



# An intermittency factor weighted laminar kinetic energy transition model for heat transfer overshoot prediction



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## ABSTRACT

An intermittency factor weighted laminar kinetic energy transition model appropriate for the prediction of overshoot in the transition region is proposed. Based on the hypersonic laminar kinetic energy transition model, study finds that the model predicts the overshoot when the transition onset is near the front of the configuration with a short transition zone, and greater gradients of relevant variables account for this circumstance. Therefore, the thought that accelerating the forming process of turbulent boundary layer in the late transition region to make greater variable gradients comes into being. Considering the convective and diffusive timescales of disturbances, an algebraic intermittency factor is presented and involved in the small-scale viscosity. In order to achieve the acceleration, compared with the DNS data as well, the intermittency factor is revised for a further step. Finally, the large-scale and small-scale viscosities are weighted by the revised intermittency factor. The revised model has been applied to flat plate boundary layer and boundary layer transitions over a blunt cone at different Reynolds numbers test cases. The results demonstrate the capacity of the model to reproduce overshoot with a reasonable degree of accuracy and reflect the effect of Reynolds number successfully. The revision originates from the perspective of transition model construction. A more sophisticated physics-based description of transition would be more preferable.

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## 1. Introduction

The stability and laminar-turbulent transition of boundary layers at supersonic and hypersonic speeds have been studied for more than 50 years [1] and have become advanced research hot-spots as well as formidable challenges. The physics underlying this phenomenon indicates that the transition is a multifold process that evolves in many different ways depending on numerous parameters of the mean flow and disturbances [1]. Hypersonic boundary layer transition phenomena have several unique features and the topics must be treated independently. In low speed boundary layers, one is accustomed to thinking of the vorticity instability mode which produces low frequency, low amplitude velocity fluctuations. A unique feature of a hypersonic boundary layer is the presence of the higher instability modes, the Mack mode [2]. These instabilities produce high frequency, large amplitude density fluctuations which can dominate the transition process [3].

From an application perspective, as boundary layer transits from laminar flow to turbulent flow, the fractional drag and aerodynamic heat of the aircrafts operating at sustained supersonic or

hypersonic speeds increase prominently, which threatens the flight safety immensely. As a result, predicting boundary layer transition accurately is of great significance to the design of aerodynamic configurations, thermal protection systems and so on.

In the computational fluid dynamics (CFD) range, primitive boundary layer transition prediction methods mainly consists of experimental or empirical correlations [4,5]. The classical attempts of these approaches are to correlate transition onsets with one or two parameters from multitudinous influencing factors such as Reynolds number, Mach number and so on. For specific conditions, these correlations achieve great success, while for general cases, lacking in universality brings about large dispersion of the prediction results.

To be reliable for a broad range of circumstances, flow mechanisms based methods dominant boundary layer transition prediction approaches by degrees. Hierarchically, these methods involve, in the order of descending requirement in computational resources, direct numerical simulation (DNS) [6], large eddy simulation (LES) [7], nonlinear parabolized stability equations (NPSE) [8],  $e^N$  methods [9] based on Linear Stability Theory (LST) and linear parabolized stability equations (PSE), and Reynolds Averaged Navier-Stokes (RANS) approaches.

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## Nomenclature

$x_j$	Cartesian coordinates	$\tau_{T,11}$	first mode characteristic timescale
$U_j$	velocity vector	$\tau_{T,12}$	second mode characteristic timescale
$\rho$	fluid density	$\mu_{T,11}$	first mode viscosity
$p$	pressure	$\mu_{T,12}$	second mode viscosity
$E$	total energy	$f_v$	viscous damping function
$T$	temperature	$f_{int}$	intermittency factor
$\delta_{ij}$	Kronecker delta function	$f_{ss}$	shear-sheltering damping function
$S$	strain rate, $ S_{ij} $	$C_\mu$	turbulent viscosity coefficient
$\Omega$	vorticity, $ \Omega_{ij} $	$\alpha_T$	effective diffusivity
$k_T$	turbulence kinetic energy	$f_\omega$	kinematic damping function
$k_L$	laminar kinetic energy	$R_{BP}$	model term for bypass transition
$\omega$	specific turbulence dissipation rate	$R_{NAT}$	model term for natural transition
$k_{T,s}$	effective small-scale turbulence	$F_2$	blend function
$k_{T,l}$	effective large-scale turbulence	$Tu$	free stream turbulence intensity
$P_{kT}$	production term of $k_T$ equation	$h_{FR}$	Reference heat transfer rate
$D_{kT}$	dissipation term of $k_T$ equation	$Re_T$	effective turbulence Reynolds number
$P_{kL}$	production term of $k_L$ equation	$Ma_{rel}$	local relative Mach number
$D_{kL}$	dissipation term of $k_L$ equation	$q$	heat transfer rate
$\mu$	molecular viscosity	$Ma$	Mach number
$\mu_{T,l}$	large-scale dynamic viscosity coefficient	$Re_\infty$	free stream Reynolds number
$\mu_{T,s}$	small-scale dynamic viscosity coefficient	$P_0$	stagnation pressure
$\nu_{T,l}$	large-scale kinematic viscosity coefficient	$T_0$	stagnation temperature
$\nu_{T,s}$	small-scale kinematic viscosity coefficient	$H_{aw}$	adiabatic wall enthalpy
$\nu_T$	turbulent kinematic viscosity coefficient	$H_{iw}$	isothermal wall enthalpy
$\lambda_{eff}$	effective length scale		
$\tau_{T,l}$	characteristic timescale		

Recently, as a main method of the refined flow simulations, the rapid developing DNS has made remarkable contributions to the reveal of transition mechanisms. However, regarding the large computational consumption, DNS remains to be a pure research tool rather than an engineering prediction method. Comparatively, based on the universal assumption following Kolmogorov's Universal Equilibrium Theory, LES reduces the computational requirements by modelling the turbulence below the inertial sub-range, while the calculation is still quite beyond affordability for engineering applications, especially for complex geometries. In addition, for hypersonic flows, on account of the massive difficulties in reliable transition experiments, DNS and LES are somewhat far ahead of experimental database.

As for flows dominated by initial small disturbances with linear growth of instability modes, the  $e^N$  methods based on the integrated amplification of wave amplitude can reproduce the early transition behaviors. While for transition scenarios resulting from nonlinear disturbances growth with strong amplification of high-frequency secondary instabilities, more sophisticated NPSE methods would be preferable [8].

From the perspective of engineering, RANS based methods represents a reasonable compromise between accuracy and expense. Coupled with RANS equations, transition models are the most practical methods to predict boundary layer transition. For a further step, the most effective practices of transition models are to extend turbulent models by including additional transport equations to reproduce transition behaviors.

The intermittent behavior was discovered in the transition process after Emmons recorded that transition was induced by the eruption of turbulent spots [10]. Based on the correlation of intermittency factor  $\gamma$  summarized by Dhawan and Narasimha [11], a  $\gamma$  transport equation was firstly proposed by Steelant and Dick [12]. Employing a  $\gamma$  equation, a  $k-\varepsilon-\gamma$  model was proposed by Cho and Chung [13] to simulate the transition behaviors in the free shear flows. Concentrating on the intermittency distribution in both

streamwise and crosswise direction, Suzen and Huang [14] developed a new  $\gamma$  transport equation. While the non-local variables, such as boundary layer thickness and boundary layer momentum thickness in Suzen and Huang's model [14] result in extremely tough work to implement the model with massively parallel execution and unstructured grids. The variables localization thought reversed the situation when Langtry, Menter and Volker [15] proposed the correlation based transition model  $\gamma-Re_\theta$ . Test cases [15,16] manifest great correspondence with the experimental results for low-speed flows. Hao et al. [17] developed the  $\gamma-Re_\theta$  transition model to be appropriate for hypersonic flows by introducing a new correlation of momentum thickness Reynolds number using local variables.

According to LST analysis, for hypersonic flows at Mach number lower than four, the first-mode disturbances master the transition process, while the second-mode disturbances master the situation when Mach number is greater than four. To take account of these two unstable modes, Warren and Hassan [18] put forward the non-turbulent viscosity  $\mu_{nt}$ , a function of non-turbulent timescale related to the unstable modes. Similarly, pondering different unstable modes, Wang and Fu [19–21] proposed a  $k-\omega-\gamma$  transition model applicable to both subsonic flows and supersonic/hypersonic flows. Hao et al.'s research [22] on the performance of the  $k-\omega-\gamma$  transition model under different free-stream conditions demonstrates that the model can predict reasonable transition trends without accurate transition onsets at different Reynolds numbers, even worse for the effect of nose bluntness. Reformulating the  $\gamma$  transport equation and modifying the timescale of the second-mode, Zhou et al. [23] made further efforts to improve the  $k-\omega-\gamma$  transition model to reflect the Reynolds number effect and nose bluntness influence more accurately.

Forsaking transition estimation correlations, phenomenological or physics-based models [24,25] are more preferable because the transition mechanisms are taken into consideration directly. However, regarding the fact that the mechanisms of transition are not

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