



Review

Enhanced biological phosphorus removal and its modeling for the activated sludge and membrane bioreactor processes


M.F.R. Zuthi^a, W.S. Guo^a, H.H. Ngo^{a,*}, L.D. Nghiem^b, F.I. Hai^b
^a Centre for Technology in Water and Wastewater, School of Civil and Environmental Engineering, University of Technology Sydney, Sydney, NSW 2007, Australia

^b Strategic Water Infrastructure Laboratory, School of Civil Mining and Environmental Engineering, Faculty of Engineering, University of Wollongong, NSW 2522, Australia

HIGHLIGHTS

- MBR's system and operational constraints may affect phosphorus removal efficiency.
- ASM-based models for P-removal need to be modified for a particular MBR system.
- Impact of P-removal kinetics on sludge properties should be considered in modeling.

ARTICLE INFO

Article history:

Received 17 February 2013

Received in revised form 8 April 2013

Accepted 10 April 2013

Available online 18 April 2013

Keywords:

Enhanced biological phosphorus removal

Membrane bioreactor

Mathematical modeling

Activated sludge process

ABSTRACT

A modified activated sludge process (ASP) for enhanced biological phosphorus removal (EBPR) needs to sustain stable performance for wastewater treatment to avoid eutrophication in the aquatic environment. Unfortunately, the overall efficiency of the EBPR in ASPs and membrane bioreactors (MBRs) is frequently hindered by different operational/system constraints. Moreover, although phosphorus removal data from several wastewater treatment systems are available, a comprehensive mathematical model of the process is still lacking. This paper presents a critical review that highlights the core issues of the biological phosphorus removal in ASPs and MBRs while discussing the inhibitory process requirements for other nutrients' removal. This mini review also successfully provided an assessment of the available models for predicting phosphorus removal in both ASP and MBR systems. The advantages and limitations of the existing models were discussed together with the inclusion of few guidelines for their improvement.

© 2013 Elsevier Ltd. All rights reserved.

1. Introduction

Controlling phosphorous (P) discharge has become a global issue in preserving surface water quality since it has been identified as the key element responsible for eutrophication in the aquatic environment. The modification of activated sludge systems for phosphorus removal (P-removal) was notably introduced through the enhanced biological phosphorus removal (EBPR) system in the late 1950s (Wentzel et al., 2008). Since then, several modifications to the EBPR systems have been proposed in the literature (Peng and Ge, 2011; Yuan and Oleszkiewicz, 2011). In the EBPR treatment system, the phosphate accumulating organisms (PAOs) of the bacterial community are enriched to accumulate large quantities of polyphosphate (poly-P) in their cells and thus enhance the biological phosphorus removal (bio-P-removal) from wastewater.

The PAOs have a strict requirement of cyclic anaerobic, anoxic and aerobic conditions which consequently makes the bio-P-removal process from wastewater a more complex one compared to the nitrogen (N) and chemical oxygen demand (COD) removal.

Biological nutrient removal (BNR) efficiencies of activated sludge processes (ASPs) and the improved variations thereof suffer from critical sensitivity to various system parameters such as sludge retention time (SRT), hydraulic retention time (HRT), alkalinity and pH, temperature and various other factors. Since MBR is a modified version of ASP with the secondary clarifier of conventional ASP replaced by the membrane separator, it also tends to suffer from the similar bioprocess system constraints of ASPs affecting its nutrient removal efficiency. Although a better overall nutrient removal efficiency of MBRs over that of the ASPs has been reported (Daigger et al., 2010; Lesjean et al., 2003), the typically longer SRT and higher mixed liquor suspended solids (MLSS) concentration frequently hinder the P-removal efficiency of the MBR treatment system. Application of MBR systems in order to meet effluent quality targets for P-removal is possible if the biological processes particularly related to P-removal could be completely understood and linked to other biological process parameters.

* Corresponding author. Address: University of Technology, Sydney School of Civil and Environmental Engineering, Center for Technology in Water and Wastewater, Building 2, Level 5, No. 1 Broadway, Sydney NSW 2007, Australia. Tel.: +61 2 95142745; fax: +61 2 95142633.

E-mail address: h.ngo@uts.edu.au (H.H. Ngo).

Nomenclature

A_2N	anaerobic–anoxic/nitrifying	n_{mPAO}	reduction factor for anoxic endogenous respiration of X_{PAO}
A_2O	anaerobic–anoxic–oxic	$n_{mPAO,Stor}$	reduction factor for anoxic respiration of X_{PHA}
AEI	aerobic/extended-idle	$NO_{(x)}$	nitrite/nitrate
ASM	activated sludge model	NO_3-N	nitrate-N
ASP	activated sludge process	NPFMBR	nearly plug flow MBR
bio-P	biological phosphorus	n_{qPAO}	reduction factor for denitrifying processes
BNR	biological nutrient removal	n_{iPAO}/S_{PAO}	reduction factor for anoxic growth of X_{PAO}
BNRAS	BNR system	OHOS	ordinary heterotrophic organisms
BNRM1	BNR model 1	P	phosphorus
b_{PAO}	endogenous respiration rate of X_{PAO}	PAOs	phosphate accumulating organisms
b_{pp,PO_4}	rate constant for lysis of X_{pp}	PHA	polyhydroxyalkanoates
$b_{Stor,VFA}$	rate constant for respiration of X_{Stor}	PHB	polyhydroxybutyrate
C	carbon	PO_4-P	phosphate-P
CAS	conventional activated sludge	poly-P	polyphosphate
COD	chemical oxygen demand	q_{Gly}	rate constant for formation of X_{GLY}
DPAOs	denitrifying PAOs	$q_{PAO,PO_4,PP}/q_{pp}$	rate constant for storage of X_{pp}
EBPR	enhanced biological phosphorus removal	$q_{PAO,SB,Stor}$	rate constant for S_A uptake rate (X_{PHA} storage)
EPS	extra-cellular polymeric Substances	$q_{PAO,VFA,PHA,An}$	rate constant for S_A uptake rate (X_{PHA} storage) (anaerobic)
F/M	food to microorganism ratio	$q_{PAO,VFA,PHA,Ax}$	rate constant for S_A uptake rate (X_{PHA} storage) (anoxic)
FCASM1	fully coupled ASM1	$q_{PAO,VFA,Stor}$	rate constant for S_A uptake rate (X_{PHA} storage)
$f_{Gly_PAO,Max}$	maximum ratio of X_{GLY}/X_{PAO}	q_{PHA_PAO}	rate for X_{PHA} consumption (X_{PAO} growth)
$f_{pp_PAO,Max}/K_{max}$	maximum ratio of $X_{PAO,PP}/X_{PAO}$	S_A	fermentation product (volatile fatty acids)
$f_{SU_PAO,lys}$	fraction of S_I generated in X_{PAO} decay	S_{ALK}	alkalinity (HCO_3^-)
$f_{XU_PAO,lys}$	fraction of X_I generated in X_{PAO} decay	SBMBR	sequencing batch MBR
GAOs	glycogen accumulating organisms	SBR	sequencing batch Reactor
HRT	hydraulic retention time	SMP	soluble microbial products
K_2PO_4	dipotassium Phosphate	SN_2	dissolved nitrogen gas
$K_{Alk,PAO}$	half-saturation coefficient for S_{ALK}	SNH	ammonium and ammonia nitrogen ($NH_4 + NH_3$)
K_{fGly_PAO}	half-saturation coefficient for X_{GLY}/X_{PAO}	S_{NO}	nitrate and nitrite ($NO_3 + NO_2$) (considered to be NO_3 only for stoichiometry)
K_{TPHA_PAO}	half-saturation coefficient for X_{PHA}/X_{PAO}	S_O	dissolved oxygen
K_{fStor_PAO}	saturation constant for X_{PHA}/X_{PAO}	S_{PO_4}	soluble inorganic phosphorus
$K_{fStor_PAO,Plim}$	half-saturation coefficient for X_{PHA}/X_{PAO} (P limit)	SRT	sludge retention time
$K_{Gly,PAO}$	half-saturation coefficient for X_{GLY}	S_S	soluble biodegradable organics
K_{i,pp_PAO}	half-inhibition coefficient for X_{pp}/X_{PAO}	SSMBR	sponge submerged MBR
$K_{NHx,PAO}$	half-saturation coefficient for S_{NH}	TOC	total organic carbon
$K_{NOx,PAO}$	half-saturation coefficient for S_{NO}	TP	total phosphorus
$K_{O_2,PAO}$	half-saturation coefficient for S_O	TSS	total suspended solids
$K_{PHA,PAO}$	half-saturation coefficient for X_{PHA}	VFA	volatile fatty acid
$K_{PO_4,PAO,lys}$	half-saturation coefficient for X_{PHA} lysis (phosphorus continuity)	WWTP	wastewater treatment plant
$K_{PO_4,PAO,nut}$	half-saturation coefficient for S_{PO_4} as nutrient (X_{PAO} growth)	X_{GLY}	stored glycogen in PAOs
$K_{PO_4,PAO,upt}$	half-saturation coefficient for S_{PO_4} uptake (X_{pp} storage)	X_I	particulate undegradable organics
$K_{pp,PAO}$	half-saturation coefficient for X_{pp}	X_{MeOH}	metal hydroxide compounds
K_{S,pp_PAO}	maximum ratio of X_{pp}/X_{PAO}	X_{MeP}	metal phosphate compounds
$K_{SB,PAO}$	half-saturation coefficient for S_S	X_{PAO}	phosphorus accumulating organisms
$K_{VFA,PAO}$	half-saturation coefficient for S_A	X_{PHA}	storage compound in PAOs
MBR	membrane bioreactor	X_{pp}	stored polyphosphates in PAOs
MEBPR	membrane EBPR	X_{Sto}	storage compound in OHOS
MLSS	mixed liquor suspended solids	Y_{H_2}	yield for OHS growth(aerobic)
MLVSS	mixed liquor volatile suspended solids	Y_{NADH_ATP}	ATP produced per NADH or P/O ratio
$m_{PAO,An}$	maintenance rate for X_{PAO} (anaerobic)	Y_{PAO}	yield for X_{PAO} growth per X_{PHA}
$m_{PAO,Ax}$	maintenance rate for X_{PAO} (anoxic)	$Y_{PAO,Ax}$	yield for X_{PAO} growth per X_{PHA} (anoxic)
m_{PAO,O_2}	observed oxygen consumption for maintenance	$Y_{PAO,Ox}$	yield for X_{PAO} growth per X_{PHA} (aerobic)
$m_{PAO,Ox}$	maintenance rate for X_{PAO} (aerobic)	$Y_{PAO_Gly,Ax}$	yield for formation of X_{GLY} (anoxic)
$m_{PAO,Stor}$	rate constant for respiration of X_{PHA}	$Y_{PAO_Gly,Ox}$	yield for formation of X_{GLY} (aerobic)
N	nitrogen	$Y_{PAO_PP,Ax}$	yield for X_{pp} formation per X_{PAO} (anoxic)
N_2O	nitrous oxide	$Y_{PAO_PP,Ox}$	yield for X_{pp} formation per X_{PAO} (aerobic)
$n_{bPP_PO_4}$	reduction factor for anoxic lysis of X_{pp}	$Y_{PHA_PAO,Ax}$	yield for consumption of X_{PHA} per X_{PAO} formation (anoxic)
NDEBPR	nitrification denitrification EBPR	$Y_{PHA_PAO,Ox}$	yield for consumption of X_{PHA} per X_{PAO} formation (aerobic)
NITs	nitrifiers		
n_{KNOx}	reduction factor for K_{NO} for X_{pp} formation		
n_{KO_2}	reduction factor for $K_{O_2,PAO}$ for X_{pp} formation		

Download English Version:

<https://daneshyari.com/en/article/7082176>

Download Persian Version:

<https://daneshyari.com/article/7082176>

[Daneshyari.com](https://daneshyari.com)