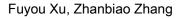
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Numerical simulation of windless-air-induced added mass and damping of vibrating bridge decks



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Numerical simulation of windless-air-induced added mass and damping of

vibrating bridge decks

Fuyou Xu, Zhanbiao Zhang*

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School of Civil Engineering, Dalian University of Technology, Dalian 116024, China

Abstract: The windless-air-induced added mass/mass moment of inertia (m_a/I_a) and damping (c_a) effects on 5 mechanical parameters of a vibrating bridge deck are usually ignored in wind tunnel tests. In this paper, for 6 7 three typical deck sections, computational fluid dynamics simulations are carried out to study the vertical/torsional single degree-of-freedom forced vibration under windless conditions, and further to reveal 8 9 the effects of m_a , I_a , and c_a on the modal parameters. The influences of turbulence model, computational 10 domain size, grid resolution, and time step size are analyzed. For the addressed issue, the Reynolds stress equation model (RSM) is found to be more suitable than the shear stress transportation (SST) k- ω model. A 11 mathematical model for aerodynamic forces at zero wind speed is presented by using the dimensionless m_a , 12 13 I_a , and c_a , and they can be extracted by combining the motions and the numerically simulated aerodynamic forces using the least squares method. The numerically simulated results for an ideal plate under small 14 amplitudes are very close to the theoretical values, and consequently verify their accuracy. The causes for the 15 non-zero values of flutter derivatives H_4^* and A_3^* at zero wind speed are revealed. In the windless air, the 16 added damping almost linearly increases with the vibration amplitude. Five existing long-span bridge deck 17 18 models are taken as examples to investigate the effects of m_a , I_a , and c_a on structural frequencies and 19 damping ratios.

Keywords: Computational fluid dynamics; Bridge deck; Mechanical parameter; Added mass/mass moment
of inertia; Damping ratio.

22 1. Introduction

Structural dynamic parameters including mass (m), mass moment of inertia (I), mechanical frequencies, 23 and mechanical damping ratios are of great significance for aerodynamic performance of long-span flexible 24 25 bridges. Wind tunnel tests for spring-suspended rigid segmental deck models are usually carried out for the study of wind induced vibrations and identification of aerodynamics parameters, usually involving both 26 vertical bending and torsional modes. In wind tunnel tests, mechanical frequencies and damping ratios are 27 usually determined according to the recorded free decay vibration signals at zero wind speed, i.e., windless 28 condition. If the vertical and torsional vibration amplitudes (A_h, A_a) are not too large, e.g., $A_h/B < 0.01$ (B is 29 deck width), $A_a < 2^\circ$, the amplitudes have negligible influence on the extracted frequencies and damping 30 ratios, and they are commonly assumed to be constants. However, some studies (Cao and Ge, 2017; Zhang 31 and Xu, 2018) found that the frequencies and damping ratios are amplitude-dependent, and related analyses 32 are currently inadequate. Furthermore, the identified system frequencies (stiffness) and damping ratios under 33 zero wind speed condition actually contain two components of contribution: (1) the mechanical part, i.e., m_{s} 34 I, spring rigidity, material, connection, etc.; (2) the aerodynamic part, originates from the interference effect 35

^{*} Corresponding author.

E-mail address: zzbiao@mail.dlut.edu.cn

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