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# A $V_2O_5/4H$ -SiC Schottky diode-based PTAT sensor operating in a wide range of bias currents



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#### ABSTRACT

A proportional to absolute temperature sensor (PTAT) based on V<sub>2</sub>O<sub>5</sub>/4H-SiC (vanadium pentoxide/4H polytype of silicon carbide) Schottky diodes is presented. The linear dependence on temperature of the voltage difference appearing at the terminals of two constant-current forward-biased diodes has been used for thermal sensing in the wide temperature range from T= 147 K to 400 K which extends down the state-of-the art of more than 80 K. The proposed sensor shows a sensitivity of 307  $\mu$ V/K, a good reproducibility and a stable linear output also in case of deviation of the two bias currents from the best operating condition.

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#### 1. Introduction

In the last few years 4H-SiC (4H polytype of silicon carbide) diodes have been widely explored for high-temperature thermal sensing [1–5]. The main advantage of these devices is the high linearity of the voltage-temperature characteristic and the long-term stability.

In a previous work, we presented a proportional to absolute temperature (PTAT) sensor consisting of two Schottky diodes with Ti/Al metal contacts [6]. The maximum sensitivity was achieved by biasing the diodes at well precise currents in their linear (resistive) region. However, in this bias range the non-linear contribution of the series resistance,  $R_s$ , can affects the diode sensor performances and, to minimize its impact, the diodes have to be biased in the exponential region of the *I-V* characteristics where  $R_s$  can be considered negligible [7–9].

To date, many works reported in literature on temperature sensors are based on SiC Schottky diodes with Ni [2–4] or Ti/Al contacts [6,7].

Although different materials have been used to fabricate 4H-SiCbased Schottky diodes [10–12], a thin layer of vanadium pentoxide

https://doi.org/10.1016/j.sna.2017.11.026 0924-4247/© 2017 Elsevier B.V. All rights reserved.  $(V_2O_5)$ , 5 nm-thick, was recently proposed as an alternative contact [13,14].

In particular, as reported in [13], the rectifying behavior of  $AI/V_2O_5/4H$ -SiC stack is due to the presence of a Schottky potential barrier at the  $V_2O_5/4H$ -SiC interface induced by the difference between the  $V_2O_5$  work function (in the range between 4.7 and 5.3 eV [15,16]) and the 4H-SiC electron affinity. Such evidences are supported by experimental measurements of *I*-*V*/*C*-*V* characteristics under light excitations at different temperatures and justified by physical-based analytical models [14]. Moreover, the ideality factor of *I*-*V* curves results close to one and, in [13], it has been ascribed to a low density of inhomogeneities at the Schottky contact [17]. Indeed, the interface quality among the materials can induce a spatial variation of the value of potential barrier height along the whole contact and, moreover, a variation of the ideality factor value from the unity.

From a technological point of view, the main advantage is the limited thermal budget involved in the  $V_2O_5$  annealing process, which is about 150 K lower than that typically used for conventional 4H-SiC metals, e.g. Ni [18]. This allows to fabricate Schottky-diode sensors at the end of an integrated circuit realization process flow. However,  $Al/V_2O_5/4H$ -SiC Schottky diodes cannot operate at temperatures higher than 425 K [13] due to a lower Schottky Barrier (SB) Height with respect to Ni or Ti 4H-SiC SB devices.

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Fig. 1. Electrical circuit of the PTAT sensor. Drawing not to scale.

In this letter, the performance of a PTAT sensor based on integrated V<sub>2</sub>O<sub>5</sub>/4H-SiC Schottky diodes is investigated. In particular, sensitivity, linearity, root mean square error (*rmse*) and repeatability are accurately analyzed in a wide range of temperatures ( $147 \le T \le 400$  K) and currents.

If compared to Si technologies [19–22], the performance of SiC-based Schottky diodes exceed that of Si-based counterparts in particular for applications requiring high-temperature and high-power. In this work, the realized sensor extends-down the operating temperature range ( $\Delta T = 253$  K), with a high sensitivity (*S* = 307  $\mu$ V/K), therefore it is particularly suitable for applications at very low temperatures, i.e., full military, automotive, extended industrial and avionic applications.

#### 2. Device structure and experimental set-up

The fabricated Schottky diodes consist of a 5  $\mu$ m–thick (8.8  $\pm$  2.2)  $\times$  10<sup>15</sup> cm<sup>-3</sup> n-doped epilayer, grown on a (0001) 4° off-axis Si-face, 350  $\mu$ m-thick and  $\rho$ ~21 m $\Omega$   $\times$  cm n<sup>+</sup> 4H-SiC substrate, as schematically shown in Fig. 1. The technological process steps are well reported in Ref. [13]. A shadow mask was explored to form circular V<sub>2</sub>O<sub>5</sub>/Al dots of 500  $\mu$ m in diameter, the distance between the two devices is 1 mm, which allows to neglect crosstalk effects among them. Indeed, considering that the lateral contribution of the current is due to the majority carriers diffusion, the electron diffusion length is less than 6  $\mu$ m for our devices [14] and, therefore, a minimum distance of about 120  $\mu$ m is enough to avoid the mutual effects on the electrostatic potentials among devices.

In our setup, two Schottky diodes,  $D_1$  and  $D_2$ , with almost identical  $I_D$ - $V_D$ -T characteristics (maximum  $rmse = 1.01 \times 10^{-5}$  calculated over the full bias range from 1 µA to 1 mA) and same ideality factor ( $\eta_1(I_D,T) \sim \eta_2(I_D,T) = \eta$ ), were driven by two external and independent current sources, providing constant  $I_{D1}$  and  $I_{D2}$  currents (Fig. 1).

The difference between the voltage drops across the two diodes  $(\Delta V_D)$  is given by the following equation [6]:

$$\Delta V_D = V_{D2} - V_{D1} = \frac{kT}{q} \eta \ln(r) + R_S(I_{D2} - I_{D1})$$
(1)

where  $V_{D1,2}$  are the diode voltage drops for  $D_1$  and  $D_2$ , respectively,  $R_s$  is the series resistance, q the electron charge, T the absolute temperature, k the Boltzmann constant and  $r = I_{D2}/I_{D1}$  is the bias currents ratio.

The 4H-SiC/V<sub>2</sub>O<sub>5</sub> Schottky diodes are biased in the exponential region of their *I*-V characteristics to reduce the contribution



**Fig. 2.** Measured (points)  $V_D$ -*T* for  $I_{D1}$  = 16  $\mu$ A and different current ratios *r* (2.75, 15.75, 28.25, 38, 53.25, 62.5). The dashed lines are the best linear fits,  $f_L(T)$ , of the experimental data. The inset shows the *I*-*V*-*T* characteristics in semi-log scale, in the temperature range 147–400 K.

of  $R_{S}$ ·( $I_{D2}$ - $I_{D1}$ ) and, therefore, to increase the sensor linearity in a widest range of bias currents [6]. In such way,  $\Delta V_D$  is linearly proportional to T for a fixed r and assuming  $\eta$  almost constant. This last assumption will be validated below.

Experimental measurements were performed through a Janis Research Inc. cryo–system [23]. Measurements were conducted in vacuum at a pressure lower than  $5 \times 10^{-6}$  mbar and a Lake Shore Cryotonics Inc. 335 temperature controller was used to automatically control the temperature from 147 to 400 K and vice-versa. A reference sensor (Lake Shore Cryotonics Inc. DT-670B-SD silicondiode [24]), with an accuracy of  $\pm 0.032$  K up to 305 K and  $\pm 0.33\%$  T (i.e.  $\pm 1.4$  K at T=440 K) for higher temperatures, was placed in thermal contact with the 4H-SiC microchip in order to monitor the true chip temperature. Another sensor (DT-670B-CU-HT), placed on the sample stage, was used to control the thermal stability of the overall equipment. Each measurement was taken several minutes after the temperature was set in order to be sure about the system thermal stability.

The external current sources used to bias the 4H-SiC Schottky diodes were provided by an Agilent HP4155B Semiconductor Parameter Analyzer. For the considered current range  $(1 \ \mu A < I_D < 1 \ mA)$  the instrument provides a resolution of 10 nA and an accuracy of  $\pm 12$  nA [25].

#### 3. Results

In the inset of Fig. 2,  $I_D$ - $V_D$  characteristics are reported for the temperature range 147–400 K. By using the extraction procedure of [7], in the evaluated temperature range,  $\eta$  remains almost constant with a mean value of around 1.05 and a standard deviation lower than 0.02. As previously mentioned, this result confirms the highly linearity of the output characteristic of the  $\Delta V_D$ -T sensor.

The best linear fittings,  $f_L(T)$ , of the  $\Delta V_D$  vs. *T* experimental points obtained in three cycles of measurements in a range from (down to) T = 147 K up to (from) 400 K are reported in Fig. 2. In particular,  $D_1$  was biased with  $I_{D1} = 16 \mu$ A, where the 4H-SiC diode, previously characterized as single-diode temperature sensor, showed its best behavior, whilst  $I_{D2}$  was varied from 44  $\mu$ A to 1 mA. The plot of Fig. 2 shows that  $\Delta V_D$  and *T* are linearly dependent each other in the considered wide temperature range ( $\Delta T = 253$  K). To mathematically evaluate the sensor linearity, we calculated the coefficient of determination ( $R^2$ ) that allows to quantify how much the experimental points deviate from the best-linear regression [26]. The corresponding sensitivities were calculated from the slope of the

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