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# Numerical investigation of laminar thermal-hydraulic performance of Al<sub>2</sub>O<sub>3</sub>-water nanofluids in offset strip fins channel

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#### ARTICLE INFO

#### ABSTRACT

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**39** 34 Using the single-phase based numerical approach, this paper studies the three-dimensional laminar flow and 14 heat transfer behavior of  $Al_2O_3$ -water nanofluids in an offset strip fins channel. Parametric variations are 15 analyzed for explaining the influences of different nanoparticle volume fraction (0%-4%) and Reynolds number 16 (500-1000). The numerical results indicate that both the heat transfer and pressure loss of offset strip fins 17 channel are enhanced significantly with the increases of nanoparticle volume fraction and Reynolds number. At 18 Reynolds number of 1000, the average heat transfer coefficient can be improved by 26.69% when adding 4% vol-19 ume fraction of  $Al_2O_3$  nanoparticles in the base fluid. Besides, the Nusselt number of  $Al_2O_3$ -water nanofluids is 20 higher than that of the base fluid at various Reynolds number only when the volume fraction of  $Al_2O_3$  nanoparticle volume fraction has the most obvious advantage due to the reduction of pumping 23 power.

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#### 36 1. Introduction

As one of the most important process equipment for exchanging the 37heat quantity, plate-fin heat exchangers are applied in many fields of 38 chemical engineering, energy storage and conversion due to its high ef-39 ficiency and compactness [1]. According to actual needs, various types 40of working fluids and fin structures can be used in the plate-fin heat 41 exchangers [2]. Offset strip fins is designed to enhance heat transfer 42 by enlarging surface area and regenerating thermal boundary layer in 43 each flow channel [3]. However, this type of fins also can increase the 44 45 pressure drop within the heat exchanger. In the past few decades, Kays [4], London and Shah [5], Hu and Herold [6], Dong et al. [7], Peng 46and Ling [8], and Fernández-Seara et al. [9] experimentally studied the 47 effects of different surface geometries on the flow and heat transfer per-4849 formance of offset strip fins. Based on such experimental data, many empirical correlations have been carried out with various working 50conditions [10-14]. Recently, with the rapid growth of computational 5152capabilities, some numerical investigations [15-17] have been performed to capture and explain the thermal-hydraulic behaviors of 53 different working fluids in the offset strip fins. Besides, in order to 5455realize the full potential of heat exchangers with offset strip fins, a 56large number of previous researches were published to optimize the 57geometric variables of offset strip fins based on different algorithms 58[18–21]. However, with the rapid increase in heat flux and owing to

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http://dx.doi.org/10.1016/j.icheatmasstransfer.2016.03.024 0735-1933/© 2016 Published by Elsevier Ltd. manufacturing limitation, it is difficult to significantly improve the 59 heat transfer capabilities of offset strip fins by changing geometric vari- 60 ables only. In addition, conventional working fluids including water, 61 ethylene glycol and oil exhibit relative low thermal conductivity. 62 Therefore, there is a need for developing new and innovative technolo- 63 gies to enhance the heat transfer of plate–fin heat exchangers with 64 offset strip fins. 65

Nanofluids, consisting of the conventional working fluids and differ- 66 ent nanometer-sized particles, seem to be a potential replacement of 67 conventional coolants [22]. In recent years, the research on various 68 nanofluids has received great attention due to the superior characteris- 69 tics of nanofluids [23–28]. Most of the investigations in general indicat- 70 ed that thermo-physical properties of nanofluids could be affected by 71 nanoparticle properties (such as type, volume fraction and size), tem-72 perature and base fluid. However, the specific influence of each factor 73 is still not very clear. There are also some inconsistencies in existing 74 literatures, due to the differences in preparation technology, measuring 75 and data analyzing methods [29-31]. All of these make it difficult to re- 76 liably model and predict the thermo-physical properties of different 77 nanofluids, which limit the further application of nanofluids. For most 78 of the investigations, the addition of nanoparticle is expected to en-79 hance the heat transfer of base fluid considering the fact that nanofluids 80 have relatively high thermal conductivity [32–35]. However, it is worth 81 pointing out that the suspensions of nanoparticles also can increase the 82 viscosity and decrease the specific heat, which mean that the improve-83 ment in thermal conductivity of nanofluids may be counteracted by the 84 negative effects of viscosity and specific heat [36-38]. Hence, a further 85 research for quantifying the effects of nanofluids on the thermal- 86

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Nomen	clature
A <sub>t</sub>	Total heat transfer area, m <sup>2</sup>
$C_p$	Specific heat, J/(kg·K)
d	Nanoparticle diameter, nm
$D_h$	Hydraulic diameter, mm
f	Fanning friction factor
Fh	Fin height, mm
Fs	Fin space, mm
Ft	Fin thickness, mm
G	Mass velocity, $kg/(m^2 \cdot s)$
h	Heat transfer coefficient, $W/(m^2 \cdot K)$
j	Colburn factor
k	Thermal conductivity, W/(m·K)
1	Fin length, mm
L	Channel length, mm
т	Mass flow rate, kg/s
М	Molecular weight, kg/mol
Ν	Avogadro number
Nu	Nusselt number
$N_{X, Y, Z}$	Nodes number in X, Y, Z directions
Р	Pressure, Pa
PP	Pumping power, W
Pr	Prandtl number
Q	Heat transfer rate, W
Re	Reynolds number
Т	Temperature, K
V	Velocity, m/s
V	Volume flow rate, m <sup>3</sup> /s
Greek sy	mbols
$\varphi$	Particle volume concentration, %
ρ	Density, kg/m <sup>3</sup>
μ	Viscosity, Pa·s
δ	Cover plate thickness, mm
к	Boltzmann constant
Subscrip	ts
bf	Base fluid
in	Inlet
nf	Nanofluids
out	Outlet
р	Nanoparticle
w	Wall
	Nomenon $A_t$ $C_p$ d $D_h$ f Fh Fs Ft G h j k l L m M Nu Nx, y, z P PP Pr Q Re T V V Greek sy $\varphi$ $\rho$ $\mu$ $\delta$ $\kappa$ Subscript $bfinnfoutpW$

hydraulic performance of various types of heat transfer structure is 87 88 needed.

Huminic et al. [39] presented a review on the heat transfer enhance-89 ment of heat exchangers by using nanofluids as coolant. Through their 90 91studies, it was found that the previous researches mainly focus on the 92plate heat exchangers [40–44], the shell-and-tube heat exchangers 93 [45,46], the compact heat exchangers [47,48] and the double-pipe heat exchangers [49-51]. The studies dealing with the analysis of 94 nanofluids in the plate-fin heat exchangers are still very limited. Javadi 9596 et al. [52] proposed a theoretical investigation on the heat transfer and flow behavior of SiO<sub>2</sub>, TiO<sub>2</sub> and Al<sub>2</sub>O<sub>3</sub> nanofluids with liquid nitrogen 97 as base fluid in the plate-fin heat exchanger. They found that nanofluids 98 have higher heat transfer and pressure loss in comparison with the base 99 fluid. In addition, their study also indicated that Al<sub>2</sub>O<sub>3</sub> nanofluids had 100 the highest overall heat transfer coefficient, while the pressure drop of 101 SiO<sub>2</sub> nanofluids was lowest. Khoshvaght-Aliabadi et al. [53] experimen-102tal studied the effects of Cu-water nanofluids on the comprehensive 103 performance of various plate-fin channels. As depicted in their investi-104 105 gations, the increase of Cu nanoparticle could significantly enhance the heat exchange capacity of every plate-fin channels, meanwhile the 106 pressure drop increased at the same time. They also found that the 107 vortex generator channel provided the maximum reduction of surface 108 area. On this basis, a comparative analysis for the typical numerical 109 methods (homogeneous, mixture and Eulerian) was performed to fur- 110 ther evaluate the laminar forced convective heat transfer of Cu-water 111 nanofluids in the vortex-generator plate-fin channel [54]. All the results 112 showed that the numerical values obtained by mixture method were 113 more close to the experimental data. Besides, Khoshvaght-Aliabadi 114 et al. [55] also experimentally study the heat transfer enhancement of 115 nanofluids in the corrugated wavy plate-fin channel at a constant wall 116 temperature condition. 117

According to the above analysis, there is no existing numerical study 118 on the thermal-hydraulic analysis of nanofluids forced laminar convec- 119 tion in the offset strip fins channel. Therefore, in the present study, a 120 numerical analysis is investigated to study the laminar heat transfer 121 and flow characteristics of an offset strip fins channel with the most 122 commonly used nanofluids (Al<sub>2</sub>O<sub>3</sub>-water) as coolant. Then, the 123 variations of heat transfer, flow and comprehensive performance with 124 the volume fraction of Al<sub>2</sub>O<sub>3</sub> nanoparticle and the Reynolds number 125 are analyzed in detail. 126

2. Mathematical model	
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#### 2.1. Geometric description and computational domain

Fig. 1(a) shows the flow directions of hot and cold working fluids in a 129 typical cross flow plate-fin heat exchanger. The geometrical parameters 130 and specific terminology of offset strip fins with rectangular cross sec- 131 tion can be defined in Fig. 1(b). Considering the symmetrical and peri- 132 odic features of the offset strip fins channel, the three-dimensional 133 structures as described in Fig. 2 are selected as the computational 134 domain to save computational time without compromising accuracy. 135 In the present study, the computational domain includes some seg- 136 ments of offset strip fins, cover plates on top and bottom of the fins, 137 and working fluid. Many previous investigations found that the flow 138 in the offset strip fins channel could be supposed 'fully developed' 139 when taking 4–5 fin periods [15,17]. Therefore, a proper computational 140 domain length (65 mm) consisting of 13 strip rows is selected to 141 accurately simulate the flow and heat transfer characteristics of offset 142 strip fins channel. Table 1 lists the values of geometrical parameters 143 needed for modeling in this work. Besides, Cu is selected as the material 144 of the fins and cover plates. 145

#### 2.2. Governing equations and boundary conditions

Normally, the numerical simulation of nanofluids flow can be per- 147 formed using two different methods which are single and two-phase 148 approach [56–59]. Due to the small size of nanoparticle, many recent 149 researches suggested that nanofluids behaved like a single-phase fluid 150 when the nanoparticle fraction was very low [60,61]. Besides, compared 151 to the two-phase based approach, the single-phase based approach is 152 relative simple to implement while the numerical accuracy remains. 153 Therefore, the single-phase based approach is considered to simulate 154 and describe the laminar flow and heat transfer behavior of nanofluids 155 flowing through an offset strip fins channel under constant wall 156 temperature. 157

In the present study, the following assumptions are considered [62]: 158

- (1) The flow is a three-dimensional steady-state,
- (2) Nanofluids is the incompressible and Newtonian fluid, 160
- (3) The velocity is same for the fluid and nanoparticles, and they are 161 in thermal equilibrium, 162
- All the nanoparticles are uniform in shape and size, (4)163
- (5) The effects of radiation and viscous dissipation are negligible, 164 165
- (6) The properties of working fluids are constant.

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