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Nickel electroplating for high-resolution nanostructures

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41 1. Introduction

 Presently, the applications of thin-film nickel (Ni) layers are wide-ranging. The electroplating process is an effective method for obtaining Ni thin films or micro- and nanostructures with good film quality and aspect ratio. Reported applications include fabrication of durable moulds for nano-imprint lithography [\[1\]](#page--1-0) and the alteration of a compound's magnetic properties for Ultra- Large-Scale Integration (ULSI) technology products, such as high- density recording systems [\[2\]](#page--1-0). Nickel films are increasingly being 50 used in the fabrication of lithography masks $[3,4]$. Ni is also an attractive material for diffractive optical elements for soft X-rays. In this energy range, Ni provides a phase shift and thereby enables fabrication of efficient diffractive optical elements such as gratings and Fresnel zone plates [\[5–7\]](#page--1-0). Fresnel zone plates with 20 nm 55 outer zone width, although rough, have been shown $[8]$. For these applications, not only smoothness of Ni, but also its stress is decisive, since these optical elements are fabricated on thin mem-branes which cannot withstand high mechanical stress.

 The specific aim of this study was to optimise the Ni deposition process in order to use Ni gratings for interference lithography at the wavelength range of extreme ultra violet (EUV). In interference lithography the interference pattern is obtained from the diffracted

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ABSTRACT

We present optimisation of a nickel electroplating process in order to obtain high-resolution nanostruc-
28 tures. Film stress and roughness were minimised and the deposition rate was well controlled at \sim 36 nm/ $\,$ 29 $\,$ min with optimised parameters of current density, pulse period, and duty cycle. The thickness uniformity 30 of the film was measured to be within 5% across the 9 mm² sample with an R.M.S. roughness of \sim 4 nm. 31 We further demonstrate electro-deposition of nano-sized lines and pillars using these parameters. Struc- 32 tures showed good resolution and uniformity down to 20 nm while pillars of 70 nm diameter with aspect 33 ratios up to 1:10 were fabricated. This process is currently being used in the fabrication of high quality 34 EUV interference lithography transmission masks in our group, and could be used in future research 35 and applications such as wire grid polarisers, Fresnel zone plates, and plasmonics. 36

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beams of gratings $[9,10]$. Since the interference pattern is formed 63 between the gratings, the incident light between the gratings must 64 be effectively blocked. Typically, this is done with a 400 nm thick 65 Au film $[9]$. However, Ni has an attenuation length of roughly 66 two-thirds that of Au at the EUV wavelength of 13.5 nm [\[11,12\].](#page--1-0) 67 Therefore, in order to obtain the same level of attenuation, a thin- 68 ner layer of Ni would be required. Consequently, the mask on 69 which the Ni layer is being deposited would experience less stress, \qquad 70 resulting in higher mask durability. Moreover, Ni gratings can be 71 used as an effective grating with relatively low thicknesses due 72 to their short attenuation length at EUV wavelength. Their short attenuation length at EUV wavelength.

In order for this Ni layer to perform satisfactorily, its quality, as 74 well as that of its fabrication procedure, must be ensured. The 75 parameters that were identified to be the most essential were uni- 76 formity of deposit and film stress. A lack of the former would result 77 in a poor and inconsistent fabrication process, while if the stress 78 experienced is too large, it would lead to mask failure. The final 79 parameter that needs to be analysed in depth is the deposition rate. 80 Knowledge of the Ni growth rate is essential in order to be able to 81 accurately and reproducibly deposit the desired metal thickness. 82 Here we report on an extensive optimisation of Ni electroplating 83 which provides fabrication of Ni nanostructures with low 84 roughness and stress and high resolution. These results enable 85 realisation of diffractive optical elements for EUV and soft X-ray 86 ranges as well as Ni nanostructures for various applications with 87 increased resolution, quality, and stability. 88

2 K. Hili et al. / Microelectronic Engineering xxx (2015) xxx–xxx

89 2. Methodology and results

21 February 2015

90 2.1. Experimental setup and sample preparation

 Various Ni deposition techniques have been documented, with the most common being electroplating [\[14\],](#page--1-0) electroforming [\[1\]](#page--1-0) 93 and electroless-plating $[15]$. In an electroplating setup, such as 94 the one shown in Fig. $1(a)$, a current is passed from an anode to a cathode through an electrolyte causing the dissociated metal ions to gain electrons and oxidise on the surface of the cathode, thereby forming a metallic coating. Electroforming is most useful when the deposit needs to be separated from the cathode base. On the other hand, electroless-plating tends to result in the deposition of a com- pound which, in the case of Ni, is usually between 90% and 98% Ni. 101 In contrast, electroplating always deposits over 99% Ni [\[16\]](#page--1-0) and allows for greater control over the process since it depends on the current forced through the electrolyte. Owing to these advan- tages, electroplating is mostly preferred to other Ni deposition techniques.

 Previous work on nickel electroplating showed that nickel deposition rate varies for different locations on the sample, which can be controlled through use of pulsed and pulse reverse plating [\[7\]](#page--1-0). Luo et al. [\[13\]](#page--1-0) performed a detailed study of thin film nickel electroplating, showing the relationship between stress and 111 temperature, with an optimal temperature of \sim 60 °C. This led to the conclusion that temperature control and relaxation through current pulsing was essential for low stress, and an optimal current 114 density of 2 mA/cm² gave stress-free thin films.

As previously mentioned, the electrical current input provides 115 control over the process. In the present study, we used a power 116 supply (Plating Electronic, PE86CB) which is capable of producing 117 stable unipolar rectangular pulses through a control feedback loop. 118 In this study we investigate all three of the current waveform's 119 variable parameters, namely the current amplitude, the duty cycle, 120 and the pulse time (i.e., waveform period). 121

In order to obtain reliable and repeatable results, the electro- 122 plating bath's operating conditions had to be monitored and 123 maintained as stable and as consistent as possible. The operating 124 conditions of the nickel sulphamate electrolyte solution $(185 \text{ g/L}$ 125 concentration, pH 3.0, 57 \degree C) are in line with those recommended 126 by the supplier (Enthone Inc.). The magnetic stirrer, as seen in 127 Fig. $1(a)$, serves to maintain an even ion distribution throughout 128 the whole bath, thereby maximising deposit uniformity. 129

Apart from the current waveform and the bath operating condi-
130 tions, the process is also dependent on the cathode's conductive 131 area. For this reason, an 18×30 mm dummy Si wafer was intro- 132 duced. In this way, changes in the sample's area are negligible 133 and the current density is kept constant for different samples. 134 The samples consisted of Si chips and 100 nm thick $Si₃N₄$ 135 membranes with a 25 nm Au seed layer on top of a 5 nm Cr adhe-
136 sion layer $[17]$. The Si dummy was coated with a 20 nm Au seed 137 layer. The patterned Cr/Au bilayer was fabricated by spin-coating 138 PMMA 950k (4% wt. in Ethyllactate, AR-P 679.04) at 2500 rpm, fol- 139 lowed by post application bake, e-beam exposure, development, 140 metal evaporation, and lift-off in acetone to remove the PMMA. 141 For fabrication of nickel nanostructures, the PMMA was applied 142

Fig. 1. (a) Schematic of the electroplating setup. (b) Testing sample design used for characterisation purposes. (c) Testing sample design used for fabrication of a line pattern with variable widths.

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