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On the running-in behavior of cam-follower mechanism

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## On the Running-in Behavior of Cam-Follower Mechanism

### Abstract

A line contact thermo-elasto-hydrodynamics analysis is developed to study the behavior of the cam-and-follower contact. The elasto-plastic model takes into account the asperity pressure and asperities' flattening due to plastic deformation. The modified Reynolds equation is solved to predict the hydrodynamic pressure. The change in the surface roughness and friction coefficient during the running-in period is taken into account with provision for thermal effects. The results show the performance parameters of the cam-follower during the running-in period are strongly affected by the rotational speed and thermal effects. In particular, the variations of film thickness and the frictional force of this mechanism, not hitherto reported in the literature, are discussed in depth. It is shown that the rate of flattening of surface roughness is a crucial factor during the running-in period.

**Keywords:** Cam and follower; thermo-elastohydrodynamic; mixed Lubrication; surface roughness; running-in

### Nomenclature:

$A_a$	Total real area of contact ( $m^2$ )	$R$	Equivalent radius of curvature of the cam and follower (m)
$A_h$	Area associated with hydrodynamic effect ( $m^2$ )	$R_{1,2,3,4}$	Length vector (m)
$A_n$	Nominal area of contact ( $m^2$ )	$R_b$	Base circle radius of the cam (m)
$C_k$	Damping Coefficient ( $Nsm^{-1}$ )	$R_{cam}$	Radius of the cam (m)
$C_p$	Thermal capacity at Constant pressure (KJ/KgK)	$T$	Temperature (K)
$D_{ij}$	Coefficients of deflection matrix	$T_0$	Reference temperature (K)
$E'$	Equivalent Young's modulus (Pa)	$U$	Non-dimensional velocity ( $u_E \mu_0 / (RE')$ )
$F$	Preload force (N)	$V$	Non-dimensional hardness number ( $HD/E'$ )
$FC$	Friction coefficient	$W$	Non-dimensional load
$F_n$	Load (N)	$W_t$	Asperity contact load
$F_t$	Friction force (N)	$X_C$	Coordinate of contact point between cam and follower (m)
$G$	Non-dimensional material number	$X_{CC}$	Coordinate of the center of curvature of the cam (m)
$H$	Non-dimensional film thickness	$Y_C$	Coordinate of contact point between cam and follower (m)
$K$	Thermal conductivity (KJ/KgK)	$Y_{CC}$	Coordinate of the center of curvature of the cam (m)
$L$	Follower lift (m)	$Z$	Viscosity pressure index
$N_a$	Number of Asperity	$a$	Hertzian half-contact width(m)
$P$	Non-dimensional Pressure	$c_i$	Relaxation factor
$P_H$	Maximum Hertzian pressure distribution(Pa)	$c_{s1}$	Damping coefficient of part 1 spring ( $Nsm^{-1}$ )
$P_a$	Non-dimensional asperity Pressure	$c_{s2}$	Damping coefficient of part 2 spring ( $Nsm^{-1}$ )
$P_h$	Non-dimensional hydrodynamic Pressure	$d$	Cam width (m)
$f_0$	Spring natural frequency (Hz)	$y_s^*$	$=y_s/\sigma$
$h$	Lubricant film thickness (m)	$z$	Distance of asperity summit to mean asperity height (m)
$h^*$	$=h/\sigma$	$z^*$	$=z/\sigma$
$h_0$	Lubricant film thickness at center of coordination (m)	$\Delta FC$	Friction coefficient difference (%)
$\bar{h}_T$	Average gap between two rough surfaces (m)	$\Delta X$	Distance between two mesh(m)
$k$	Stiffness (N/m)	$\Delta \bar{t}$	Time step
$k_0$	Spring Stiffness (N/m)	$\alpha_{EHL}$	Elastohydrodynamic pressure-viscosity coefficient
$k_{s1}$	Stiffness of part 1 Spring (N/m)	$\beta$	Asperity Radius (m)
$k_{s2}$	Stiffness of part 2 Spring (N/m)	$\bar{\beta}$	$=\beta/R$

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