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#### Special Issue on CAD/Graphics 2017

# Optimized sequence planning for multi-axis hybrid machining of complex geometries

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#### ABSTRACT

The emerging hybrid machining platform potentiates the manufacturing of complex structures that are previously unmachinable solely by subtractive machining. The essence of such a platform is the alternation incorporating both additive and subtractive process. Multiple alternations are needed to eventually produce a complex model. The planning of the build-up height in each alternation plays a crucial role in the overall process: a large build-up height of partial construction may block the cutter from accessing the in-process part; conversely, frequent alternations will degrade the overall efficiency as well as the surface finish. In order to find a perfect balance, a metric called machinability is proposed to evaluate the subtractive machining feasibility. An efficient algorithm for calculating the machinability under the dynamic obstacle growing environment is then developed accordingly. Based on that, an efficient and deterministic top-down sequential maximization algorithm is presented that is able to minimize the number of alternations while at the same time ensuring a smooth tool path for each subtractive operation. Ample computer simulation examples are given to illustrate the effectiveness of the proposed methodology.

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#### 1 1. Introduction

Traditionally, industrial parts with complex geometries and also 2 3 high precision requirements are manufactured by a five-axis sub-4 tractive machining process out of a raw stock, which is costly and extremely time consuming since up to 80% of material has to be 5 machined off. For instance, for just finish-cut (the final cut), a sin-6 gle large blisk used in aero-engines can take days to machine. The 7 8 subtractive process is also impaired by the so-called accessibility 9 problem - any area on the workpiece surface must be accessible 10 to the tool so that it is able to contact and remove the excessive material without colliding with other parts of the workpiece or the 11 environment. For a part with slender or curvy features and narrow 12 13 cavities in between, collision is very likely to occur. This issue also limits the selection of tool and undermines the smoothness of the 14 tool alignment. 15

16 On a different note, in some applications, it is required that the 17 tool path follows a specific flow-line direction such that the left-18 over scallops comply with a specified pattern, e.g., some compo-19 nents in fluid machinery - blisks, impellers and inducers-are re-20 quired to be machined by a spiral-like tool path. This extra re-21 quirement further circumscribes the already limited tool accessible

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http://dx.doi.org/10.1016/j.cag.2017.07.018 0097-8493/© 2017 Elsevier Ltd. All rights reserved. range. To a large extent, the traditional subtractive machining process will no longer be qualified under these requirements.

Additive manufacturing can bypass all the aforementioned issues of the subtractive process. However, current additive manufacturing technologies are limited by their attainable accuracy and surface quality [1,2]. As a result, a part initially additively manufactured always needs a final finish-cutting by five-axis machining, thus still facing the same accessibility issue.

Recently, a new type of machine tool - hybrid machine tool has emerged in the market that provides an integrated platform of both additive and subtractive processing (see Fig. 1(a)). With the help of this new platform, the additive process and the subtractive process can be integrated into one embodiment [3–5]. It can be anticipated that, with a proper hybrid manufacturing process, a complex component, such as the blisk shown in Fig. 1(b), which originally cannot be machined to realize the desired tool path pattern or is very difficult to be machined at all due to the accessibility constraint, can now be manufactured with high surface quality and authenticity to the specified tool path pattern.

The most challenging issue in hybrid manufacturing is the determination of the alternating sequence  $\{A_1, S_1, A_2, S_2, \ldots, A_m, S_m\}$  42 where *A* and *S* stand for additive and subtractive, respectively. As 43 each  $A_i$  or  $S_i$  requires a new calibration and certain pre-processing 44 of the additive nozzle or the cutting tool, and for each  $S_i$  certain 45 residual material must be left underneath the top built contour 46 JID: CAG

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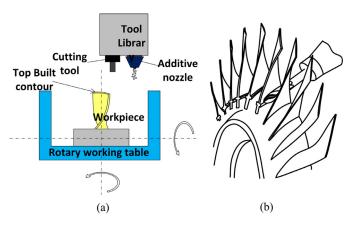


Fig. 1. (a) The typical configuration of a hybrid machine; (b) A blisk of complex shape.

of  $A_i$  (see Fig. 1(a)) so that the next build  $A_{i+1}$  can start, natu-47 rally the number "m" should be as small as possible. However, in 48 the existing literature, to the best of our knowledge, there are no 49 50 published studies addressing this so called optimal sequence plan-51 ning problem. In terms of related research, Akula and Karunakaran [6] identified the build direction as an essential parameter in plan-52 ning a hybrid process. Hu et al. [7] accessed the build direction 53 54 by taking into account the tool accessibility, the processing time 55 and the number of support structures; users can specify their cus-56 tomized requirements by changing the weights of all these factors. Ruan et al. [8] planned the hybrid process by decomposing the 57 part into non-uniform thickness slices so as to build the part more 58 59 efficiently. Similarly, a slicing direction is calculated in [9], along which the part is decomposed without overhang features, thus the 60 61 support structure is avoided. Unfortunately, none of these studies ever mentioned the sequence planning issue when dealing with 62 complex structures. Apart from these works in process planning, 63 64 other related works in this field mainly concern with the hardware 65 or controller aspects [10–12], which are unfortunately irrelevant to 66 our current issue.

One of the most critical constraints in planning an alternating 67 sequence is the aforementioned "accessibility" for subtractive ma-68 chining. Fig. 2(a) shows a part which is impossible to be manufac-69 70 tured by the traditional machining due to this accessibility constraint. However, with a hybrid process, it is possible to machine 71 the workpiece when it is partially formed, and the interference 72 is thus avoided given the fact that the potential obstacles (parts 73 of the design geometry) have not yet emerged, as illustrated in 74 75 Fig. 2(b).

It is worth mentioning that past research in the calculation
of tool accessible region in multi-axis machining is prosperous.
[13] proposed a configuration space method to map the obstacles and machine limit to a 2-D configuration space to give a
feasible tool range. Balasubramaniam [14] proposed a visibility

based method which captures the tool accessible range in 3-81 D Cartesian space. Castagnetti et al. proposed a DAO (Domain of 82 Admissible Orientation) concept to optimize the tool path [15]. 83 Gray et al. devised a rolling ball method (RBM) to avoid the global 84 gouging by positioning the tool inside the rolling ball [16]. Wang 85 and Tang [17] came up with a fast algorithm for calculating the 86 accessible region by updating the boundary of the previous one, 87 assuming the region changes smoothly along the tool path. Most of 88 these sampling based algorithms demand a considerable amount of 89 computing power to achieve an acceptable accuracy. To overcome 90 this issue, an alternative planar accessible range of tool orientation 91 was reported in [18] specifically for blisk machining, which would 92 achieve a real-time performance. Liang et al. [19] recently intro-93 duced a boundary based method for constructing an accessible 94 range, where each obstacle surface was simplified as a boundary 95 curve. Both performance and accuracy are considerably increased. 96

To eventually obtain a smooth tool path under the accessibility 97 constraint, various optimization algorithms have been proposed, 98 which can be categorized into two groups - those that work with 99 respect only to the part coordinate system [14,18,20–23] and hence are independent of the machine tool, and those that work in the machine coordinate system [17,24–26] and thus truly reflect the smoothness of the movement of the machine's axes. 103

Conceivably, if the alternating sequence is more densely layered 104 (i.e., *m* is large), each layer would have a better accessibility con-105 dition, and thus it would be easier to plan the tool orientation to 106 prevent the potential interference while maintain the smoothness 107 of the final tool path. However, as already pointed out, this bet-108 ter accessibility condition is obtained at the cost of significantly 109 increased total manufacturing time and an inferior surface finish 110 (due to dense marks at the interface between  $A_i$  and  $A_{i+1}$ ). There-111 fore, the main objective of this research is the development of an 112 algorithm that will, for an arbitrary part and a given tool, find the 113 minimum alternating sequence while maintaining sufficient tool 114 accessibility during each subtractive process  $S_i$ . 115

This paper is organized as follows. First, in Section 2, we de-116 scribe an important algebraic metric called dynamic tool accessible 117 region and its efficient computation which will be used to evalu-118 ate the machinability of layers. Afterwards, in Section 3, we present 119 our main result of the top-down sequential maximization, which 120 essentially leads to our final minimization algorithm. In Section 4, 121 several computer simulation examples are given to illustrate the 122 robustness and effectiveness of the proposed approach. Finally, we 123 conclude the paper in Section 5 with some pointers to future re-124 search. 125

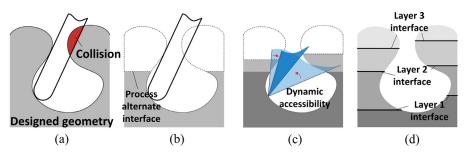
#### 2. Machinability and its calculation

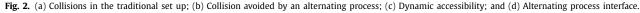
#### 2.1. Metric of machinability

As stated earlier, hybrid machining is known for its capability of 128 manufacturing parts with complex shapes or narrow gap features 129 that are basically unmachinable via traditional subtractive machin-

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