

Simulation of three-phase spouted bed reactor for solid catalyst alkylation

Roberto Galiasso Tailleur*

Department of Chemical Engineering, Texas A&M University, College Station, TX 77843-3123, USA

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Abstract

A process simulator was developed to afford better understanding of the performance of the isobutane–butene alkylation plant that uses a three-phase spouted bed-reactor hydrocyclon and a super acid solid catalyst. The system was simulated by using correlations developed in the cold model and apparent kinetic constants measured in a batch reactor for 1-butene–isobutene alkylation. A new type of catalyst, $\text{PtSO}_4\text{Zr/TiO}_2$, was used in the presence of recycled alkylate and hydrogen. The computer simulator numerically solved the mass and energy balance equations for the riser and downcomer. It was determined that a gas–liquid–solid with similar properties to the system under study do not shown a charm regime of flow and that the new design of the gas disengaging zone at the end of the riser prevent the undesired recirculation of large bubble and provide stability. New gas hold-up, linear velocity of the liquid, recycle ratio, and mass transfer correlations obtained reproduce the result within a $\pm 10\%$ error. The result of the alkylation plant simulation indicated a large influence of linear velocity and temperature on activity, selectivity, and stability of catalytic system. The other important operating parameters are alkylate/olefin and isobutane/olefin ratios. The optimal operating conditions were determined for a particular catalyst and set of cost.

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1. Introduction

The development of an alkylation process that uses a solid catalyst is one of the most challenging activities in efforts to improve the production process of a “green” gasoline component. Currently commercial alkylation of olefins is done using strong acids (HF and H_2SO_4) with good selectivity and activity but generating or a toxic sludge (H_2SO_4) or having strong safety limitations (HF). The development of an active and stable solid super acid alkylation catalyst will introduce interesting technical and economical possibilities and represent a big challenge. Weitkamp and Traa [1] has reviewed the state of the art in solid alkylation; since then there have been many contributions in this area. In this research, we used different catalyst formulations base on a wide porous Si-based mesoporous material in which Pt and ZrSO_x species were present on the surface. In previous work [2], a kinetics model was developed using

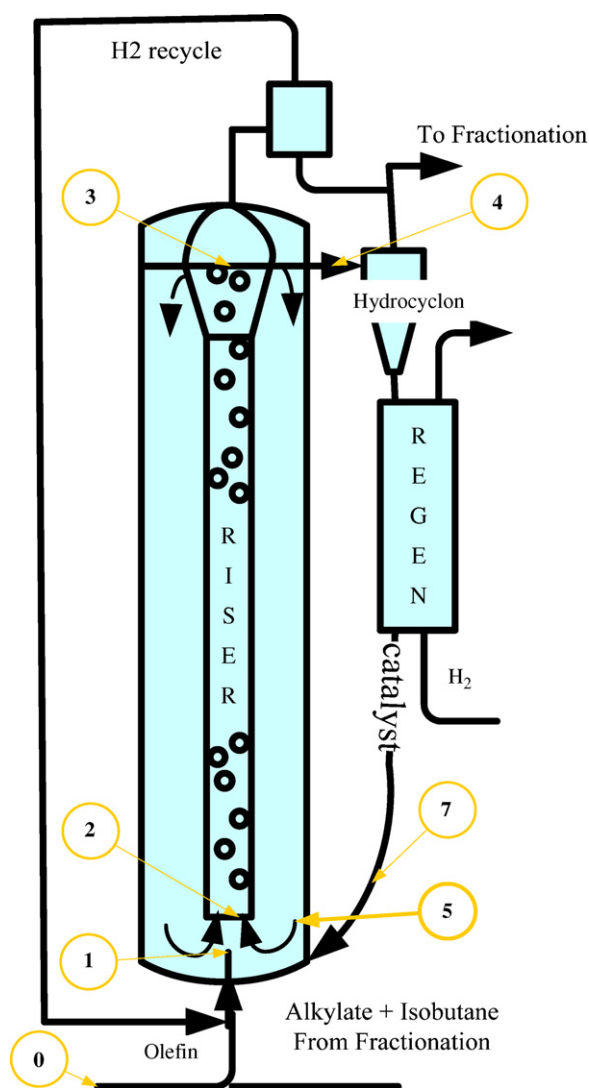
this type of catalyst for olefin–isobutane alkylation in the presence of hydrogen. We studied the application of this catalyst in a slurry-type reactor hydrocyclon coupled with a fluidized-bed regenerator. The simulation of a slurry reactor was recently summarized by De Jong et al. [3] and by Ramswamy et al. [4]. Our present research focuses on the use of three-phase spouted bed hydrocyclon instead of slurry reactor [5] technology.

1.1. Process description

In this alkylation process (Fig. 1), the feeds comprise a liquid phase composed of olefins, isobutene and alkylate, and a hydrogen-rich gas stream that comes into the bottom of the reactor (see callout 1, Fig. 1). Gas and liquid phase are internally contacted with a solid super acid catalyst coming from the regenerator (7, Fig. 1). At the inlet (1), fresh feeds are combined with those internally recycled through the downcomer (5). All components enter into the riser where they move upward. The gas is stripped from the reacting mixture at the top of the reactor where it is cooled and separated at high pressure. From the top of this separator the gas (mainly H_2) is recycled to the inlet of the

* Tel.: +1 979 218 1903; fax: +1 979 845 6446.

E-mail address: galiasso@cantv.net.



The cold model consists in a 0.4 m diameter and 3.5 m tall metallic reactor, with a 0.16 m internal riser and 0.04 m inlet liquid nozzle diameter, connected to a 0.18 m diameter hydrocyclon. The riser ends up in an enlarged degassing zone (cone of 0.35 m height and 60° angle). The basic configuration can be seen in Fig. 2. The octane is continuously fed to the reactor into a conical bottom, and the gas (air + 10% of CH₄) is distributed inside the riser inlet zone. The gas is injected at 0.1 m above the bottom of the draft tube by means of a parallel set of five tubes of 0.002 m internal diameter and 0.05 m length. The liquid-containing solid is withdrawn from the upper part and

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