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Research paper

An analysis of the effect of the footprint orientation on the thermalhydraulic performance of a microchannels heat sink during flow boiling of R245fa



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HIGHLIGHTS

• Experimental analyses of a microchannels heat sink during flow boiling of R245fa.

• The footprint orientation effect on thermal-hydraulic performance was evaluated.

• HP provides highest heat transfer coefficient and VP lowest pressure drops.

Images of the flow boiling showed thermal instabilities.

• One method for heat transfer coefficient had satisfactory prediction.

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ABSTRACT

The present study concerns an experimental investigation of flow boiling of R245fa in a 50 parallel rectangular 123.3 \times 494.2 μm^2 microchannels heat sink. Heat transfer coefficient and pressure drop results were obtained for footprint heat fluxes up to 300 kW/m², mass velocities from 300 to 1000 kg/ m² s, liquid subcoolings at the test section inlet of 5 and 10 °C and saturation temperature of 30 °C. The heat sink performance was evaluated for its footprint area horizontally positioned (HP), its footprint area vertically aligned with the microchannels horizontally positioned (VHP) and its footprint area vertically positioned with upflow through the microchannels (VP). Average footprint heat transfer coefficients up to 30 kW/m² $^{\circ}$ C were obtained. Moreover, for two-phase flow and fixed heat flux, the heat transfer coefficient increases with decreasing mass velocity and liquid subcooling, while the pressure drop increases with increasing mass velocity and decreasing liquid subcooling. The heat sink according to the HP orientation provides higher overall heat transfer coefficients. The highest and lowest pressure drops were observed for the VHP and VP orientations, respectively. The effect of the footprint orientation on the heat transfer coefficient increases with increasing mass velocity and liquid subcooling. Temperature oscillations with higher amplitude and frequency were observed for the VHP orientation. Images of the flow boiling process revealed that bubbles agglomerate in the lower part of the heat sink for the VHP orientation under conditions of high mass velocities. Reverse flows were observed only for HP and VHP footprint orientations. Discontinuities in the boiling curve just before the ONB have occurred simultaneously to bubble nucleation at the outlet plenum. Li and Wu [42] was the best method to predict the heat transfer coefficient data. For pressure drop, the Homogeneous Model using the two-phase viscosity given by Cicchitti et al. [46] presented the best prediction of the experimental results compare with the others predictive methods evaluated, but no one of pressure drop predictive methods evaluated in the present study was accurate enough to predict the R245fa database for flow boiling conditions.

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Nomenclature		σ	surface tension [N/m]	
		τ	elongated bubble period [s]	
А	area [m ²]	ξ	fraction of data predicted within an error band of $\pm 30\%$	
C _p	heat capacity [kJ/kg °C]		[%]	
D _h	hydraulic diameter [m]	η	mean absolute error [%]	
dp/dz	pressure drop gradient [kPa/m]			
F	enhancement factor [dimensionless]	Subscripts		
f	frictional factor [dimensionless]	1φ	single-phase flow	
G	mass velocity [kg/m ² s]	2φ	two-phase flow	
g	gravitational acceleration [m/s ²]	1	pre-heater inlet	
HP	horizontally positioned [dimensionless]	acl	accelerational	
Н	microchannel depth [m]	adj	adjust	
h	heat transfer coefficient [W/m ² °C]	С	convective	
i	enthalpy [kJ/kg]	ch	channel	
i _{lv}	enthalpy of vaporization [kJ/kg]	cont	contraction	
k	thermal conductivity [W/mK]	df	differential pressure measurement	
L	length [m]	eff	effective, effective contact with the fluid	
М	molar mass [kg/Mol]	elet	electrical power	
m	mass flux [kg/s]	end	end	
р	absolute pressure [kPa]	env	environment	
pr	reduced pressure [dimensionless]	exp	expansion	
Q	dissipated energy [W]	fluid	fluid	
$\mathbf{q}^{\prime\prime}$	heat flux [W/m ²]	ftp	footprint area	
S	suppression factor [dimensionless]	film	liquid film	
Т	temperature [°C]	heated	heated	
T	average temperature [°C]	homo	homogeneous model	
t _{film}	liquid film time [s]	in or 2	heat spreader inlet	
tı	liquid slug time [s]	1	liquid-phase	
t _{max.film}	maximum liquid film time [s]	11	viscous–viscous flow	
t _v	vapor slug time [s]	lo	the two-phase mixture as liquid	
VHP	vertically oriented with horizontal channels	NB	nucleate boiling	
	[dimensionless]	v	vapor-phase	
VP	vertically positioned with vertical channels	VO	the two-phase mixture as vapor	
	[dimensionless]	real	real	
W	microchannel width [m]	out or 3	heat spreader outlet	
х	vapor quality [dimensionless]	plm	inlet and outlet plenum	
Х	Lockhart–Martinelli parameter [dimensionless]	sat	saturated state	
X	average vapor quality [dimensionless]	TP	two-phase	
		wall	wall	
Greek sy	Greek symbols			
δ0	liquid film thickness [m]	Dimensio	De sumpers	
δ_{end}	final liquid film thickness [m]	BO	$BO = q''/G \cdot l_{lv}$ bolling number [dimensionless]	
δ _{min}	minimum liquid film thickness [m]	BO	$BO = g(\rho_l - \rho_g) D_{h}^{T/\sigma} \text{ bond number [dimensionless]}$	
Δp	differential pressure [kPa]	Co	$Co = I/D_h \sqrt{\sigma/g} \cdot (\rho_l - \rho_v)$ confinement number	
ΔT_{sub}	liquid subcooling [°C]	En	[uninensionness] $\operatorname{Er} = C^2 (a, \alpha, \beta)$ Froude number [dimensionless]	
$\Delta \overline{T}$	wall superheating [°C]	ΓΓ Dr	$r_1 = G / p_1 \cdot g \cdot D_h$ Froude number [dimensionless]	
μ	dynamic viscosity [Pa s]	Pr	$r_1 = c_p \cdot \mu/\kappa$ rialiau number [almensionless]	
ν	kinematic viscosity [Pa s]	ке Сл	$\kappa e = G \cdot D_h \mu$ Reynolds number [dimensionless] $C_7 = L D \cdot P_8 \cdot P_7 C_{rastz}$ number [dimensionless]	
ρ	density [kg/m ³]	GZ	$G_{L} = L_{I} D_{h} Re PI Graetz number [unitensionless]$	

1. Introduction

During the last five decades, the electronic industry has experienced an exponential increase of the number of transistors in the microprocessors. This miniaturization process is associated with the need of dissipating extremely high heat fluxes from the microelectronic devices. These circumstances drove the electronic industry and the heat transfer academics to focus on the development of heat sinks capable of meeting such demands. Heat sinks based on single-phase flow through multi parallel micro-scale channels are currently available in the market for replacing aircooling as a more energy-efficient solution. Besides, heat spreaders based on flow boiling mechanism inside micro-scale channels have been considered as a better alternative to dissipate the very high heat transfer rates from electronic devices because of their compactness and excellent heat transfer performance.

According to Ribatski et al. [1] and Qu and Mudawar [2], flow boiling in small diameter channels presents as advantage over conventional channels the combination of higher surface area in contact with the coolant per volume and superior heat transfer coefficients. Moreover, evaporation in microchannels minimizes temperature gradient along the heat sink length when compared against single-phase cooling. These characteristics allow Download English Version:

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