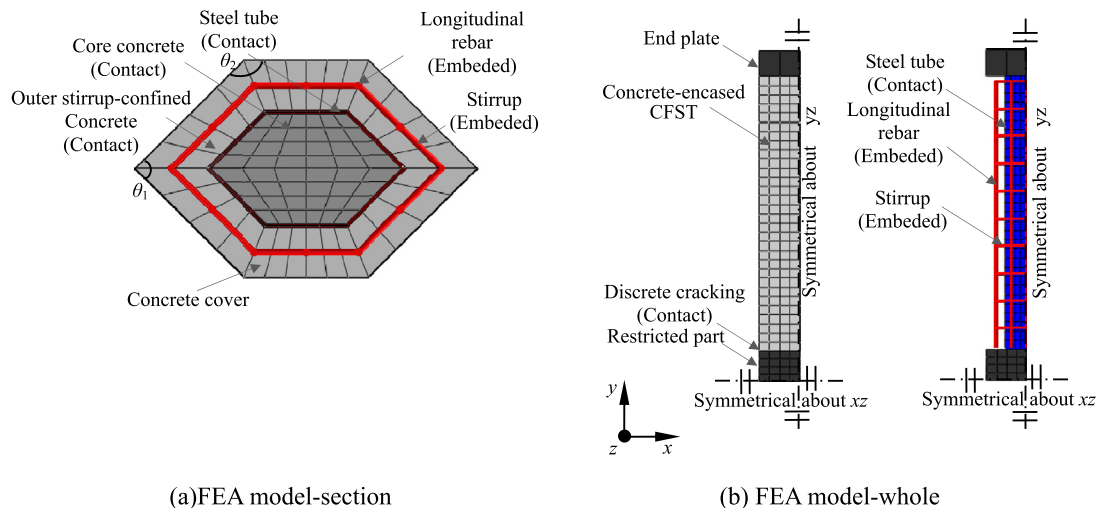


Fig. 1. Schematic view of the FEA model.

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