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First-principle modeling and characterization of thermal modulation in comprehensive two-dimensional gas chromatography using a microfabricated device

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ABSTRACT

Thermal modulation of analyte effluents at a junction between serially connected complementary columns is a critical process in comprehensive two-dimensional gas chromatography (GC × GC). However, little effort has been made to theoretically study this process with a full understanding of key phenomena. We developed a theoretical model of single-stage thermal modulation processes based on fundamental physics of gas chromatography (GC) with the aim to elucidate factors leading to improvements in GC × GC analyses. Model predictions were compared with experimental data obtained using our microfabricated thermal modulator (μ TM) operating as a single-stage thermal modulator. Built upon one-dimensional (¹D) GC theory, our model predicted the temporal and spatial distribution of analyte concentration within a thermal modulator (TM) channel during periodically repeating modulation cycles, each consisting of a cooling and heating period and yielding sharp peaks from a broad first dimension peak. Our model incorporated the effect of the location of the incoming ¹D Gaussian peak to the μ TM, with respect to the onset of the cooling period and the influence of cold interconnects on the thermal modulation and the influence of cold interconnects on the thermal modulation and the influence of cold interconnects on the thermal modulation process. Excellent match between experiment and simulation was obtained. Finally we proposed a few design modifications which could drastically improve performance of our μ TM.

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1. Introduction

Resolving analytes in highly complex mixtures poses a significant challenge for analytical chemists. Peaks of such complex mixtures tend to overlap each other, a phenomenon known as coelution. Securing large peak capacity commonly entails increasing the column length, decreasing the column diameter, or a combination of both [1–7]. The use of a column with such a great excess of peak capacity can ease some of the problems but the costs are high in terms of analysis time, detection limits and instrument requirements. In contrast, two-dimensional gas chromatography (GC × GC) is a promising alternative approach that enables complex mixtures to be resolved with higher separation capacity and selectivity than the conventional approach described above. Furthermore, the GC × GC technique potentially permits

http://dx.doi.org/10.1016/j.snb.2016.02.132 0925-4005/© 2016 Elsevier B.V. All rights reserved. development of a miniaturized GC lab-on-a-chip system incorporating a microfabricated thermal modulator (μ TM) for real-time field deployment under limited resources without the separation performance compromised by reduced column lengths [8–12].

In $GC \times GC$, two columns with different separation mechanisms, namely the first dimension (¹D) column and the second (²D) dimension column, are used to separate the gas species (Fig. 1). The additional dimension enhances the peak capacity of the system, as a result of which a much higher number of compounds can be separated and analyzed. Various different column combinations have been tried since the 1990s [13], such as a combination of non-polar coating in the ¹D column and a polar coating in the ²D column [14,15]; a polar coating in the ¹D column and non-polar coating in the ²D column, [16–19] and various degrees of polarity in the ¹D column and ²D column [20]. A combination of a non-polar ¹D column and a polar²D column is one of the most popular combinations used. The use of a non-polar column permits virtually direct transfer of methods that have already been developed in the context of conventional GC. Analytes in the same homologous group are separated in the ¹D on the basis of their different volatilities. In the ²D, separation happens due to both boiling point and polarity. How-

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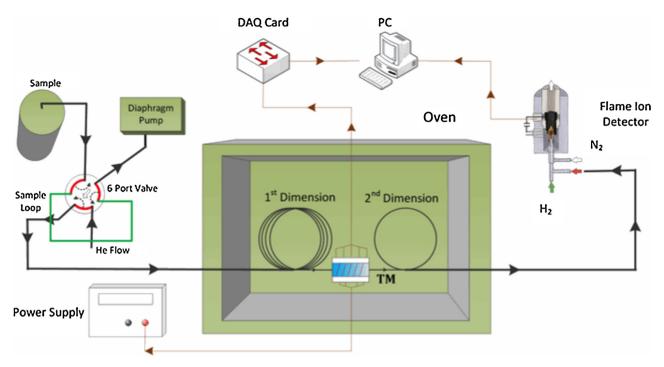


Fig. 1. Schematic of a typical GC × GC system incorporating thermal modulator (TM) and two columns with their internal surfaces coated with complementary stationary phases for analyte separation. Additional components of the system include a sample injection unit, a temperature-controlled oven, a gas sensor (flame ionization detector), a computer system for programmable TM operation and data acquisition, and a power supply.

ever, any boiling point contribution to the ²D retention time can be neutralized by temperature ramping on the ²D; as a result, separation is primarily governed by specific polarity-based interactions [14]. That is, the two chromatographic processes are complementary to each other, and the separation is orthogonal. More recently, it has been found that a polar/medium polar ¹D and a polar ²D column can provide valuable results especially when highly polar and semi-polar analytes such, as alcohols, aldehydes, ketones, esters and acids, are among the key components of the mixture [20,21].

An intermediate modulator device placed at the junction between the ¹D and ²D plays a key role in realizing $GC \times GC$ analyses (Fig. 2A) [22,23]. While different types of modulators exist, thermal modulators (TMs) have become widely used due to their ability to provide comprehensive modulation resulting in increased analyte detectability relative to other modulator types [24-30]. The injected mixture is partially separated in the ¹D, and arrives at the interface between the ¹D and the μ TM (Fig. 2B). This device cuts and re-concentrates the effluent peak from a long ¹D column, at a time interval known as the modulation period (P_M) and re-injects them onto a short ²D column as sharp sub-bands [31]. This prevents recombination of the species that have been partially separated in the ¹D after their re-injection to the ²D. Further, focusing the sections of the ¹D effluent and re-injecting them into the ²D greatly increases the peak height, whereby enhancing the detection limit relative to the noise threshold of the detector (Fig. 2C). Mapping the obtained signal peaks with respect to both the ¹D retention time and the ²D retention time results in the two-dimensional (2D) gas chromatogram and allows for high-resolution analysis of complex gas compound mixtures at large capacity (Fig. 2D). Based on this transformation, a ²D contour plot is obtained and is subsequently used to identify any compounds present in the original mixture (Fig. 2E). However, Blumberg, Blumberg et al. [32,33] show that while the theoretical peak capacity of $GC \times GC$ is much higher than that of the conventional GC, current experimental studies show GC × GC only achieves moderately improved separation capability. Only under highly optimized conditions leading to modulated

peaks at a FWHH of <20 ms, can the theoretical maximum peak capacity be obtained. Further, if the FWHH of the modulated peaks approaches 100 ms, the effective gain becomes 1. While $GC \times GC$ still yields a few secondary benefits with broader modulated peaks, such as group-type identification/structured chromatograms [34], higher sensitivity, and large peak amplitudes [35], the primary benefit of GC × GC over conventional GC in terms of peak capacity becomes less obvious [36]. Hence, the modulator device is the key bottleneck in reaching the desired separation performance of $GC \times GC$. To reach the maximum possible potential of $GC \times GC$ operated by thermal modulation, a TM needs to inject very sharp effluent bands with full-width at half height (FWHH) as narrow as 10 ms into the ²D with a short channel length of 1-2 cm at a flame ionization detector (FID) data acquisition rate of $\sim 1 \text{ kHz}$ [32,33,36]. Hence, there is significant room for improving the peak capacity obtainable using $GC \times GC$ by optimizing the performance of the modulator to realize the ideal $GC \times GC$ operation above. Since, the FWHH of the modulated peak is the critical parameter determining the effective peak capacity of the $GC \times GC$ system, we use that as the performance metric of the system in our study.

To our best knowledge, no rigorous theoretical model exists that provides a good design guideline for TMs. This prevents researchers from achieving optimal performances for TMs based on a thorough understanding of physics governing the thermal modulation process. Hence, they usually resort to the expensive route of reducing the minimum trapping temperature, with the aim to achieve small FWHH of injection. This paper presents a theoretical basis to predict the behavior of a microfabricated TM device (µTM) developed in our previous study [8,9]. The goal of this paper is to understand the physics governing the operation of the device, so as to develop better and more efficient µTMs in the future. While our original µTM is a two-stage device as described later in Section 2.2, we have operated it as a single-stage device, where the both stages are synchronously operated with no time lag between the heat pulses applied to the stages, and developed a model for the microscale thermal modulation process based on the first principles

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