



## Brief paper

# Distributed formation tracking of networked mobile robots under unknown slippage effects<sup>☆</sup>

Sung Jin Yoo<sup>a</sup>, Tae-Hyoung Kim<sup>b,\*</sup><sup>a</sup> School of Electrical and Electronics Engineering, Chung-Ang University, 84 Heukseok-Ro, Dongjak-Gu, Seoul 156-756, Republic of Korea<sup>b</sup> School of Mechanical Engineering, Chung-Ang University, 84 Heukseok-Ro, Dongjak-Gu, Seoul 156-756, Republic of Korea

## ARTICLE INFO

## Article history:

Received 8 May 2014

Received in revised form

24 November 2014

Accepted 19 January 2015

Available online 17 February 2015

## Keywords:

Adaptive formation tracking

Collision avoidance

Networked mobile robots

Skidding and slipping

Directed graph

## ABSTRACT

A distributed formation tracking problem considering collision avoidance among robots is investigated for a class of networked mobile robots with unknown slippage effects. The position information of the leader robot is time-varying and accessible to only a small fraction of the follower robots. The skidding and slipping effects are considered in the kinematics and dynamics of multiple mobile robots and assumed to be unknown, together with the matrices of the robot dynamics. A distributed recursive design methodology using the function approximation technique is derived to design each follower robot's local controller with collision avoidance ability under directed networks. The main difficulty of this design is deriving the adaptive compensation laws of unknown slippage effects in order to achieve both formation tracking and collision avoidance by using one local controller for each follower under limited communication links. The boundedness of all signals in the networked closed-loop system and guaranteed collision avoidance among robots are established through Lyapunov stability analysis.

© 2015 Elsevier Ltd. All rights reserved.

## 1. Introduction

Recursive and systematic design approaches such as backstepping (Krstic, Kanellakopoulos, & Kokotovic, 1995) and dynamic surface design (Swaroop, Hedrick, Yip, & Gerdes, 2000) have been widely used to design control systems of mobile robots at the dynamic level (see Do, Jiang, & Pan, 2008, Dong & Kuhnert, 2005, Fukao, Nakagawa, & Adachi, 2000, Jiang & Nijmeijer, 1997, and the references therein). These previous works generally disregarded slippage effects which should be considered in practical applications. Thus, significant research activities in modeling and control methodologies have been proposed in the presence of wheel skidding and slipping (Low & Wang, 2008; Wang & Low, 2008). To deal

with unknown skidding and slipping, an adaptive tracking control approach was proposed for single mobile robots at the dynamic level (Yoo, 2010). In Yoo and Park (2013), a formation controller using a virtual structure (Do & Pan, 2007) was designed for multiple robots with slippage effects. However, this method has two restrictions: (i) each robot needs all robots' information to update its own state because of an inherent property of virtual structure approach; and (ii) the collision avoidance problem among robots is not considered.

Distributed consensus problems using the graph theory have received a great deal of attention from the control community due to the consideration of limited communication among agents. (See, for instance Hou, Cheng, & Tan, 2009, Liu, Chen, & Lu, 2009, Mei, Ren, & Ma, 2012, Olfati-Saber, Fax, & Murray, 2007, Ren & Beard, 2008, Su, Chen, Wang, & Lin, 2011, Yu, Chen, Cao, & Kurths, 2010, and the references therein). Meanwhile the collision avoidance problem among nonlinear agents with a lack of shared information has not been addressed. Besides, there are no other any research results on the distributed formation tracking and collision avoidance in the presence of slippage effects connected with nonlinearities unmatched in control inputs.

Motivated by these observations, this paper investigates a distributed formation tracking and collision avoidance problem of networked mobile robots with unknown slippage effects. The information of a time-varying leader robot is only available to a

<sup>☆</sup> This research was supported by the MSIP (Ministry of Science, ICT and Future Planning), Korea, under the ITRC (Information Technology Research Center) support program (NIPA-2014-H0301-14-1044) supervised by the NIPA (National ICT Industry Promotion Agency) and by Basic Science Research Program through the National Research Foundation of Korea (NRF) funded by the Ministry of Education, Science and Technology (2012R1A1A1001440 and 2012-012295). The material in this paper was not presented at any conference. This paper was recommended for publication in revised form by Associate Editor Yoshihiko Miyasato under the direction of Editor Toshiharu Sugie.

\* Corresponding author.

E-mail addresses: [sjyoo@cau.ac.kr](mailto:sjyoo@cau.ac.kr) (S.J. Yoo), [kimth@cau.ac.kr](mailto:kimth@cau.ac.kr) (T.-H. Kim).

subset of follower robots. A distributed dynamic surface design methodology using the adaptive function approximation technique is derived to design the potential-function-based local controller using only neighbors' information under directed networks. The contributions of this paper are three-fold: (i) compared with the existing literature, the distributed collision avoidance problem in the presence of limited communication links is considered for networked nonlinear mobile robots for the first time; (ii) adaptive laws for compensating unknown slippage effects are derived to achieve both distributed formation tracking and collision avoidance by using one local controller to each follower robot in directed networks; and (iii) information on all matrices of the robot dynamics and all slippage effects is not required to implement the proposed control system. The stability of the controlled closed-loop system is analyzed through Lyapunov stability theorem.

## 2. Problem formulation

### 2.1. Graph theory notions

Let  $\mathcal{G} \triangleq (\mathcal{V}, \mathcal{E})$  be a directed graph with the set of nodes or vertices  $\mathcal{V} \triangleq \{1, \dots, M\}$  and the set of edges or arcs  $\mathcal{E} \subseteq \mathcal{V} \times \mathcal{V}$ . An edge  $(j, i) \in \mathcal{E}$  means that agent  $i$  can obtain information from agent  $j$ , but not vice versa where  $j$  and  $i$  are the parent node and child node, respectively. The set of neighbors of a node  $i$  is  $\mathcal{N}_i = \{j | (j, i) \in \mathcal{E}\}$ , which is the set of nodes with edges incoming to node  $i$ . A directed path from node  $i_1$  to node  $i_k$  is a sequence of edges of the form  $(i_1, i_2), (i_2, i_3), \dots, (i_{k-1}, i_k)$  in a directed graph. A directed tree is a directed graph where every node has one parent except for the root and the root has directed paths to every other node. A directed graph has a directed spanning tree if there exists at least one agent that has directed paths to all other agents.

### 2.2. Kinematics and dynamics of networked mobile robots in the presence of slippage effects

Suppose that there exist  $M$  followers, labeled as agents 1 to  $M$ , and a leader, labeled as an agent 0 under a directed graph topology. A group of the followers consists of  $M$  wheeled mobile robots in the presence of the wheel's skidding and slipping described by Yoo (2010)

$$\begin{aligned} \dot{q}_i &= J_i(q_i)(z_i - \xi_i) + \varphi_i(q_i, \mu_i), \\ \tau_i &= H_i(\dot{z}_i - \dot{\xi}_i) + C_{i,1}(\dot{q}_i)(z_i - \xi_i) + C_{i,2}(q_i)\dot{\varphi}_i(q_i, \mu_i) \\ &\quad + C_{i,3}(\dot{q}_i)\varphi_i(q_i, \mu_i) \end{aligned} \quad (1)$$

where  $i = 1, 2, \dots, M$ ,  $q_i = [x_i, y_i, \theta_i]^\top \in \mathbb{R}^3$ ;  $(x_i, y_i)$  are the coordinates of the midpoint between two driving wheels of the  $i$ th robot,  $\theta_i$  is the heading angle of the  $i$ th robot,  $z_i = [v_i, \omega_i]^\top \in \mathbb{R}^2$ ;  $v_i$  and  $\omega_i$  are a forward linear and an angular velocity of the  $i$ th robot, respectively,  $\xi_i = [\xi_{i,1}, \xi_{i,2}]^\top \in \mathbb{R}^2$ ;  $\xi_{i,1}$  is the longitudinal slip velocity of the  $i$ th robot and  $\xi_{i,2}$  is the yaw rate perturbation due to the wheel slippage of the  $i$ th robot,  $\varphi_i = [-\mu_i \sin \theta_i, \mu_i \cos \theta_i, 0]^\top \in \mathbb{R}^3$ ;  $\mu_i$  denotes the lateral skidding velocity of the  $i$ th robot,  $\tau_i = [\tau_{i,1}, \tau_{i,2}]^\top \in \mathbb{R}^2$  is the control torque applied to the wheels of the  $i$ th robot, and  $J_i(q_i) = \begin{bmatrix} \cos \theta_i & \sin \theta_i & 0 \\ 0 & 0 & 1 \end{bmatrix}^\top$ . The definitions of the matrices  $H_i$ ,  $C_{i,1}(\dot{q}_i)$ ,  $C_{i,2}(q_i)$ , and  $C_{i,3}(\dot{q}_i)$  in the dynamics (2) are given in Yoo and Park (2013). Each follower described by (1) and (2) can consist of heterogeneous kinematics and dynamics.

**Assumption 1** (Wang & Low, 2008). The skidding and slipping perturbations  $\xi_{i,1}$ ,  $\xi_{i,2}$ , and  $\varphi_i(q_i, \mu_i)$  are bounded as  $|\xi_{i,1}| < \beta_{i,1}$ ,  $|\xi_{i,2}| < \beta_{i,2}$ , and  $\|\varphi_i(q_i, \mu_i)\| = |\mu_i| < \beta_{i,3}$  due to  $\|[-\sin \theta_i, \cos \theta_i]^\top\| = 1$ , respectively, where  $\beta_{i,j} > 0$ ,  $j = 1, 2, 3$ , are

unknown constants. Their first derivatives are bounded as  $|\dot{\xi}_{i,1}| < \beta_{i,d1}$ ,  $|\dot{\xi}_{i,2}| < \beta_{i,d2}$ , and  $\|\dot{\varphi}_i(q_i, \mu_i)\| < \beta_{i,d3} + \beta_{i,3}(|\omega_i| + |\dot{\mu}_i|)$  with  $|\dot{\mu}_i| < \beta_{i,d3}$  where  $\beta_{i,dj} > 0$ ,  $j = 1, 2, 3$ , are unknown constants.

**Assumption 2.** The system matrices  $H_i$ ,  $C_{i,1}(\dot{q}_i)$ ,  $C_{i,2}(q_i)$ , and  $C_{i,3}(\dot{q}_i)$  for the dynamics (2) are unknown where  $i = 1, \dots, M$ .

The communication topology for the  $M + 1$  robots is described by a directed graph  $\mathcal{G} \triangleq (\mathcal{V}, \mathcal{E})$  with  $\mathcal{V} \triangleq \{0, 1, 2, \dots, M\}$ . To represent the communication among follower robots, we define a subgraph as  $\bar{\mathcal{G}} \triangleq (\bar{\mathcal{V}}, \bar{\mathcal{E}})$  with  $\bar{\mathcal{V}} \triangleq \{1, 2, \dots, M\}$ . The adjacency matrix  $\bar{\mathcal{A}}$  of the subgraph  $\bar{\mathcal{G}}$  is  $\bar{\mathcal{A}} = [a_{ij}] \in \mathbb{R}^{M \times M}$ ;  $a_{ij} > 0$  if  $(j, i) \in \bar{\mathcal{E}}$ ,  $a_{ij} = 0$  otherwise, and  $a_{ii} = 0$ . Then, the (nonsymmetric) Laplacian matrix  $\mathcal{L}$  of  $\mathcal{G}$  is defined as  $\mathcal{L} = \begin{bmatrix} 0 & 0_{1 \times M} \\ -b & \bar{\mathcal{L}} + \mathcal{B} \end{bmatrix}$  where  $b = [b_1, \dots, b_M]^\top$ , with  $b_i > 0$  if the leader robot  $0 \in \mathcal{N}_i$  and  $b_i = 0$  otherwise, denotes the communication weight from the leader robot to the follower robots,  $\mathcal{B} = \text{diag}[b_1, \dots, b_M]$ , and  $\bar{\mathcal{L}} = \bar{\mathcal{D}} - \bar{\mathcal{A}}$  is the Laplacian matrix of the subgraph denoting the communication among followers. Here,  $\bar{\mathcal{D}} = \text{diag}[d_1, \dots, d_M]$ ;  $d_i = \sum_{j=1, j \neq i}^M a_{ij}$  is the diagonal element of the degree matrix  $\bar{\mathcal{D}}$ .

**Remark 1.** If the directed graph  $\mathcal{G}$  has a spanning tree,  $\text{rank}(\mathcal{L}) = M$  (Ren, 2008). Then,  $\text{rank}(\mathcal{L} + \mathcal{B}) = M$  from  $(\mathcal{L} + \mathcal{B})\mathbf{1}_M = b$  where  $\mathbf{1}_M$  is an  $M$ -vector of all ones.

### 2.3. Potential function for collision avoidance

The potential function for collision avoidance among robots is defined as

$$P_{i,h} = \left( \min \left\{ 0, \frac{\varsigma_{i,h}^2 - \bar{L}_{i,h}^2}{\varsigma_{i,h}^2 - l_{i,h}^2} \right\} \right)^2 \quad (3)$$

where  $i = 1, \dots, M$ ,  $h = 1, \dots, M$ ,  $h \neq i$ ,  $\varsigma_{i,h} = \sqrt{(x_i - x_h)^2 + (y_i - y_h)^2}$  denotes the distance between the  $i$ th robot and the  $h$ th robot,  $\bar{L}_{i,h} = \max\{L_i, L_h\} > 0$ ;  $L_i$  and  $L_h$  are the radii of the detection region of the  $i$ th robot and the  $h$ th robot, respectively, and  $l_{i,h} = l_{h,i} > 0$  is the avoidance region denoting the smallest safe distance between the robots and  $\bar{L}_{i,h} > l_{i,h} > 0$ .

The partial derivatives of  $P_{i,h}$  with respect to the  $x_i$  and  $y_i$  coordinates are defined as

$$\frac{\partial P_{i,h}}{\partial x_i} = \begin{cases} \bar{P}_{i,h}(x_i - x_h), & \text{if } l_{i,h} < \varsigma_{i,h} < \bar{L}_{i,h}; \\ 0, & \text{otherwise,} \end{cases} \quad (4)$$

$$\frac{\partial P_{i,h}}{\partial y_i} = \begin{cases} \bar{P}_{i,h}(y_i - y_h), & \text{if } l_{i,h} < \varsigma_{i,h} < \bar{L}_{i,h}; \\ 0, & \text{otherwise,} \end{cases} \quad (5)$$

where  $\bar{P}_{i,h} = 4 \frac{(\bar{L}_{i,h}^2 - l_{i,h}^2)(\varsigma_{i,h}^2 - \bar{L}_{i,h}^2)}{(\varsigma_{i,h}^2 - l_{i,h}^2)^3}$ .

### 2.4. Problem statement

The control objective is to design the approximation-based distributed adaptive formation control laws  $\tau_i$  for networked mobile robots (1) and (2) under a direct graph so that

(I) outside the detection range ( $\varsigma_{i,h} \geq L_{i,h}$ ),  $\lim_{t \rightarrow \infty} \|\psi_i(t) - l(t) - \Delta_{i0}\| < \bar{\epsilon}$  and  $\lim_{t \rightarrow \infty} (\sin(\theta_i(t)) - \theta_0(t)) + \frac{\mu_i}{v_0} \leq \iota_i$  where  $\psi_i = [x_i, y_i]^\top$ ,  $\bar{\epsilon} > 0$  and  $\iota_i > 0$  are constants that can be made sufficiently small,  $\Delta_{i0} = \Delta_i - \Delta_0 \in \mathbb{R}^2$  denotes the desired offset between the  $i$ th follower robot and the leader robot, and  $l(t) = [x_0(t), y_0(t)]^\top \in \mathbb{R}^2$  is the leader's position generated by  $\dot{x}_0 = v_0 \cos(\theta_0)$ ,  $\dot{y}_0 = v_0 \sin(\theta_0)$ , and  $\dot{\theta}_0 = \omega_0$  with the position  $(x_0, y_0)$  and orientation  $\theta_0$  and the linear and angular velocities ( $v_0 > 0$ ,  $\omega_0$ ); and

Download English Version:

<https://daneshyari.com/en/article/695533>

Download Persian Version:

<https://daneshyari.com/article/695533>

[Daneshyari.com](https://daneshyari.com)