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**Evolutionary Fixed-Structure Controller Tuning Against Multiple Requirements**  $\frac{1}{2}$  Fixed-Structure Controller Tuning Against Multiple Republican Against  $\frac{1}{2}$ 

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multiple requirements. Based on evolutionary computation, it allows solving control problems based on complex specifications, i.e. criterion whose gradients or sub gradients can't be easily formulated: thus it appears to be well adapted to the industrial framework. The tool is described and few examples show its efficiency in computing fixed-structure controller against complex specifications. **Abstract:** This work deals with a new *Matlab* tool for computing fixed-structure controller against efficiency in computing fixed-structure controller against complex specifications. complex specifications, i.e. criterion whose gradients or sub gradients can't be easily formulated: thus it efficiency in computing fixed-structure controller against complex specifications. *philippe.feyel@sagem.com* 

 $\odot$  2016, IFAC (International Federation of Automatic Control) Hosting by Elsevier Ltd. All rights reserved. *Keywords*: Evolutionary Optimization, Robust Control, Controller Tuning, H-infinity, Fixed-Structure. *Keywords*: Evolutionary Optimization, Robust Control, Controller Tuning, H-infinity, Fixed-Structure. *Keywords*: Evolutionary Optimization, Robust Control, Controller Tuning, H-infinity, Fixed-Structure. *Keywords*: Evolutionary Optimization, Robust Control, Controller Tuning, H-infinity, Fixed-Structure.  $\heartsuit$  zoto, if  $\text{AC}$  (international rederation of Automatic Control) flosting by Elsevier Lt

## 1. INTRODUCTION 1. INTRODUCTION 1. INTRODUCTION 1. INTRODUCTION

In the industrial framework, the control engineer must design a unique control law that valid on a single prototype, with a a unique connor in many sufficient degree of robustness to satisfy a complex high level sufficient degree of robustness to satisfy a complex high level<br>close-loop specification on many systems. As shown in Fig. 1, the specification is very often in the form of requirements  $r$ , the specification is very often in the form of requirements related to  $m$  any quantities (here noted  $Z_j$ ). In the industrial framework, the control engineer must design a unique control law that valid on a single prototype, with a



Fig. 1. Close-loop with high level specification Fig. 1. Close-loop with high level specification To assist in his task, H∞ synthesis (Doyle *et al*., 1989) has Fig. 1. Close-loop with high level specification

To assist in his task, H<sub>∞</sub> synthesis (Doyle *et al.*, 1989) has emerged as an efficient tool for robust control in the emerged as an embedded to her recessor center. In the industrial community. However, this approach is well known maasum community. However, this approach is well known<br>to have two major drawbacks. 10 assist in his task,  $H_{\infty}$  synthesis (Doyle *et al.*, 1989) has emerged as an efficient tool for robust control in the to have two major drawbacks.

First, the choice of the "best" weighting filters, used to shape close-loop transfers, is a hard task, as they are supposed to express as close as possible numerous and complex express as close as possible numerous and complex specifications. For that purpose, a very time-consuming  $i$  term all specifications. The controller satisfying all specificative procedure has to be used in the design process to get  $\alpha$  controller satisfying all specifications. First, the choice of the best weighting filters, used to shape close-loop transfers, is a hard task, as they are supposed to specifications. For that purpose, a very time-consuming a controller satisfying all specifications.

Secondly, it is also well known that the order of  $H_{\infty}$ controllers is high: it is equal to that of the synthesis model controllers is high: it is equal to that of the synthesis model and the weights. Thus the classical approach is to a posteriori Secondly, it is also well known that the order of  $H_{\infty}$ and the weights. Thus the classical approach is to a posteriori simplify this controller but with the loss of guarantees on the overall optimality and the specification fulfilment. simplify this controller but with the loss of guarantees on the overall optimality and the specification fulfilment.

simplify this controller but with the loss of guarantees on the

In this paper, we try to make the methodology for computing controllers be more efficient and more direct with a less controllers be more efficient and more direct with a less<br>costly development time by calculating a structured controller directly optimized on the high level specification. For that purpose, we introduce *HinfStoch\_ControllerTuning*, provided that the form of *m* and *provided that high level specifications* are in the mumerical *Matlab* tool for computing such controllers a new numerical *Matlab* tool for computing such controllers provided that high level specifications are in the form of *m* evaluable requirements  $Z_1 < Z_1, Z_1 < Z_2, ..., Z_m < Z_m$ . In this paper, we try to make the methodology for computing provided that high level specifications are in the form evaluable requirements  $Z_1 < \overline{Z}_1$ ,  $Z_1 < \overline{Z}_2$ , ...,  $Z_m < \overline{Z}_m$ . In this paper, we try to make the methodology for computing For that purpose, we introduce *HinfStoch\_ControllerTuning*,  $Z_1 \times Z_1, Z_2 \times Z_2, ..., Z_m \times Z_m$ .

Here the optimization of complex criterion is made possible by the use of efficient evolutionary optimization dedicated to by the use of efficient evolutionary optimization dedicated to structured control problems (Feyel et al., 2014). Indeed, such techniques do not need to formulate gradients, the only constraint being the capability of evaluating criterion. Due to time compute consuming calculation of consuming calculation  $\frac{1}{2}$  and  $\frac{1}{2}$  are solved in the stochastic optimization, the main drawback deals with the time consuming calculation, of course quite reasonable in the consuming calculation, or course quite reasonable in comparison with the *try and error* iterative procedures used comparison with the *try and error* iterative procedures used<br>to tune weighting functions. Here the optimization of complex criterion is made possible Here the optimization of complex criterion is made possible structured control problems (Feyel *et al*., 2014). Indeed, such constraint being the capability of evaluating criterion. Due to to tune weighting functions.

This tool can be viewed as a complementary tool to other powerful commercial tools such as *Looptune* (Gahinet et al., 2011) and more recently *Systune* (Apkarian, 2013) both based on non-smooth optimization. Indeed, Systune allows tuning fixed-structure controller towards predefined criterion tuning fixed-structure controller towards predefined criterion (whose gradients or sub gradients are known) such as step time responses, gain of close-loop transfers, stability in multiple plant case, etc… Examples have shown its multiple plant case, etc… Examples have shown its mattepte plant case, etc… Examples have shown its efficiency (Mathworks, 2014). powerful can be viewed as a complementary tool to other based on non-smooth optimization. Indeed, S*ystune* allows (whose gradients or sub gradients are known) such as step time responses, gain of close-loop transfers, stability in efficiency (Mathworks, 2014).

*HinfStoch\_ControllerTuning* has key features which make its use very interesting in the industrial framework: HinfStoch\_ControllerTuning has key features which make its *HinfStoch\_ControllerTuning* has key features which make its<br>use you interesting in the industrial framework: use very interesting in the industrial framework:

- Any kind of requirements may be optimized provided that they can be evaluated ; thus complex provided that they can be evaluated ; thus complex provided that they can be evaluated ; thus complex criterion such as in (Anderson, 2010) can be optimized, optimized,  $\epsilon$  opumized, - Any kind of requirements may be optimized <sup>7</sup>Hily kind of requirements may be optimized criterion such as in (Anderson, 2010) can be
- Experimental data (such as disturbances temporal experimental data (such as distancements temporaries) can be directly used for the controller computation, computation, computation, - Experimental data (such as disturbances temporal - Experimental data (such as disturbances temporal records) can be directly used for the controller
- Parallel computation (Luszczek, 2006) is well adapted to evolutionary computation and thus makes the controller computation time quite reasonable,
- Because all requirements are specified in the tool using any *Matlab* instructions, all features of *Matlab* can be used. For instance nothing prevents the user from coupling the tool with *Simulink* in order to evaluate requirements with servo-loops simulated directly in a non-linear framework.

We emphasize that for requirements already predefined in *Systune*, using *Systune* is preferable because much faster (although *HinfStoch\_ControllerTuning* can yield to comparable results but in a longer time). In all other cases, using the tool introduced in this paper is interesting.

The paper is organized as follows. In section II, we briefly recall some theorical elements about the computation of fixed-structure controllers with evolutionary techniques. Then *HinfStoch\_ControllerTuning* is introduced in section III, and examples of uses, showing the flexibility and the capability of the tool, are described in section IV.

## 2. THEORICAL BACKGROUND

## *2.1 Optimizing controllers against multiple requirements*

Given a plant *P*(*s*) depicted in Fig. 2 on which  $e \in \mathbb{R}^{n_e}$  is the external input vector including disturbances, sensor noise, references,  $z \in \mathbb{R}^{n_z}$  are the controlled outputs,  $u \in \mathbb{R}^{n_u}$  is the control input vector and  $y \in \mathbb{R}^{n_y}$  are the measured variables. The  $H_{\infty}$  standard control problem consists at first in designing some weighting functions  $W_o(s)$  and  $W_i(s)$  to shape some closed-loop transfers to satisfy robustness and/or performance specifications ; then a stabilizing controller can be computed which minimizes  $\|W_a(s)F_i(P,K)W_i(s)\| < \gamma$ .



Fig. 2. Generalized control form with weights.

The main difficulty in this design relies obviously on the choice of well-suited pre- and post-compensators to handle the high-level specification requirements with good stability margins. Thus, in the full-order case, the tuning of weighing functions is a time consuming task which consists in solving the following problem:

$$
\min_{\substack{W_0(s), W_i(s) \\ \text{subject to } Z_1 < \overline{Z}_1, \dots, Z_m < \overline{Z}_m} \tag{1}
$$

where each  $Z_i$  is a high-level requirement.

The H∞ loop-shaping approach (McFarlane *et al*., 1992) is a particular case of the previous  $H_{\infty}$  control problem where weighting functions used to shape an open-loop target, are externalized as in (2)  $(H(s)$  is the system to be controlled).

$$
\left\| \begin{pmatrix} W_o(s) \\ W_i(s)^{-1} K(s) \end{pmatrix} S(s) \left( W_o(s)^{-1} H(s) W_i(s) \right) \right\|_{\infty} < \gamma_{.}(2)
$$
  

$$
S(s) = (I + H(s) K(s))^{-1}
$$

An important property of the  $H_{\infty}$  loop-shaping approach is the direct link between  $\gamma$  and the generalized gain and phase margins (respectively noted ∆*G* and ∆Φ) (Vinnicombe, 2000). Indeed:

$$
\Delta G \ge \frac{1+\gamma^{-1}}{1-\gamma^{-1}}, \ \Delta \Phi \ge 2a\sin\left(\gamma^{-1}\right). \tag{3}
$$

Thus  $\gamma = 3$  ensures that  $\Delta G \ge 6$  dB and  $\Delta \Phi \ge 40^\circ$ . Note that  $\gamma$ > 1 in this approach. Furthermore good values for ∆*G* and ∆Φ don't imply a small γ value.

A drawback of the  $H_{\infty}$  loop-shaping approach is the high order of computed controllers. Thus the question of simultaneously tuning the frequency weights and the final controller appears as a natural extension of the problem (1), that is:

$$
\min_{\substack{W_0(s), W_i(s), K(s) \\ \text{subject to}}} \gamma
$$
 (4)

*K*(*s*) *stabilizin g and*  $Z_1 < Z_1, ..., Z_m < Z_m$ 

In fact, optimizing the weights may be redundant with the optimization of the fixed-order final controller because at the end of the optimization process, the controller contains all the dynamical information needed to satisfy the specifications. However, the obtained value for  $\gamma$  is already considered as a robustness indicator relative to the weights with the relations (3) in the  $H_{\infty}$  loop-shaping framework.

Thus, without loss of generality, we can simplify the problem (2) by using directly static weights *Di* and *Do* (like "scalings") in the place of the frequency weights  $W_i(s)$  and  $W_o(s)$ , which leads to the scaled stabilization problem (5).

$$
\left\| \begin{pmatrix} D_o \\ D_i^{-1} K(s) \end{pmatrix} S(s) \left( D_o^{-1} H(s) D_i \right) \right\|_{\infty} < \gamma.
$$
 (5)

 $S(s) = (I + H(s)K(s))^{-1}$ 

The optimization problem (4) simplified to (6).

$$
\min_{D_0, D_i, K(s)} \gamma
$$
  
subject to (6)

*K*(*s*) *stabilizin g and*  $Z_1 < Z_1, ..., Z_m < Z_m$ Note that relations (3) remain satisfied.

A robust controller  $K(s)$  aims to satisfy some complex specifications, which can be expressed by constraints such as

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