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# Preferential oxidation of CO in excess H<sub>2</sub> over CeO<sub>2</sub>/CuO catalyst: Effect of calcination temperature

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#### Abstract

Different from the classical configuration CuO/CeO<sub>2</sub> catalyst, the inverse configuration CeO<sub>2</sub>/CuO catalyst (atomic ratio of Ce/Cu = 10/100) was prepared by impregnation method. Five calcination temperatures were selected to investigate the interaction between CeO<sub>2</sub> and CuO support. It is found that as calcination temperature increased from 500 to 900 °C, sintering of CeO<sub>2</sub> particles on the support occurred together with the diffusion of a portion of Ce<sup>4+</sup> ions into CuO crystals, forming solid solution. Formation of interface complex Ce–O–Cu was suggested by TPR measurements. The catalyst calcined at 700 °C gives the highest activity for preferential oxidation of CO in excess H<sub>2</sub> stream.

#### Key words

preferential oxidation; carbon monoxide; cerium oxide; cupric oxide; TPR

## 1. Introduction

Proton exchange membrane fuel cell (PEMFC) generally requires a H<sub>2</sub>-rich stream with CO content less than 10 ppm. The gas mixture obtained by steam reforming of natural gas (mainly methane) and the following water-gas shift reaction (WGS) still contains ca. 0.5%–2% CO besides ca. 18% CO<sub>2</sub>. For small scale PEMFC stacks, e.g., the one in house use, the unit to remove CO from the reforming-WGS gas mixture should be small as possible as can in volume. Selective methanation of CO is a way to remove CO from the gas mixture, while methanation of a part of CO<sub>2</sub> is also accompanied. Thus a relatively large amount of hydrogen is consumed, which decreases electric power output of PEMFC. In contrast, preferential oxidation of CO in excess H<sub>2</sub> (CO-PROX) is a more suitable way to remove CO from the gas mixture. CuO/CeO2 composite has been proved to be a promising catalyst for CO-PROX due to its good activity and low cost relative to noble metal supported catalysts [1]. Several methods such as coprecipitation, citrate, urea-nitrate combustion and impregnation methods were reported to prepare CuO/CeO<sub>2</sub> catalyst in literatures [2-6]. It seems that the urea-nitrate combustion method is better than the citrate method [2,4]. In comparison of co-precipitation method with impregnation method, Gamarra et al. [3] reported that the one prepared by impregnation method with atomic ratio of Cu/Ce = 0.022 is better. On the other hand, calcination temperature of the catalyst has a great influence on the catalytic activity for CO oxidation [7-9]. Jung et al. [7] reported that the calcination at 700 °C is optimal for CuO/CeO<sub>2</sub> catalyst prepared by co-precipitation method at Cu content of 5.1 wt%. On the mechanism of CO-PROX, it is proposed that the catalytically active center for CO oxidation is Cu–O–Ce structure on the interface of CuO and CeO<sub>2</sub> phases as shown in Equation (1) [10–12]. The symbol "□" represents oxygen vacancy.

$$Cu^{2+} - O^{2-} - Ce^{4+} + CO = Cu^{+} - \Box - Ce^{3+} + CO_2$$
(1)

Martínez-Arias et al. [13] detected superoxide ion  $O_2^$ by EPR technique on the partially reduced CuO/CeO<sub>2</sub> sample prepared by the method of incipient wetness impregnation of CeO<sub>2</sub> support using an aqueous solution of Cu(NO<sub>3</sub>)<sub>2</sub>. Temperature-programmed reduction (TPR) in H<sub>2</sub>-N<sub>2</sub> mixture gas suggests several different states of CuO<sub>x</sub> dispersed on CeO<sub>2</sub> support, i.e., highly dispersed CuO<sub>x</sub> with strong interacting with the support, well dispersed CuO<sub>x</sub> clusters, and CuO crystallites [8,9,14,15]. Formation of solid solution Cu– Ce–O is also confirmed [3,7,16]. Shan et al. [16] reported a solid solution Cu<sub>x</sub>Ce<sub>1-x</sub>O<sub>y</sub> ( $x \le 0.1$ ) formed after calcination at 650 °C. And they found at a larger x value, the segregated

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CuO phase became present [16]. CuO crystallites on CeO<sub>2</sub> support can be recognized by XRD. Moreover, due to the interaction between CuO<sub>x</sub> and CeO<sub>2</sub>, an extent of reduction of CeO<sub>2</sub> in CuO/CeO<sub>2</sub> catalyst would occur concurrently with CuO<sub>x</sub> species at the reduction temperature of CuO<sub>x</sub>, even though pure CeO<sub>2</sub> itself began to be reduced only at a much higher temperature [14,15].

The inverse configuration CeO<sub>2</sub>/CuO catalyst was firstly designed by Hornes et al. as an alternative to the classical configuration CuO/CeO<sub>2</sub> for preferential oxidation of CO in excess H<sub>2</sub> stream [17]. The inverse system, synthesized by microemulsion method, showed a better activity for CO-PROX than Cu<sub>0.2</sub>Ce<sub>0.8</sub>O<sub>2</sub> reference catalyst [17]. The idea of the authors was that, using large size of CuO particles as support to decease the reducibility of the catalytically active centers, and therefore to obtain a wider temperature window with high CO conversion and high selectivity to CO<sub>2</sub> of O<sub>2</sub> for CO-PROX. Another merit of the inverse system is the decreased usage of rare earth metal oxide CeO<sub>2</sub>.

We followed the inverse design of the work [17], and prepared CeO<sub>2</sub>/CuO catalyst (atomic ratio of Ce/Cu = 10/100) by impregnating a commercial CuO powder with Ce(NO<sub>3</sub>)<sub>3</sub> solution. Five calcination temperatures, i.e., 500, 600, 700, 800 and 900 °C, were selected to investigate the interaction between cerium oxide component and CuO support.

# 2. Experimental

#### 2.1. Catalyst preparation

5 g commercial CuO powder (Beijing Chemicals, China) was used as support. 5 mL water-ethanol mixture (2 mL distilled water plus 3 mL ethanol (95%)) was taken to dissolve an appropriate amount of cerium nitrate (Tianjin Fuchen Chemicals, China). After CuO powder was added into the cerium nitrate solution, the solid-liquid mixture was stirred into slurry with glass rod and agitated supersonically at 60 °C for 15 min with continuous stirring by hand, in order to evaporate the excess liquid. Then, the resulting solid was dried in oven at 120 °C for 4 h. At last the solid was calcined in a muffle furnace at a given temperature for 2 h. Five calcination temperatures, i.e., 500, 600, 700, 800 and 900  $^\circ C,$  were selected to investigate the effect of calcination temperature. CeO2/CuO catalysts obtained at the five calcination temperatures all had the same atomic ratio of Ce/Cu equal to 10/100, so they were denoted as 10 at.% CeO<sub>2</sub>/CuO in the text of this paper.

# 2.2. Catalyst characterization

Phase identification of the five CeO<sub>2</sub>/CuO catalysts was carried out on an X-ray diffractometer (Shimadzu XRD-6000, Japan) with Cu  $K_{\alpha}$  radiation at the fixed measurement parameters. Temperature-programmed reduction (TPR) experiments were performed on the apparatus (PX2000, Pengxiang Co., Tianjin, China), where a 20%H<sub>2</sub>-N<sub>2</sub> mixture gas was flowing at 20 mL/min over the sample (20 mg) during the heating process at 10 °C/min from room temperature to 900 °C. Specific surface area (SSA) and pore volume were measured by BET method at liquid nitrogen temperature (Belsorp-Max, Japan).

Catalytic activity of CeO<sub>2</sub>/CuO catalysts for CO-PROX was tested in a fixed-bed flow reactor under atmospheric pressure. 200 mg catalyst (60–80 mesh) was loaded into a U-type quartz tube reactor (6 mm i.d.). The CO-containing gas was composed of 2 vol% CO, 75 vol% H<sub>2</sub> and 23 vol% N<sub>2</sub>, flowing at 100 mL/min controlled by a mass flow controller (MFC). Air was co-fed by another MFC, set at 15 mL/min. Reaction products' analyses were performed on a gas chromatograph with a thermal conductivity detector (TCD). In the oven of the gas chromatograph, a packed column (Shincarbon ST 50/80, Shimadzu Column Packing, Japan) was connected to separate H<sub>2</sub>, O<sub>2</sub>, N<sub>2</sub>, CO and CO<sub>2</sub> in the reaction products.

# 3. Results and discussion

#### 3.1. XRD phase identification

XRD patterns of the five CeO2/CuO catalysts obtained at different calcination temperatures are shown in Figure 1. It is seen that the diffraction of CeO<sub>2</sub> phase has a growing intensity with calcination temperature increasing. This can be ascribed to a continuous sintering of CeO<sub>2</sub> phase dispersed on CuO support. Besides, it can also be envisaged that a portion of Ce<sup>4+</sup> ions were capable of diffusing into CuO crystals forming solid solution at high calcination temperatures. The intensities of the two most intense XRD peaks (plane (-111)) at  $2\theta = ca. 35.56^{\circ}$ , plane (111) at  $2\theta = ca. 38.72^{\circ}$ ) of CuO phase in CeO<sub>2</sub>/CuO catalysts are shown in Figure 2. It is clear that the peak intensity increased at first and then decreased on plane (111) as the calcination temperature rose from 500 to 900 °C. Whereas, the pure CuO samples had an increasing trend in intensity with calcination temperature rising, if considering the baseline count fluctuation of XRD equipment, for the same XRD peak as shown in Figure 3.



Figure 1. XRD patterns of  $CeO_2/CuO$  catalysts calcined at different temperatures. The black full circles denote  $CeO_2$  phase. Other peaks belong to CuO phase

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