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Simulation of the ozone pretreatment of wheat straw

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HIGHLIGHTS

- Two models for ozonolysis pretreatment of wheat straw were developed.
- First study that takes into account the residual lignin.
- Compared cuticle model with the existing general model for ozonolysis of biomass.
- Cuticle model better fit with experimental data.

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ABSTRACT

Wheat straw is a potential feedstock in biorefinery for sugar production. However, the cellulose, which is the major source of sugar, is protected by lignin. Ozonolysis deconstructs the lignin and makes cellulose accessible to enzymatic digestion. In this study, the change in lignin concentration with different ozonolysis times (0, 1, 2, 3, 5, 7, 10, 15, 20, 30, 60 min) was fit to two different kinetic models: one using the model developed by Garcia-Cubero et al. (2012) and another including an outer mass transfer barrier or "cuticle" region where ozone mass transport is reduced in proportion to the mass of unreacted insoluble lignin in the cuticle. The kinetic parameters of two mathematical models for predicting the soluble and insoluble lignin at different pretreatment time were determined. The results showed that parameters derived from the cuticle-based model provided a better fit to experimental results compared to a model without a cuticle layer.

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1. Introduction

Wheat straw is an agricultural byproduct of wheat that is annually produced in abundance around the world. The world's wheat production in 2014 was 716 Tg (USDA (2014). Assuming a residue/crop ratio of 1.3 (Talebnia et al., 2010), about 931 Tg of total wheat residue is annually produced. If 60% is used for ground cover to prevent soil erosion 559 Tg of wheat straw is available as waste. Wheat straw is composed of lignin (15–20%), celluloses (33–40%), and hemicelluloses (20–25%) (Talebnia et al., 2010). The lignin in the wheat straw is made up of monomer units such as p-hydroxy phenyl-guaiacyl-syringyl (H-G-S) lignin, and contains approximately 5, 49, and 46% of H, G, and S units, respectively (Lapierre et al., 1995). In order to utilize structural carbohydrates of the wheat straw in a biochemical biorefinery setting, a pretreatment process is necessary to disrupt the recalcitrant structure of mainly lignin. Pretreatment is known to increase the susceptibility of cellulose and hemicellulose to cellulolytic enzymes for the production of fermentable sugars. The main goal of pretreatment process is to increase the surface area and porosity of the substrate, reduce the crystallinity of the cellulose, degrade hemicellulose and lignin, and disrupt the heterogeneous structure of the cellulosic materials (Talebnia et al., 2010). The pretreatment processes are of four types: physical, physico-chemical, chemical, and biological. Physical pretreatment is based on size reduction of the wheat straw by means of milling, grinding, or chipping (Pedersen and Meyer, 2009). Liquid hot water (Petersen et al., 2009), steam explosion (Ballesteros et al., 2006), and ammonia fiber explosion (Sun and Cheng, 2002) are the physico-chemical pretreatment methods. The use of acids, alkalines, and oxidizing agents for the pretreatment of wheat straw is known as chemical pretreatment (Saha et al., 2005). The pretreatment by means of microorganisms such as white and soft rot fungi are types of biological pretreatment (Talebnia et al., 2010).





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Nomenclature

CI_i	confidence intervals	$R_{1,S}$	reaction kinetics, kg _{Straw} . kg_sLg/min
C _{ii}	ith diagonal element of covariance matrix	$R_{2,S}$	reaction kinetics, kg _{Straw} . kg_sLg/min
Cov	covariance matrix	SE	standard error
DF	degree of freedom	sLg	soluble lignin, kg_sLg/kg _{Straw}
Do_3	diffusion coefficient, m ² /s	sLg _c	soluble lignin in cuticle, kg_sLg/kg _{Straw}
d_p	diameter of particle, m	sLg _{c.Model.}	predicted soluble cuticle lignin, kg_sLg/kg _{Straw}
iĹg	insoluble lignin, kg_iLg/kg _{Straw}	sLg _{c.Exp.i}	experimental soluble lignin, kg_sLg/kg _{Straw}
iLg _c	insoluble lignin in cuticle, kg_iLg/kg _{Straw}	sLg _{ModeLi}	predicted soluble lignin, kg_sLg/kg _{Straw}
iLg _{c.o}	initial insoluble lignin in cuticle, kg_iLg/kg _{Straw}	sLg _s	soluble lignin of solid, kg_sLg/kg _{Straw}
iLg _{c.Model.i}	predicted insoluble cuticle lignin, kg_iLg/kg _{Straw}	Т	time, min
iLg _{Exp.i}	experimental insoluble lignin, kg_iLg/kg _{Straw}	$t_{\alpha/2.Df}$	student's t inverse cumulative distribution
iLg _{Model.i}	predicted insoluble lignin, kg_iLg/kg _{Straw}	U	velocity, m/sec
iLg _s	insoluble lignin of solid, kg_iLg/kg _{Straw}	V_s	voluble of solid, m ³
J	Jacobian matrix	W_s	weight of solid, kg
k_1	reaction rate, kg _{Straw} /kg_iLg/min	Ζ	distance, m
k_2	reaction rate, kg _{Straw} /kg_sLg/min		
$K_{O,CS}a_p$	mass transfer coefficient between cuticle and the inte-	Greek	
	rior solid, 1/min	α_1, α_4	stoichiometric, dimensionless
$K_{O,GC}a_p$	mass transfer coefficient between gas phase and the	α_2	stoichiometric, kg_iLg/kg_O _{3 S}
	cuticle, 1/min	a,	stoichiometric, kg sLg/kg O_{35}
$K_{O,S}a_p$	mass transfer coefficient between gas phase and solid	as	stoichiometric, kg sLg/kg O_{35}
	phase, 1/min	3	void fraction, dimensionless
Κ	condition number	$\rho_{\rm S} \rho$	density of solid, kg/m ³
0 _{3,C}	ozone in the cuticle, <i>kg_O_{3,S}/kg_{Straw}</i>	λ_c	cuticle lignin fraction, dimensionless
O _{3,G}	ozone in the gas phase, <i>kg_O_{3,G}/kg_{Straw}</i>	щ	dynamic viscosity, pa sec
O _{3,S}	ozone in the solid phase, <i>kg_O_{3,S}/kg_{Straw}</i>	$\kappa_{\rm hr}$	permeability, m ²
θ_i	best fit parameter	λ_{max}	largest eigen value
Р	pressure, pa	λ_{min}	smallest eigen value
Р	products	β_F	Forchheimer drag coefficient, kg/m ⁴
PI	prediction interval	φ	sphericity, dimensionless
R_1	reaction kinetics, kg _{Straw} . kg_sLg/min	Δ	square root of machine precision
R_1	reaction kinetics, kg _{Straw} . kg_sLg/min	Α	confidence interval
$R_{1,C}$	reaction kinetics, kg _{Straw} . kg_sLg/min		
$R_{2,C}$	reaction kinetics, kg _{Straw} . kg_sLg/min		

Ozone pretreatment uses ozone as an oxidizing agent. Ozone is a very powerful oxidizing species with an oxidation potential of 2.07 eV (Mandavgane and Yenkie, 2011). There are many advantages of the ozone pretreatment process compared to other pretreatment techniques. For instance, ozone causes minimal degradation of cellulose and hemicelluloses due to the considerably higher reaction rate of ozone with substituted aromatic molecules such as lignin. The ozonation process also does not produce toxic compounds and can be performed at room temperature and pressure, which reduces the capital and energy costs (Neely, 1984). In addition, earlier studies demonstrated efficiency of ozone pretreatment to improve sugar release during enzymatic hydrolysis (Bule et al., 2013; García-Cubero et al., 2009; Wu et al., 2013).

The majority of studies involving the ozonation pretreatment of lignocellulose required a relatively long residence time in the reactor, typically 60 min or greater. As a result, utilizing ozone as a sole pretreatment process for lignocellulose can be unpractical. The study demonstrating ozonolysis of wheat straw and rye straw which increased sugar yield from 29% and 16% (untreated) to 88.6% and 57% (ozone treated), respectively (untreated) (García-Cubero et al., 2009) required 2.5 h of ozone exposure. Also, the ozonolysis of sugarcane bagasse showed an increase in glucose yield from 6.64% (untreated) to 52.44% (ozone treated) after 120 min of ozone pretreatment (Travaini et al., 2013). In contrast, the ozonolysis (for 120 min) of energy grasses showed a lower sugar yield compared to untreated energy grasses after enzymatic hydrolysis (Panneerselvam et al., 2013). These

kg/m⁴ on observations suggest that the applicability of ozone pretreatment depends upon the biomass characteristics. In order to make ozone pretreatment economically feasible, its optimization either through better elucidation of the ozone interaction with lignin or

needed. Although many studies have been conducted on the ozonolysis process, mathematical models explicitly predicting ozone lignin degradation phenomena are rare. García-Cubero et al. (2012) introduced a model to characterize the effects of ozonation on the insoluble and soluble lignin (MBachu and Manley, 1981) content of biomass. However, the model presented by García-Cubero et al. (2012) did not take into account the residual lignin that remained unaffected by the ozone. In contrast, their model predicts that prolonged ozone exposure removes lignin completely which contradicts experimental results where lignin concentration reaches a plateau.

through the reduction of the overall pretreatment time is urgently

Several attempts have been made in the development of numerical models for the ozone lignin interaction process. The kinetic model proposed by Binder et al. (1980) showed that the ozone lignin interaction has two different kinetic behaviors: a falling rate phase followed by a constant rate phase, however, only the falling rate period was addressed in their model. MBachu and Manley (1981) suggested that lignin degradation follows first-order kinetics, and they derived the first order reaction equation of lignin degradation of ozone treated spruce periodate and spruce cuoxam lignin as follows:

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