

Two-dimensional bubble rising through quiescent and non-quiescent fluid: Influence on heat transfer and flow behavior



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ABSTRACT

An understanding of the bubble properties, size distributions and shapes and their ability in various applications is of fundamental importance for comprehending flow dynamics and mass transfer phenomena in bubble column reactors. A large number of studies have focused on open tube bubble columns, and the knowledge concerning bubble columns is still limited. In this paper, a 2D phase field model is presented for numerical study of a bubble rising in a fluid and its influence on heat transfer parameters on a single channel. The computational model entails the Navier–Stokes equation for fluid flow and VOF (Volume of fluid) model for interface deformation and morphology. A C++ based open source software; OpenFOAM is utilized for this simulation. It is found that rising bubble can be used as an effective method for reducing thermal boundary layer and increasing Nusselt number and consequently increasing heat transfer in industrial applications. Investigating the influence of the bubble rising on the non-quiescent fluid in a vertical channel revealed that bubble rising in high Reynolds number does not have sensible effect on Nusselt number, but in low Reynolds number it shows a significant enhancement in Nusselt number. Also the results predicted that bubble injection frequency has a direct effect on Nusselt number behavior.

1. Introduction

Multi-phase fluid systems play an important role in many natural and industrial processes such as combustion, petroleum refining, chemical engineering and cleaning. Rising of a bubble in a liquid is one of the typical dynamics of multi-fluid systems. A sound understanding of the fundamentals of the rising bubble is crucial in a variety of practical applications ranging from the rise of steam in boiler tubes to gas bubbles in oil wells. Numerical modeling of a rising bubble in a fluid medium can be rather difficult because of the singularity-like discontinuity of fluid properties such as density and viscosity, and of the pressure jump across the interface due to surface tension. Useful computational schemes have been developed to overcome the difficulties; some popular approaches include the volume of fluid [1], level set, phase field and front tracking [2]. Chen et al. [3] and Maxworthy [4] for vapor bubbles moving under a submerged surface in water, they concluded that bubble velocity increases with bubble volume and plate angle, reaching a maximum at an angle of 50° to the horizontal. In a study by Brucker [5], PIV (Particle Image Velocimetry) was used to obtain the temporal evolution of the flow field in the near wake of single rising bubbles of 5–7 mm diameter in water. Shin and Choi [6] proposed the efficient and stable way of sharp energy method for two-

phase flow with phase. They simulated a bubble rise with phase change and compared with experimental data. The bubble growth rate from the simulation was well compared with experiment. Liu and Palm [7] investigated a three dimensional numerical study on bubble growth and merger in a micro-channel with diameter of 0.64 mm with R134a as working fluid. They found that the evaporation rate is much higher in the first two stages due to the thermal boundary layer effects. Dhole et al. [8] studied Mass transfer from a spherical bubble rising in power-law fluids at intermediate Reynolds numbers. Based on their presented numerical results, a simple mass transfer correlation was developed to estimate the value of Sherwood number in a new application. The dynamics of a vapor bubble between its liquid phase and a heated plate studied in relation to the breakdown and recovery of the film boiling by Joo and Park [9]. They focused on the effects of the degree of superheat from the solid plate, and the wetting/dewetting characteristics of the liquid on the solid plate. Zhang et al. [10] studied an SPH modeling of bubble rising and coalescing in three dimensions. Several cases of single bubbles rising through viscous fluids are tested and the SPH results validated by both the experimental data and other numerical results. Furthermore, the phenomena of bubbles coalescing in both vertical and horizontal directions simulated. The flow and heat transfer of MHD nanofluid between parallel plates in the presence of thermal radiation

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Nomenclature

C_{p_g} (J/kg.K) Gas heat capacity
 ρ (kg/m³) Liquid density
 C_p (J/kg.K) Liquid heat capacity
 $\hat{\rho}$ (kg/m³) Gas density
 K (W/m.K) Liquid heat conductivity
 ρ_b (kg/m³) Bulk density
 K_g (W/m.K) Gas heat conductivity
 ν_t (m²/s) Turbulant Kinitic Viscosity
 L (m) Duct height
 $\hat{\nu}$ (m²/s) Gas Kinitic Viscosity
 P (Pa) Pressure
 ν_l (m²/s) Liquid Kinitic Viscosity
 F_s (N) surface tension force
 μ_l (Kg.m/s) Liquid Dynamic Viscosity

T_{in} (K) Initial gas and liquid temperature
 $\hat{\mu}$ (Kg.m/s) Gas Dynamic viscosity
 T_{hot} (K) Hot wall temperature
 μ_b (Kg.m/s) Bulk Dynamic viscosity
 t (s) Simulation time step
 λ_l Liquid Phase Conductivity
 U (m/s) Velocity
 $\hat{\lambda}$ Gas Phase Conductivity
 W (m) Duct width
 λ_b Local Average Conductivity

Greek symbols

α Volume Fraction
 τ (N/m) Surface Tension

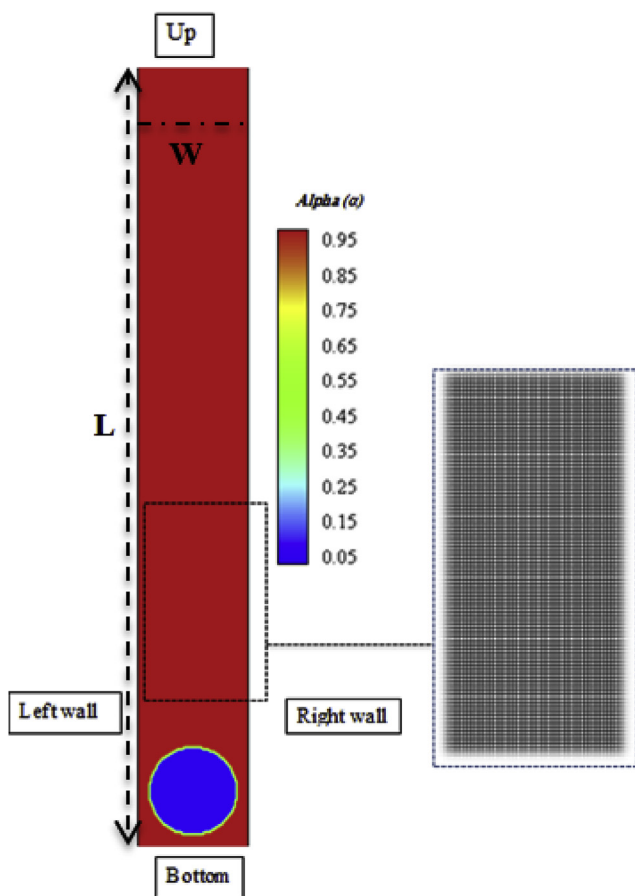


Fig. 1. Geometry of the problem.

was studied by Dogonchi et al. [11]. The effects of various parameters such as the squeeze number, the magnetic parameter, the volume fraction of nanofluid, the Eckert number and the radiation parameter investigated on the velocity and temperature in their study. Observations of coalescence between different size bubbles during pool nucleate boiling of water on a horizontal, electrically-heated titanium foil by Golobic at al [12]. revealed evidence of asymmetrical interactions between the bubbles before coalescence. They suggested that a fast

Table 1
Simulation parameters quantities.

| Parameter | Description | Value |
|-------------------------------|------------------------------------|--------------------|
| Properties | | |
| t (s) | Simulation time step | 0.00005 |
| ν_l (m ² /s) | liquid dynamic viscosity | 1×10^{-4} |
| ρ (kg/m ³) | Liquid density | 1000 |
| C_p (J/kg.K) | Liquid heat capacity | 1000 |
| K (W/m.K) | Liquid heat conductivity | 10 |
| ν_g (m ² /s) | Gas dynamic viscosity | 1×10^{-4} |
| ρ_g (kg/m ³) | Gas density | 10 |
| C_{p_g} (J/kg.K) | Gas heat capacity | 1000 |
| K_g (W/m.K) | Gas heat conductivity | 0.025 |
| τ (N/m) | Surface tension | 0.1 |
| T_{in} (K) | Initial gas and liquid temperature | 293 |
| T_{hot} (K) | Hot wall temperature | 393 |

Table 2
First case boundary layers which is considered in this study (quiescent liquid).

| quiescent liquid case | |
|-----------------------|-----------------------------|
| geometry parts | Boundary condition |
| Bottom | Wall |
| up | Wall |
| Right and left walls | Wall (Constant Temperature) |

Table 3
Boundary conditions for the second case, bubble rising in a non-quiescent liquid.

| non-quiescent liquid case | |
|---------------------------|-----------------------------|
| geometry parts | Boundary condition |
| Bottom | Velocity inlet |
| up | Pressure outlet |
| Right and left wall | Wall (Constant temperature) |

growing bubble could push superheated liquid under a more slowly growing bubble. Bubble coalescence was also experimentally studied by Coulibaly et al. [13] who showed that the heat transfer was enhanced only when the coalescence occurred at least 2 ms after bubble

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