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A model for multiple transport mechanisms through nanopores of shale gas reservoirs with real gas effect—adsorption-mechanic coupling



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ABSTRACT

Multiple transport mechanisms coexist in nanopores of shale gas reservoirs with complex pore size distribution and different gas-storage processes, including continuum flow, slip flow and transition flow of bulk gas and surface diffusion for adsorbed gas. The force between gas molecules and the volume of the gas molecules themselves cannot be negligible in shale gas reservoirs with high pressure and nanoscale pores, influences gas transport and must be taken into account as a real gas effect. During depressurization development of shale gas reservoirs, the adsorbed gas desorption and a decrease in an adsorption layer influence gas transport. Meanwhile, due to the stress dependence, decreases in intrinsic permeability, porosity and a pore diameter also influence gas transport. In this work, a unified model for gas transport in organic nanopores of shale gas reservoirs is presented, accounting for the effects of coupling the real gas effect, stress dependence and an adsorption layer on gas transport. This unified model is developed by coupling a bulk gas transport model and an adsorbed gas surface diffusion model. The bulk gas transport model is validated with published molecular simulation data, and the adsorbed gas surface diffusion model is validated with published experimental data. The results show that (1) in comparison with the previous models, the bulk gas transport model developed on the basis of a weighted superposition of slip flow and Knudsen diffusion can more reasonably describe bulk gas transport, (2) surface diffusion is an important transport mechanism, and its contribution cannot be negligible and even dominates in nanopores with less than 2 nm in diameter, and (3) the effect of stress dependence on fluid flow in shale gas reservoirs is significantly different from that in conventional gas reservoirs, and is related to not only the shale matrix mechanical properties and the effective stress but also the gas transport mechanisms. © 2015 Elsevier Ltd. All rights reserved.

1. Introduction

Recoverable reserves of shale gas in the United States are estimated to be $24.409 \times 10^{12}\,\mathrm{m}^3$ [1]. Over the past years, profitable production in shale gas reservoirs is a result of technological advancement in horizontal drilling and hydraulic fracturing [2]. Even with significant progress made in production of shale gas reservoirs, gas recovery remains very low, estimated at 10–30% of original gas in place [3]. One of the issues yet to be addressed is the lack of a valid predictive tool for shale-gas production [4]. A model for gas transport in nanopores of shale gas reservoirs is the fundament for numerical simulation and production forecast [5,6].

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Typical organic-rich shale has low porosity (less than 10%) and permeability (ranging from nano Darcy to micro Darcy) [7]. According to the International Union of Pure and Applied Chemistry (IUPAC), classification of a pore size in shale can be divided into ultramicropores (pore diameter <0.7 nm), micropores $(0.7 \text{ nm} \sim 2 \text{ nm})$, mesopores $(2 \text{ nm} \sim 50 \text{ nm})$ and macropores (>50 nm). Small-scale nanopores dominate in shale. The pore volume with a pore radius of less than 10 nm accounts for the total pore volume up to 42% [8]. Some of the pores and the paths connecting the pores have a pore radius of even less than 2 nm and only a small amount of macropores distributes [9]. The effective pore size estimated by Kang et al. shows that shale could be considered as a microporous-mesoporous material [10]. According to a general classification, shale pores can be divided into organic pores and inorganic pores; organic pores account for a significant portion [9]. Shale gas is self-generating and self storage, and free gas, adsorbed gas and dissolved gas coexist in shale gas reservoirs

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Nomenclature

b	gas slippage constant, dimensionless	J_{s}	surface diffusion mass flux for real gas, kg/(m ² ·s)
C_{g}	gas compressibility factor, 1/MPa	$J_{\rm si}$	surface diffusion mass flux for ideal gas, kg/(m ² ·s)
$\tilde{C_{ m k}}$	Knudsen diffusion conductance considering real gas ef-	Jt	total mass flux for real gas, kg/(m²·s)
	fect, s	$J_{\rm v}$	slip mass flux for real gas, kg/(m ² ·s)
$C_{\rm kad}$	Knudsen diffusion conductance considering real gas ef-	J_{vi}	slip mass flux for ideal gas, kg/(m ² ·s)
	fect and adsorption layer, s	K	intrinsic permeability of shale under effective stress
C_{ki}	Knudsen diffusion conductance when gas is considered		condition, m ²
	as ideal gas, s	<i>K</i> n	Knudsen number for real gas, dimensionless
$C_{\rm knon-ad}$	Knudsen diffusion conductance with considering real	<i>K</i> n _i	Knudsen number for ideal gas, dimensionless
	gas effect and without adsorption layer, s	K_{o}	intrinsic permeability of shale at atmospheric pressure,
$C_{\text{knon-str}}$	Knudsen diffusion conductance with considering real		m^2
	gas effect and without stress dependence, s	1	distance along the gas transport direction, m
C_{kstr}	Knudsen diffusion conductance considering real gas ef-	M	gas molar mass, kg/mol
	fect and stress dependence, s	N_A	Avogadro's constant, 6.0221415×10^{23} /mol
$C_{\rm s}$	adsorbed gas surface diffusion conductance, s	p	gas pressure, MPa
$C_{\rm sc}$	adsorbed gas concentration when gas is considered as	p'	gas pressure at certain time during depressurization,
	real gas, kg/m ³		MPa
$C_{\rm sci}$	adsorbed gas concentration when gas is considered as	$p_{\rm c}$	overburden pressure, MPa
	ideal gas, kg/m ³	p_{e}	effective stress, MPa
$C_{\rm si}$	adsorbed gas surface diffusion conductance when gas is	p_{L}	Langmuir pressure, MPa
	considered as ideal gas, s	q	shale porosity coefficient, dimensionless
$C_{\text{snon-str}}$	adsorbed gas surface diffusion conductance with con-	$q_{\rm a}$	standard adsorbed gas volume per unit weight, m ³ /kg
	sidering real gas effect and without stress dependence, s	$q_{ m L}$	Langmuir volume, m ³ /kg
$C_{\rm sstr}$	adsorbed gas surface diffusion conductance considering	R	gas universal constant, J/(mol·k)
	real gas effect and stress dependence, s	r	pore radius under effective stress condition, m
C_{t}	total flow conductance when gas is considered as real	Δr	decreased pore radius due to stress dependence, m
	gas, s	r'	pore radius under effective stress condition at certain
$C_{\rm tad}$	total flow conductance considering real gas effect and		time during depressurization, m
	adsorption layer, s	$r_{ m ad}$	adsorption layer for real gas, m
$C_{\rm ti}$	total flow conductance when gas is considered as ideal	$r'_{\rm ad}$	adsorption layer for real gas at certain time during
	gas, s		depressurization, m
$C_{\text{tnon-ad}}$	total flow conductance with considering real gas effect	$r_{ m adi}$	adsorption layer for ideal gas, m
thon uu	and without adsorption layer, s	$r_{\rm o}$	pore radius under atmospheric pressure, m
$C_{t-non-ini}$	fluence factor total flow conductance without considering	S	shale permeability coefficient, dimensionless
	real gas effect, or stress dependence, or adsorption lay-	T	reservoir temperature, K
	ers, s	t_{M}	the average time required for one collision between the
$C_{\text{tnon-str}}$	total flow conductance with considering real gas effect	•••	gas molecules, s
thon str	and without stress dependence, s	$t_{\rm S}$	the averaged time required for one collision between a
$C_{ m tstr}$	total flow conductance considering real gas effect and		nanopore wall and gas molecule, s
tot.	stress dependence, s	$t_{ m T}$	the average time consumed for one collision of overall
C_{v}	slip flow conductance when gas is considered as real		gas molecules, s
•	gas, s	Ζ	gas deviation factor, dimensionless
C_{vad}	slip flow conductance considering real gas effect and	α	rarified effect coefficient for real gas, dimensionless
vuu	adsorption layer, s	α_1	fitting constant, dimensionless
C_{vi}	slip flow conductance when gas is considered as ideal	α_{i}	rarified effect coefficient for ideal gas, dimensionless
VI	gas, s	α_{o}	rarified effect coefficient when $Kn \to \infty$, dimensionless
$C_{\text{vnon-ad}}$	slip flow conductance with considering real gas effect	β	fitting constant, dimensionless
viioii-au	and without adsorption layer, s	ζmb	the correction factor for bulk gas transport in shale,
$C_{\text{vnon-str}}$	11 0 1 1 1 1 1 1 00	31110	dimensionless
V11011-3t1	and without stress dependence, s	ξms	surface diffusion coefficient in shale, dimensionless
$C_{ m vstr}$	slip flow conductance with considering real gas effect	η	gas viscosity, p _a ·s
VJLI	and stress dependence, s	θ	gas coverage on nanopores wall for real gas, dimension-
$D_{ m f}$	fractal dimension of the pore surface, dimensionless		less
$D_{\rm s}$	surface diffusion coefficient, m ² /s	$\theta_{\mathbf{i}}$	gas coverage on nanopores wall for ideal gas, dimen-
$D_{\rm s}^{ m 0}$	surface diffusion coefficient when gas coverage is "0",	1	sionless
- 3	m^2/s	κ	the ratio of the rate constant for blockage to the rate
$d_{ m m}$	gas molecular diameter, m;		constant for forward migration, dimensionless
	(c) Heaviside function, dimensionless	κ_{b}	the rate constant for blockage, m/s
ΔH	isosteric adsorption heat at the gas coverage of "0",	$\kappa_{ m m}$	the rate constant for forward migration, m/s;
	J/mol	$\lambda_{\rm m}$	molecular mean free path for real gas, m
$J_{ m b}$	total mass flux for bulk real gas, kg/(m ² ·s)	λ_{i}	molecular mean free path for ideal gas, m
$J_{ m bi}$	total mass flux for bulk ideal gas, kg/(m²·s)	λ_{T}	molecular mean free path of the overall gas molecules, m
$J_{\rm ci}$	continuum mass flux for ideal gas, $kg/(m^2s)$	σ	the ratio of normalized molecule size to local average
$J_{\rm k}$	Knudsen diffusion mass flux for real gas, kg/(m ² ·s)	J	pore diameter, dimensionless
$J_{ m ki}$	Knudsen diffusion mass flux for ideal gas, $kg/(m^2 \cdot s)$	τ	tortuosity, dimensionless
JKI		J	
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