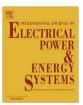
FISEVIER

Contents lists available at ScienceDirect

Electrical Power and Energy Systems

journal homepage: www.elsevier.com/locate/ijepes



Probability of adequacy evaluation considering power output correlation of renewable generators in Smart Grids



Stefania Conti*, Santi A. Rizzo

Dipartimento di Ingegneria Elettrica, Elettronica e Informatica (DIEEI), University of Catania, Italy

ARTICLE INFO

Article history: Received 27 March 2013 Received in revised form 27 February 2014 Accepted 21 March 2014

Keywords: Distributed generation Islanding Power output correlation Power system reliability Probability of adequacy Renewable generators

ABSTRACT

Smart Grids implementation is mainly intended to reduce the negative impact of distributed generators' (DGs) high penetration (especially renewable DGs), and to optimally manage distributed resources in order to improve overall efficiency and power quality. In terms of service continuity, this implies being able to reduce average outages rate and duration. A possible solution is to operate in intentional islanding some portions of the distribution network when faults occur. To this aim local DGs' adequacy must be evaluated.

This paper presents a new analytical expression useful to assess the ability of local DGs to meet a potential island load. Such an expression accounts for both load shedding and curtailment policies and it encompasses the correlation among loads' power demand, the correlation among renewable DGs' power outputs for generators of the same technology, the correlation among renewable DGs' power outputs for generators of different technologies, and, finally, the correlation among loads' power demands and renewable DGs' power outputs.

© 2014 Elsevier Ltd. All rights reserved.

Introduction

During the last decade two major issues have been characterizing planning and operation of modern distribution networks [1-4]. One is the need to increase the installed capacity of renewable distributed generation in order to meet the international environmental issues [5–7] and to bring energy production closer to load centres [8]. The other one is the pressure posed on distribution networks in terms of national regulations aiming at improving service quality and, in particular, service continuity [9–12]. In this context, the possibility to supply electrical loads in the event of fault in the main distribution system, by means of local distributed generators (DGs), is acknowledged as a valuable perspective to improve the overall system reliability. The basic concept is to operate in islanding mode some portions of the distribution network when a fault occurs, in order to minimize the unsupplied loads until the system is restored to improve reliability [13-16]. To reach such a challenging goal, it is necessary to estimate the ability of distributed generators to meet the island load [17-19]. A major issue in the adequacy [20-23] assessment procedure is taking into account the correlation existing among the power outputs of unconventional DGs (UDGs) based on the same renewable intermittent

primary energy source (such as sun and wind) [24–29]. In the present work, the set made up by the islands' UDGs based on the same technology is called a *class* (e.g. solar class and wind class).

A generalized systematic approaches and the related analytical expressions have been presented in [30] to evaluate distribution system reliability in Smart Grids where island operation of micro-grids is intended to help improving local and overall reliability thanks to an advanced automation and protection scheme that allows multi-microgrid network paradigm implementation [31]. The expressions also consider a procedure to calculate the adequacy of micro-grids in the presence of both conventional and renewable DGs. The main merit of such a procedure is to provide a new general analytical expression that takes into account both load shedding (user load disconnection) and curtailment (user load reduction) policies to quantify the adequacy of a potential island. On the other hand, its main drawback is that it neglects the correlation among island loads' power demand, the correlation among power outputs of island UDGs belonging to the same class, the correlation among power output of different classes of island UDGs, and the correlation between power demands and power outputs, respectively, of island loads and UDGs.

In order to overcome the aforesaid limitations, this paper presents a new analytical expression that takes into account both load shedding and curtailment policies and, also, encompasses all the aforementioned power correlations. To do this, the proposed

^{*} Corresponding author. Tel.: +39 0957382604. E-mail address: stefania.conti@dieei.unict.it (S. Conti).

Nomenclature			
i k	load point (LP) identification index faulted branch identification index	С	class identification index, defined as a set of generators made up of unconventional DGs based on the same
$egin{aligned} \lambda_i \ U_i \end{aligned}$	LP i annual outage rate LP i annual outage duration	d	technologies distributed generator identification index, equal to the
$\lambda_{i,k}$	LP <i>i</i> annual outage rate due to a fault in branch <i>k</i>	u	number of the node at which it is connected
$U_{i,k}$	LP <i>i</i> annual outage duration due to a fault in	nu	number of UDGs in a class for a given island
.,,.	branch k	ns	number of sets, where a set is made up by the genera-
f_k	branch k failure rate (number of faults/year)		tors' power outputs of a specific island's class for a given
$t_{R,k}$	branch k repair time		period and hour (the number of data items in each set is
CBS	switch represented by a combination of circuit breaker		equal to nu : $P_{1,s}^U P_{2,s}^U, \dots, P_{nu,s}^U$
	(CB) and sectionalizer (a sectionalizer is always installed	S DUc	set identification index (a number between 1 and <i>ns</i>)
	where a CB is placed, hence when a CB is mentioned, it refers to the CB of a CBS)	$P_{cmb,s}^{U_c}$	power output of combination <i>cmb</i> for set <i>s</i> of class <i>c</i> , whose value depends on the powers of set <i>s</i> and on
j	switch (CBS or sectionalizer) identification index, equal		the generators' states combination <i>cmb</i> , where each
J	to the identification index of the branch in which it is		state is up or down
	installed (j indicates also the island created after open-	$ ho_{cmb,s}^{U_c}$	probability related to $P_{cmb,s}^{U_c}$
	ing switch <i>j</i>)	$ ho_{p,h,l}^{U_c}$	probability associated to power level <i>l</i> in the hourly gen-
PoA	probability of adequacy (it estimates the ability of local	r p,n,ı	eration model of class c, related to period p at hour h
	DGs to meet the island load)	$ ho_{d,l}^{\sf C}$	probability associated to power level <i>l</i> in the conven-
$ ho_{A,j}$	PoA of local DGs in island or (as indicates the sectional	, , , , , , , , , , , , , , , , , , ,	tional generator model of DG d
$ ho_{A,sc}$	PoA of local DGs in island <i>sc</i> (<i>sc</i> indicates the sectionalizer closest to the fault among those installed between	$ ho_{d,\ l}^{\scriptscriptstyle G}$	probability that DG d provide a power equal to level l
	CBS <i>j</i> and the fault)	N/	during the year
$t_{S,j}$	sectionalizer <i>j</i> switching time	N_j nl_{Li}	number of working points at which island j can operate number of power levels for LP i
$t_{S,sc}$	sectionalizer sc switching time	$nl_{G,d}$	number of power levels for DG d
$t_{AV,j}$	time to be available for the local DGs of island j (time	NL _i	number of LPs belonging to island <i>j</i>
	needed to reconnect the generators)	NG _i	number of DGs belonging to island j
$t_{AV,sc}$	time to be available for the local DGs of island sc	m [°]	one combination, with $m \in [1, N_j]$
np n	number of periods which the years is divided into period identification index (a number between 1 and <i>np</i> ,	$P_{j,m}^L$	total power demand in island j for the m -th combination
р	e.g. a value between 1 and 4 when the years is divided	$P_{j,m}^G$	total power output available in island j for the m -th
	into the four seasons)	J,	combination
t	day type identification index (1 stands for workday, 2	$ ho_{j,m}$	occurrence probability of the <i>m</i> -th combination
	stands for holiday and weekend)	wd _p , hd	p number of workdays (W) and holydays (H), respec-
h	hour identification index (a value between 1 and 24)	oW (tively, in period p
nl	number of power levels for the load model of an LP or	$ \rho_{A,j,p,h}^{}, \mu $	$_{Aj,p,h}^{H}$ PoA of island j , respectively, in W and H days of period p and hour h
1	the generation model of a UDGs' class	N^W , N^I	$H_{p,h}$ number of working points at which island j can oper-
l	level identification index (a number between 1 and nl)		ate at period p, hour h, in W and H days, respectively
$ ho_{i,p,t,h,l}^{L}$	probability that LP <i>i</i> absorbs an active power equal to	$P_{i,n,h,m}^{LW}, I$	$p_{j,p,h,m}^{LH}$ total power demand in island j considering the
$P_{i,p,t,h,l}$	level l , at hour h , in day t , of period p	J.)F. 111.	m-th combination at period p , hour h , in W and H days,
$ ho_{i,l}^L$	probability that LP i absorbs an active power equal to	-C	respectively
, .	level <i>l</i> during the year	$P_{j,p,h,m}^G$	total power output available in island j for the m -th
nd	data number of collected historical data, in term of	οW	combination at period <i>p</i> and hour <i>h</i>
	active power absorbed by a LP at hour h in all days of	$ u_{j,p,h,m}, u$	$o_{j,p,h,m}^H$ probability of the m -th combination at period p , hour h , in W and H days, respectively
	type t belonging to p		noar, in vv and ir anys, respectively

expression exploits hourly generation models that account for power output correlation for a class of UDGs in an island. Moreover, the proposed formulation is based on hourly load models too. From a practical viewpoint, one load model and one generation model have to be developed for each LP and each UDGs' class of an island, respectively. It is worth to note that hourly load and generation models permit to take into consideration correlation among loads, correlation among different classes of UDGs and correlation among loads and UDGs [28].

Distribution system reliability and local DGs adequacy

Typical indexes to evaluate distribution system reliability [32] can be estimated by means of the annual outage rate (λ_i) and duration (U_i) of all load points (LPs), which, respectively, are the number of outages and the total outage time in a year for the i-th LP [20]. Their value mainly depends on LP power demand and

location, DGs type, capacity and position, fault location, switches type and installation point. It is known that the following expressions can be applied in order to compute their value:

$$\lambda_i = \sum_k \lambda_{i,k} \tag{1}$$

$$U_i = \sum_{k} U_{i,k} \tag{2}$$

where $\lambda_{i,k}$ is the LP i annual outage rate due to a fault in branch k; $U_{i,k}$ is the LP i annual outage duration due to a fault in branch k.

Table 1 shows the expressions presented in [30] for all possible cases defined by the relative position of LPs, faults and switches, in networks with and without DGs for distribution systems where island operation is allowed and not allowed.

Fig. 1 and Table 2 help to understand how to identify the various cases (see [30] for more details).

Download English Version:

https://daneshyari.com/en/article/6860289

Download Persian Version:

https://daneshyari.com/article/6860289

<u>Daneshyari.com</u>