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Robust residual-based a posteriori Arnold–Winther mixed finite element analysis in elasticity^{*}

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Dedicated to Professor Ivo Babuška

Abstract

This paper presents a residual-based a posteriori error estimator for the Arnold–Winther mixed finite element that utilises a post-processing for the skew-symmetric part of the strain. Numerical experiments verify the proven reliability and efficiency for suitable approximation of the skew-symmetric deformation gradient. Numerical evidence supports that the L^2 -stress error estimator is robust in the Poisson ratio and allows stable error control even in the incompressible limit. (© 2015 Elsevier B.V. All rights reserved.

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1. Introduction

The problem in linear elasticity considers the connected reference configuration of the elastic body $\Omega \subset \mathbb{R}^2$ with polygonal boundary $\partial \Omega = \Gamma_D \cup \Gamma_N$ with closed and connected Γ_D of positive surface measure and $\Gamma_N = \partial \Omega \setminus \Gamma_D$ for applied tractions. Given a volume force $f : \Omega \to \mathbb{R}^2$, a displacement $u_D : \Gamma_D \to \mathbb{R}^2$, and a traction $g : \Gamma_N \to \mathbb{R}^2$, find a displacement $u : \Omega \to \mathbb{R}^2$ and a stress tensor $\sigma : \Omega \to \mathbb{S} := \{\tau \in \mathbb{R}^{2 \times 2} : \tau = \tau^T\}$ such that

$$-\operatorname{div} \sigma = f, \quad \sigma = \mathbb{C}\varepsilon(u) \quad \text{in } \Omega,$$

$$u = u_D \quad \text{on } \Gamma_D, \quad \sigma v = g \quad \text{on } \Gamma_N.$$
 (1.1)

Throughout this paper, \mathbb{C} denotes the bounded and positive definite fourth-order elasticity tensor for isotropic linear elasticity. The symmetric mixed finite element method is a very popular choice for a robust stress approximation; cf. [1–6] for details and related references.

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The a posteriori error analysis for the Arnold–Winther finite element method may follow the ideas of [7–9] to derive a stress error control

$$\|\sigma - \sigma_{AW}\|_{\mathbb{C}^{-1}}^2 \le \min_{v \in V} \|\mathbb{C}^{-1}\sigma_{AW} - \varepsilon(u_D + v)\|_{\mathbb{C}}^2 + C_1 \operatorname{osc}^2(f, \mathcal{T}) + C_2 \operatorname{osc}^2(g, \mathcal{E}(\Gamma_N))$$

for the stress error $\sigma - \sigma_{AW}$ even with a rather explicit estimate of the constant in front of the oscillations and the (unwritten) multiplicative constant 1 in front of the first term that measures the quality of the approximation $\mathbb{C}^{-1}\sigma_{AW}$ of symmetric gradients $\varepsilon(v) := (Dv + D^T v)/2$ for $v \in V$. The space V consists of all square-integrable displacements with homogeneous boundary conditions along Γ_D and with a square-integrable functional matrix Dv.

A severe additional difficulty of this approximation is that only the symmetric part is approximated and not the full gradient Dv so that [9] cannot be applied for a residual-based a posteriori error estimation of the aforementioned first term. Other mixed finite element schemes like PEERS in [7] involve some additional variable to approximate the asymmetric part of the gradient. This paper presents an explicit error estimate which involves an arbitrary asymmetric approximation γ_h and provides an abstract a posteriori error control of the residual type, which is useful for adaptive mesh-refining algorithms,

$$\begin{aligned} \eta_{\ell}^{2} &= \operatorname{osc}^{2}(f, \mathcal{T}) + \operatorname{osc}^{2}(g, \mathcal{E}(\Gamma_{N})) + \sum_{T \in \mathcal{T}} h_{T}^{2} \|\operatorname{curl}(\mathbb{C}^{-1}\sigma_{AW} + \gamma_{h})\|_{L^{2}(T)}^{2} \\ &+ \sum_{E \in \mathcal{E}(\Omega)} h_{E} \|[\mathbb{C}^{-1}\sigma_{AW} + \gamma_{h}]_{E} \tau_{E} \|_{L^{2}(E)}^{2} + \sum_{E \in \mathcal{E}(\Gamma_{D})} h_{E} \|(\mathbb{C}^{-1}\sigma_{AW} + \gamma_{h} - Du_{D})\tau\|_{L^{2}(E)}^{2}. \end{aligned}$$

(The details on the standard notation can be found below for computable volume contributions on a triangle T of diameter h_T and various jumps across an edge E of length h_E .) For any (piecewise smooth) choice of γ_h , this a posteriori error estimator is reliable in the sense that

$$\|\sigma - \sigma_{AW}\|_{\mathbb{C}^{-1}} \le C_{\text{rel}}\eta_{\ell} \tag{1.2}$$

with some λ -independent constant $C_{\text{rel}} \approx 1$. One opportunity to ensure efficiency is a global minimisation over all piecewise polynomial γ_h of the error estimator η_ℓ . The bubble function technique shows that the particular choice of γ_h enters the efficiency estimates with some λ -independent constant $C_{\text{eff}} \approx 1$,

$$\eta_{\ell} \leq C_{\text{eff}} \left(\|\sigma - \sigma_{\text{AW}}\|_{\mathbb{C}^{-1}} + \|\text{skew}(Du) - \gamma_h\|_{L^2(\Omega)} \right).$$

$$(1.3)$$

Hence, one efficient choice for γ_h is to choose it as a sufficiently accurate polynomial approximation of the asymmetric gradient skew $(Du) := (Du - D^T u)/2$. Since a global approximation or even minimisation may be too costly, this paper proposes to apply a post-processing step to compute such a sufficiently accurate approximation $\gamma_h = \text{skew}(Du_{AW}^*)$ for the post-processed displacement u_{AW}^* in the spirit of Stenberg [10]. The approximation $\gamma_h = \text{skew}(Du_{AW}^*)$ is proven to be robust in the Poisson ratio $v \to 1/2$ for sufficiently smooth functions. For domains with re-entrant corners or incompatible boundary conditions, numerical experiments confirm that the proposed computation of γ_h leads empirically to reliable and efficient a posteriori error control independent of the Poisson ratio $v \to 1/2$.

The remaining parts of this paper are organised as follows. In Section 2 the notation, the weak formulation of (1.1) and the Arnold–Winther finite element space [1] are defined. Section 3 derives the a posteriori error analysis for the residual-based a posteriori error estimator and proves reliability and efficiency. Section 4 outlines a post-processing of the displacement that leads to an approximation γ_h of the asymmetric gradient. Section 5 presents numerical results of four benchmark problems that verify reliability and efficiency of the residual-based a posteriori error estimator in combination with the post-processing and illustrates its robustness for Poisson ratio $\nu \rightarrow 1/2$.

The main parts of this research are restricted to 2D because the Argyris finite element method is employed to allow for a quasi-interpolation in the Arnold–Winther finite element functions.

2. Preliminaries

For
$$v = (v_1, v_2) \in \mathbb{R}^2$$
 and $\tau = (\tau_{jk})_{j,k=1,2} \in \mathbb{R}^{2 \times 2}$, set

$$\operatorname{Curl}(v) \coloneqq \begin{pmatrix} \frac{\partial v_1}{\partial y} & -\frac{\partial v_1}{\partial x} \\ \frac{\partial v_2}{\partial y} & -\frac{\partial v_2}{\partial x} \end{pmatrix}, \quad \operatorname{curl} \tau \coloneqq \begin{pmatrix} \frac{\partial \tau_{12}}{\partial x} & -\frac{\partial \tau_{11}}{\partial y} \\ \frac{\partial \tau_{22}}{\partial x} & -\frac{\partial \tau_{21}}{\partial y} \end{pmatrix}, \quad \operatorname{div} \tau \coloneqq \begin{pmatrix} \frac{\partial \tau_{11}}{\partial x} & +\frac{\partial \tau_{12}}{\partial y} \\ \frac{\partial \tau_{22}}{\partial x} & +\frac{\partial \tau_{22}}{\partial y} \end{pmatrix}.$$

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