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Efficient and noise-resistant parameter estimation method for maneuvering targets in stepped frequency radar

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ABSTRACT

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Keywords: Stepped frequency (SF) radar Cubic phase (CP) signal Parameter estimation Recursive delay correlation transform (RDCT) In this paper, a novel efficient parameter estimation method is proposed for maneuvering targets based on the stepped frequency radar. Since the envelope migration can be represented by the exponential phase variance with respect to range frequency, the received echoes are first converted into the range frequency domain and modeled as cubic phase (CP) signals. Then, a new correlation transform, referred to as recursive delay correlation transform (RDCT), is defined and applied to estimate the parameters of maneuvering targets. Since RDCT is simple and only requires the fast Fourier transform (FFT) and the nonuniform FFT (NUFFT), the searching operation is unnecessary and the computational cost is significantly reduced. Compared to the other four representative methods, the proposed RDCT-based method has no error propagation and can greatly improve the anti-noise performance on the premise of retaining the computational efficiency, achieving a good balance between the computational complexity and estimation performance. Theoretical analyses of anti-noise and anti-aliasing performance, and several simulation results verify the effectiveness of the proposed parameter estimation method.

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1. Introduction

With the development of modern radar technology in both military and civil fields, improving the resolution has been receiving more and more attentions. The study on forming the highresolution signal waveforms and the corresponding signal processing methods has important significance for the high-accuracy detection, multi-targets identification and multi-targets imaging. Generally, widening the signal bandwidth and lengthening the coherent processing interval (CPI) are common approaches to achieve high-resolution range and velocity measurements. Due to the disadvantages of the high sampling rate, large data storage and high hardware cost, synthesizing a large bandwidth is preferable to directly transmitting a conventional wideband signal and has become one of the most important trends in the field of highresolution radar system design [1]. Since stepped frequency (SF) waveforms can synthesize a very wide frequency bandwidth with narrow bandwidth transmitter and receiver, they are widely used in high-resolution radar system (such as synthetic aperture radar (SAR) imaging, inverse SAR (ISAR) imaging, etc.) [2,3].

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It is well known that the "stretch" processing method [3,4] based on the inverse discrete Fourier transform (IDFT) is widely used in the SF radar. It can obtain high range resolution profiles (HRRPs) with narrow instantaneous bandwidth and low system complexity. However, the "stretch" processing method is highly sensitive to the target motion, and thus it is inappropriate for the maneuvering targets. As for the maneuvering targets with complex motion, the existence of relative motion parameters between radar and targets inevitably induces envelope migration (EM) and Doppler frequency spread (DFS) terms. These factors degrade the focusing quality of HRRPs, resulting in the resolution descending and performance deterioration for the detection and estimation. Therefore, for detecting and estimating the maneuvering targets with complex motion in the SF radar, it is quite important to precisely compensate the EM and DFS terms.

For the EM compensation, many effective methods have been presented, including envelope correlation [5,6], keystone transform [7–9], Radon transform [10] and entropy minimization algorithm [11,12], etc. The envelope correlation compensates the EM based on the estimated velocity obtained from correlation operation. Thus, it is limited to the high signal-to-noise ratio (SNR) environments. Keystone transform can compensate the EM via scaling operation without any prior kinetic information of targets and is suitable for the low SNR circumstances. However, it performs poorly in the situation of existing velocity ambiguity [9]. Although Radon transform and entropy minimization algorithm can deal with the

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velocity ambiguity, they are implemented by the searching operation, bringing heavy computational load.

3 For the DFS terms compensation, the straightforward way is to 4 construct the compensation function based on the accurately es-5 timated parameters. Generally speaking, the uniformly accelerated 6 motion is accurate enough to describe the motion characteristics 7 of maneuvering targets. In the SF radar, the acceleration of the tar-8 get contributes to a quadratic phase term and a cubic phase term. 9 Thus, the azimuth echoes should be modeled as the cubic phase 10 (CP) signals. Recently, with regard to the parameter estimation of 11 CP signals, many methods have been proposed, and they generally 12 fall into two categories: methods based on correlation and meth-13 ods without correlation. Most typical methods based on correla-14 tion include product high order ambiguity function (PHAF) [13], 15 product high-order match phase transform (PHMT) [14], product 16 generalized cubic phase function (PGCPF) [15], TC-dechirp Clean 17 [16] and higher order ambiguity function-integrated cubic phase 18 function (HAF-ICPF) [17], etc. The essence of these methods is to 19 reduce the order of CP signals via multilinear or bilinear operators, 20 then the estimated parameters are obtained via Fourier transform 21 or one-dimensional search. However, they are prone to the low 22 resolution and high SNR threshold problems. The maximum likeli-23 hood algorithm [18] and the discrete chirp Fourier transform [19] 24 belong to the category of methods without correlation. Although 25 these methods achieve good performance in the low SNR envi-26 ronments, the required multi-dimensional search consumes heavy 27 computational burden.

28 Recently, in order to compensate EM and DFS terms simulta-29 neously, several detection and estimation methods for the ma-30 neuvering targets have been proposed, such as, Radon-Fourier 31 transform/Generalized Radon-Fourier transform (RFT/GRFT) [20, 32 21], Radon Lv's distribution (RLVD) [22] and phase differentiation-33 RLVD (PD-RLVD) [23,24], etc. RFT/GRFT are typical likelihood ratio 34 test detectors and achieve optimal estimation performance, but 35 the ergodic search in them will inevitably introduce huge com-36 putational complexity. To reduce the computational complexity, a 37 fast implementation based on particle swarm optimization (PSO) 38 has been presented in [25], but it is sensitive to the set of initial 39 parameters and may converge to the local optimal maximum, re-40 sulting in performance degradation. By calculating the LVD along 41 the trajectory of the target, RLVD and PD-RLVD can jointly elim-42 inate EM and DFS and coherently accumulate the energy on the 43 two-dimensional (2D) frequency plane. LVD is free of searching 44 and only requires the 2D Fourier transform over a scaled time-45 lag instantaneous autocorrelation function [26], which significantly 46 reduces the computational complexity. However, matching the tra-47 jectory of the target requires large quantities of searching calcula-48 tions, which would lead to a heavy computational burden.

49 Drawing lessons from the current parameter estimation meth-50 ods for the maneuvering targets and considering the tradeoff be-51 tween the computational complexity and the anti-noise perfor-52 mance, we propose a search-free and noise-resistant parameter 53 estimation method based on a novel defined correlation transform, 54 referred to as RDCT. In the proposed method, the received echoes 55 are first converted into the range frequency domain to eliminate 56 the EM and modeled as CP signals. Then, the defined RDCT is 57 applied to directly estimate the motion parameters. The imple-58 mentation of RDCT only requires FFT and NUFFT, which help avoid 59 brute-force search, and thus the computational cost is saved. Fur-60 thermore, the analyses of cross terms, anti-noise performance and 61 anti-aliasing performance demonstrate that the proposed method 62 is appropriate for the situation of multiple targets with ambigu-63 ous velocities and it can acquire higher anti-noise performance 64 compared to PHMT, HAF-ICPF and TC-dechirp Clean. Through the 65 simulations for synthetic models, we validate the effectiveness of 66 the proposed method.

67 The remainder of this paper is organized as follows. In Section 2, we establish the signal model of maneuvering targets in the 68 69 SF radar. In Section 3, we introduce the principle of the proposed parameter estimation method based on the novel defined RDCT 70 71 and discuss the influence of cross terms. In Section 4, we theoretically analyze the computational cost, anti-noise performance and 72 anti-aliasing performance of the proposed method and specifically 73 74 discuss the differences from the LVD-based methods. In Section 5, 75 simulations with synthetic radar data are carried out and the con-76 clusions are drawn in Section 6.

2. Signal model

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Assume that the transmitted signal in the SF radar is

$$S_T(\tau_r, t_m) = u(\tau_r) \exp\left[j2\pi f_c(m)(\tau_r + t_m)\right]$$
(1)
⁸²
⁸³

where τ_r is the fast time (range time), $t_m = mT_r$ is the slow time (azimuth time) with T_r denoting the pulse duration time (PRT), $0 \le m \le M - 1$ denoting the pulse index and M denoting the number of pulses within a CPI. $u(\tau_r)$ is the transmitted waveform. $f_c(m) = f_c + m\Delta f$ is the carrier frequency of the *m*th pulse where f_c is the initial carrier frequency and Δf is the frequency step size.

Suppose that there are K moving targets in the scene. For the wideband transmitted signal, the baseband received echoes can be expressed as [27,28]

$$S_B(\tau_r, t_m) = \sum_{k=1}^{K} \sqrt{\kappa_k} \sigma_k u \left(\kappa_k \left(\tau_r - \frac{2R_k(t_m)}{c - \nu_k} \right) \right)$$

$$gamma = \sum_{k=1}^{K} \sqrt{\kappa_k} \sigma_k u \left(\kappa_k \left(\tau_r - \frac{2R_k(t_m)}{c - \nu_k} \right) \right)$$

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$$x \exp\left[-j4\pi f_c(m)\frac{R_k(t_m)}{c+\nu_k}\right]$$
(2) 98
99

$$t \exp\left[-j4\pi f_c(m)\frac{v_k \tau_r}{c+v_k}\right]$$

where σ_k is the backscattering coefficient of the *k*th target. $\kappa_k = \frac{c-v_k}{c+v_k}$ is the scale factor of the *k*th target with v_k and *c* denoting the radial velocity of the *k*th target and the speed of light, respectively. $R_k(t_m)$ is the instantaneous range between radar and the *k*th target. The last term in (2) is the intra-pulse Doppler. Obviously, it varies with $f_c(m)$ and results in the range-Doppler coupling. To compensate this coupling term, the wideband matched filter (WFM) [27] is performed on the received echoes and the results are given by

$$S_M(\tau_r, t_m) = \sum_{k=1}^{K} \kappa_k \sigma_k p\left(\kappa_k \left(\tau_r - \frac{2R_k(t_m)}{c - \nu_k}\right)\right)$$
¹¹²
¹¹³
¹¹⁴
¹¹⁴
¹¹⁴

$$\sum_{k=1}^{k=1} \left(\left(\left(C - V_k \right) \right) \right)$$

$$\times \exp\left[-i4\pi f_k(m) \frac{R_k(t_m)}{2} \right]$$
(3)

$$\times \exp\left[-j4\pi f_c(m)\frac{\kappa_k(t_m)}{c-\nu_k}\right]$$
¹¹⁶
¹¹⁷
¹¹⁸

where $p\left(\kappa_k\left(\tau_r - \frac{2R_k(t_m)}{c - \nu_k}\right)\right) = \int \left|u\left(\kappa_k\left(\tau_r - \frac{2R_k(t_m)}{c - \nu_k}\right)\right)\right|^2 d\tau_r$. Under the assumption of $|\nu_k|/c \ll 1$, we have $\kappa_k \approx 1$ and $c - \nu_k \approx c$. Thus, (3) can be further simplified as

$$S_M(\tau_r, t_m) \approx \sum_{k=1}^K \sigma_k p \left(\tau_r - \frac{2R_k(t_m)}{c} \right) \exp\left[-j4\pi f_c(m) \frac{R_k(t_m)}{c} \right]$$
(4)

Usually, the uniformly accelerated motion is accurate enough to describe the moving characteristics of the maneuvering targets. Thus, $R_k(t_m)$ can be expressed as

$$R_k(t_m) = R_{0k} + v_k t_m + \frac{1}{2} a_k t_m^2$$
(5)

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