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Heat and mass transfer of adult incontinence briefs in computational simulations and objective measurements



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ABSTRACT

This study aims to evaluate the heat and mass transfer of two kinds of multilayer adult incontinence briefs (diapers for short) in the dry condition and dynamic heat and moisture transfer processes in the wet condition in computational simulations and objective measurements. A commercial disposable brief (PROTEC) with polyethylene, superabsorbent polymers (SAP) and polypropylene, and another kind reusable brief (Reusable) with waterproof breathable fabric, full cotton inner pad and moisture management treatment nonwoven were evaluated. A software platform (S-smart system) with user friendly interfaces was employed in computational simulations. Wear trials were conducted by asking young female adults between 20 and 26 years old to wear incontinence briefs. Objective measurements revealed that there was significantly higher liquid moisture management capacity, water vapor permeability, thermal conductance and maximum value of heat flux in the Reusable than in PROTEC briefs. The simulation and wear trial results showed that there were significantly lower temperatures and humidity at the skin in the diaper area and diaper inner surface fabric in the Reusable briefs compared to the PROTEC ones. The good agreement between simulations and wear trials were observed. The 2D and 3D directly visualizes the changes of fabric temperature/humidity gradient and capacity of absorbing moisture etc. in each layer. The results indicate that the superior fabric's heat/moisture transporting properties, when incorporated into diapers, is the main mechanism for reducing heat and wetness of the diaper area. The results provide guidance for the optimal design of Eco-friendly diapers with reusable, breathable, biodegradable materials.

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1. Introduction

Disposable diapers and incontinence pads of adults may be mainly worn by people with medical conditions which cause them to suffer from urinary or fecal incontinence. Since these people are unable to control their bladders or bowels, incontinence products are always used in the wet state. While the degree of skin wetness is proportional to incontinence products wetness, this might cause diaper dermatitis [1]. Additionally, the sensation of wetness in the diaper area also showed a strong association with discomfort [2].

In addition to causing skin wetness, like other clothing, the incontinence products, as an interactive barrier, could affect the heat transfer efficiency. They also block the diffusion of fresh air to the skin. The former depresses the rate of heat loss from the body by conduction and convection [3] and the latter is a key factor in clothing comfort [4]. Therefore, it is important for one to know what impact the wearing of incontinence products with different textile materials has on thermal functional performance.

The evaluations on the comfort performance associated with the heat and moisture transfer behaviors of clothing are divided into three phases:

Phase 1: The evaluations were performed by subjective wearer trials. This was also employed in a study in terms of infants' comfort perception of breathable and non-breathable diapers [2]. Since infants could not express themselves verbally, in this study the adult subjects had to wear diapers to participate in the wear trials, although the products used the standard infant diaper component materials. This case demonstrates that the subjective wearer trials might fail to simulate the practical experimental conditions accurately, leading to the inconsistent results.

Phase 2: The objective simulation tests were developed and expressed by the mathematical modeling and numerical simulation [5–12]. There should have been a more acceptable option, however, since the ways of the complex expression uses mathematical models, relevant computational algorithms and numerical solutions, that limit their extensive uses.

Phase 3: More recently, on the basis of the mathematical modeling and numerical simulation, a software platform, called the S-smart system, was designed and developed [13,14]. This is a

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Nomenclature

Nomenciature			
<i>C</i> *	saturated water vapor concentration, kg m ^{-3}	ms	sweat accumulation on the skin surface in $g s^{-1} m^{-2}$
C_a	water vapor concentration in the air filling the inter-fi-	p_A	proportion of clothing-covered area
υu	ber void space, kg m^{-3}	p_h	proportion of dry heat loss at the clothing-covered area
C_{f}	water vapor concentration in the fibers of the fabric,	p_m	proportion of moisture vapor from the skin at the cloth-
. j	$kg m^{-3}$	rm	ing-covered area
$C_{\rm res}$	dry respiration heat loss, W m^{-2}	S_{v}	surface volume ratio of the fiber, m^{-1}
$C_{\rm skA}$	convective heat loss from the skin in the area covered	S _c	the heat storage of the core, W m^{-2}
5101	by clothing, W m $^{-2}$	S_s	the heat storage of the skin, W m^{-2}
$C_{\rm skU}$	convective heat loss from the skin in the area uncovered	r	fiber radius
	by clothing, W m^{-2}	Rea	evaporation heat resistance on the skin surface, m ² -
c_v	volumetric heat capacity of the fabric, kJ m ^{-3} K ^{-1}		$Pa W^{-1}$
D_a	diffusion coefficient of water vapor in the air of the fab-	Resk	evaporation resistance of the skin, $m^2 Pa W^{-1}$
	ric, $m^2 s^{-1}$	R _{skA}	radioactive heat loss from the skin in the area covered
D_f	diffusion coefficient of water vapor in the fibers of the		by clothing, W m^{-2}
	fabric, m ² s ⁻¹	$R_{\rm skU}$	radioactive heat loss from the skin in the area uncov-
DRY	dry heat loss from human body, W ${ m m}^{-2}$		ered by clothing, W m $^{-2}$
E_{rsw}	evaporative heat loss by regulatory sweating from skin,	$T(T_{fi})$	temperature of the fabric, K
	W m ⁻²	T_{sk}	temperature of skin surface, K
$E_{\rm dif}$	diffusive heat loss from skin surface, W m ^{-2}	T_{cr}	temperature of core, K
Eres	latent respiration heat loss, W m^{-2}	T_r	temperature of the air, K
$E_{\rm skA}$	evaporative heat loss from the skin in the area covered	W	Moisture transfer resistance, s m^{-1}
	by clothing, W m ^{-2}	V_{bl}	skin blood flow rate, $l h^{-1} m^{-1}$
$E_{\rm skU}$	evaporative heat loss from the skin in the area uncov-	Ea	volume fraction of water vapor
	ered by clothing, W m ^{-2}	\mathcal{E}_{f}	volume fraction of fibers
$FL_{(R)}$	elementary total thermal radiation incident inside the	ε_l	volume fraction of liquid phase
r	clothing traveling to the left (right), W m^{-2}	3	porosity of the fabric density of the liquid water, kg m ⁻³
Γ_f	effective sorption rate of the moisture	ρ_l	effective tortuosity of the fabric for water vapor diffu-
$\Gamma_{ m lg} M$	Evaporation/condensation rate of the liquid/vapor metabolic rate of human body, W m ⁻²	$ au_a$	sion
Gs	Incidence of the external thermal radiation, W m ^{-2}	ξ_1	proportions of moisture sorption at fiber surface cov-
1	distance between skin surface and inner surface of	\$ 1	ered by air
ı	clothing or the neighboring clothing layers, m	21	surface tension of fiber, J m ⁻¹
h_{lg}	mass transfer coefficient for evaporation and condensa-	$\gamma \\ \theta$	contact angle of the liquid water on the fiber surface
''Ig	tion, m s ^{-1}	α	effective angle of capillaries in the fabric
Kl	thermal conductivity of the liquid water, W m ^{-1} K ^{-1}	β	radiation absorption constant of the fiber, m^{-1}
K _{min}	minimum thermal conductance of body tissue, W m ^{-2} -	η	dynamic viscosity of liquid, kg $m^{-1} s^{-1}$
•••••••	K^{-1}	λ	heat of sorption or desorption of vapor by fibers, kJ kg $^{-1}$
K _{mix}	effective thermal conductivity of the fabric, W m ^{-1} K ^{-1}	λ	heat of sorption or desorption of liquid by fibers, kJ kg ^{-1}
K	Thermal conductivity of the liquid water, W m ^{-1} K ^{-1}	σ	Stefan–Boltzmann constant, W $m^{-2} K^{-1}$
m _{rsw}	regulatory sweating in g s ⁻¹ m ⁻²		·······

computer aided design tool with user-friendly interfaces which can be operated easily by the common designers, engineers and researchers without professional background knowledge of mathematics and computational techniques. In the earlier work, the thermal functional performances, wearing the hydrophilic and hydrophobic sportswear (single-layer) [13], and personal protective clothing (PPC, two-layer clothing assemblies), were simulated [15]. There was good correspondence between the predicted results and the experimental measurements, on the temperature at the skin, core and inner surface of the clothing, and the humidity in the clothing microclimate, suggesting that the S-smart system is satisfactory. 2D and 3D visualizations of this system further demonstrates the dynamic observations of heat and moisture transfer in clothing. However, the above mentioned simulation tests were limited to single-layer clothing or two-layer clothing assemblies made of common thickness of the fabric. To date, the simulation tests of a multilayer clothing assembly with unusual thickness such as diapers, has not yet been investigated.

Modern incontinence products of adults have a layered construction, which is illustrated in Fig. 1. From outside to inside, the commercial products (Fig. 1(A)) consisted of an outer shell of polyethylene film as a moisture barrier (outer layer), an absorbing layer of a mixture of cotton and superabsorbent polymers (SAP) for wetness (middle layer), and a wicking layer nearest the skin of polypropylene nonwoven material with a distribution layer directly beneath, which transfers wetness to the absorbent layer (inner layer). According to the literature, good water transport properties of incontinence products, such as high absorption capacity, low rewet, and fast strike-through time, are related to wet comfort [16-18]. Our previous study [19] found that the PPC cotton underwear with moisture management treatment (MMT) had significantly higher cumulative one-way moisture transport capacity and liquid moisture management capacity, which made clothing microclimate humidity significantly lower. Meanwhile, PPC outerwear made of waterproof breathable fabric had significantly higher water vapor permeability and thermal conductance, which helped clothing to speed up the evaporation process and heat dissipation. Based on the previous study, we extend our investigation to the newly designed incontinence products, which are hybrids of reusable briefs made of waterproof breathable fabric and disposable inner pads. The pads consisted of a replaced inner layer of full cotton nonwoven with MMT and an outer layer made of very thin breathable paper for the construction of the holding pads, and the same SAP/cotton absorbent middle layer, due to

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