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Fault-Tolerant Control for Discrete Linear Systems with Consideration of Actuator Systems with Consideration of Actuator
Saturation and Performance Degradation \star ault-Tolerant Control for Discrete Linea Fault-Tolerant Control for Discrete Linear

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systems with actuator faults. The main contribution of this paper lies in the capability of dealing with the actuator saturation and accepting the performance degradation. In this paper, a fault estimation observer is first designed by constructing an equivalent descriptor system model of the original plant. To accept performance degradation of the post-fault system, a degradation factor is introduced into the reference model. In the fault-tolerant control design, both the actuator saturation and performance degradation are considered, and the fault-tolerant control input and the degradation factor are simultaneously designed by solving a constrained optimization problem. Finally, an aircraft example is simulated to demonstrate the effectiveness and performance of the proposed method. optimization problem. Finally, an aircraft example is simulated to demonstrate the effectiveness optimization problem. Finally, an aircraft example is simulated to demonstrate the effectiveness Abstract: This paper proposes an active fault-tolerant control method for discrete-time linear a fault estimation observer is first designed by constructing an equivalent descriptor system
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1. INTRODUCTION 1. INTRODUCTION 1. INTRODUCTION 1. INTRODUCTION 1. INTRODUCTION

In the past decades, fault diagnosis and fault-tolerant control techniques have been widely investigated due to their capabilities in improving safety and availability of as system. Fruitful results have been proposed in the literature, see e.g. Chen and Patton (1999), Blanke et al. (2006), $\frac{1}{999}$, $\frac{1}{100}$ al. (2006), Noura et al. (2009), Rodrigues et al. (2014), R odrigues et al. (2007), Ye and Yang (2006) and the references therein. references therein. references therein. In the past decades, fault diagnosis and fault-tolerant

In Lunze et al. (2003) and Steffen (2005) , a new methodology called fault hiding approach has been proposed to achieve fault-tolerance. The fault hiding goal is to make the reconfigured system exhibit similar behaviour to that of the nominal plant. In this paradigm, the nominal controller is kept in the loop and a reconfiguration block is inserted between faulty plant and nominal controller to inserted between faulty plant and nominal controller to
generate useful control signals so as to hide the impact of faults. As pointed out in Khosrowjerdi & Scheila Barzegary (2014), this approach provides a way for minimallyinvasive alternations of the loop, which is the main advantage of the fault hiding approach. In recent years, the fault hiding methodology has been applied to piecewise affine, tage of the fault hiding approach. In recent years, the fault
hiding methodology has been applied to piecewise affine,
linear parameter-varying, and Lipschitz nonlinear systems, In Lunze et al. (2003) and Steffen (2005) , a new method-

see in Steffen (2005), Richter (2011), Rotondo et al. (2014), Tabatabaeipour et al. (2015) and Khosrowjerdi & Soheila Barzegary (2014). In spite of wide investigation, there are still some problems to be addressed in the fault-tolerant control design based on fault hiding approach. First, many existing results do not consider the fault diagnosis problem but assume that fault has already been accurately estimated, which is obviously an impractical assumption. Second, in most of the existing fault hiding approaches, the actuator saturation is not considered. This may lead to severe problem when these approaches are applied to lem but assume that fault has already been accurately
estimated, which is obviously an impractical assumption.
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the actuator saturation is not considered. This may le voted to the performance degradation in the fault-tolerant voted to the performance degradation in the fault-tolerant
design. In practice, however, the control margin of a faulty system will degrade due to the presence of faults and actuator saturation. Therefore, the fault-tolerant control scheme should be able to accept performance degradation in order to keep the operation safety. To the best of our knowledge, only few papers (Zhang & Jiang (2003); Jiang & Zhang (2006); Theilliol et al. (2008); Qi et al. (2014)) investigated the performance degradation in fault-tolerant control design. control design. control design. see in Steffen (2005), Richter (2011), Rotondo et al. (2014), **besties and conserved transies of conserved the conserved to estimate the conserved to est**

Considering the aforementioned problems, this paper proposes a fault-tolerant control method with consideration of the actuator saturation and performance degradation. The main contribution of this paper lies the following aspects. First, an augmented state observer by constructing a descriptor system representation is proposed to estimate a descriptor system representation is proposed to estimate a descriptor system representation is proposed to estimate Considering the aforementioned problems, this paper pro-

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mental Research Funds for the Central Universities (Grant No. HIT.NSRIF.2015034). HIT.NSRIF.2015034). HIT.NSRIF.2015034). mental Research Funds for the Central Universities (Grant No.

the fault. Second, the actuator saturation is considered in the proposed fault-tolerant control. Moreover, a novel degradation factor is introduced in the fault-tolerant control design so that the proposed fault-tolerant controller has the capability of accepting performance degradation.

2. PROBLEM FORMULATION

Consider the following discrete-time linear system

$$
\begin{cases}\nx(k+1) = Ax(k) + Bu(k) \\
y(k) = Cx(k)\n\end{cases} \tag{1}
$$

where $x(k) \in \mathbb{R}^n$ is the state, $u(k) \in \mathbb{R}^p$ is the control input, and $y(k) \in \mathbb{R}^m$ is the output. $A \in \mathbb{R}^{n \times n}$, $B \in \mathbb{R}^{n \times p}$, and $C \in \mathbb{R}^{m \times n}$ are known constant matrices.

In this paper, only actuator faults are considered. The actuator faults are modeled as a multiplicative representation, i.e. the actuator faults change the input matrix B to B_f , which is given as

$$
B_f = B\Lambda \tag{2}
$$

Herein, $\Lambda \in \mathbb{R}^{p \times p}$ is a diagonal matrix which implies the impact of the actuator faults, i.e.

$$
\Lambda = \begin{bmatrix} \lambda_1 & \cdots & 0 \\ \vdots & \ddots & \vdots \\ 0 & \cdots & \lambda_p \end{bmatrix}
$$
 (3)

In fact, γ_i represents the effectiveness factors of the *i*th actuator. $\gamma_i = 0$ means that the *i*th actuator is presented to be total failure, such as a stuck fault; $0 < \gamma_i < 1$ denotes the fault of the ith actuator may be a partial loss of control effectiveness; and $\gamma_i = 1$ implies the *i*th actuator is faultfree. For the convenience of fault estimation, the scalars $\lambda_i, i = 1, 2, \ldots, p$ are assumed to be constant or slowvarying.

Considering the actuator faults, the model of the faulty plant is given by

$$
\begin{cases}\nx(k+1) = Ax(k) + B_f u(k) \\
y(k) = Cx(k)\n\end{cases} \tag{4}
$$

Moreover, the actuator saturation is considered in this paper. That is, the control input $u(t)$ is subject to the following saturation constraint

$$
u(k) \in \mathcal{U} := \{ u \in \mathbb{R}^p | \underline{u}_i \le u_i \le \bar{u}_i \}
$$
 (5)

where u_i and \bar{u}_i denote the minimum and the maximum actions of the ith actuator, respectively.

The aim of this paper is to design a fault-tolerant scheme such that the reconfigured state of the faulty plant (4) exhibits similar output to that of the following nominal model

$$
\begin{cases}\nx_r(k+1) = Ax_r(k) + Bu_r(k) \\
y_r(k) = Cx_r(k)\n\end{cases} \tag{6}
$$

where $x_r(k) \in \mathbb{R}^n$, $u_r(k) \in \mathbb{R}^p$ and $y_r(k) \in \mathbb{R}^m$ are the state, the control input and the output of the nominal system, respectively. Without loss of generality, it is assumed that $u_r(k)$ is designed such that the nominal output $y_r(k)$ tracks a given reference $r(k)$, i.e. $y_r(k) \rightarrow r(k)$.

Due to the presence of the actuator faults and saturation, it is reasonable to allow the faulty plant (4) to have certain performance degradation compared to the nominal model (6).

3. FAULT ESTIMATION OBSERVER DESIGN

Recently, descriptor system approach has been used to deal with fault diagnosis (Gao and Wang (2006), Gao and Ding (2007)). However, these works focus on sensor fault diagnosis. On the other hand, the descriptor system approach has not fully investigated in the actuator fault diagnosis. In view of this, this paper proposes an actuator fault estimation observer based on the descriptor system approach.

First, the actuator faults is converted into an additive representation by letting

$$
f(k) = (I_p - \Lambda)u(k)
$$
 (7)

where $f(k) \in \mathbb{R}^n$ is an virtual equivalent fault, I_p is used to denote a $p \times p$ identity matrix.

By using (7), the model (4) becomes

$$
\begin{cases}\nx(k+1) = Ax(k) + Bu(k) - Bf(k) \\
= Ax(k) + B_f u(k)\n\end{cases}
$$
\n(8)

Let

$$
\bar{x}(k) = \begin{bmatrix} x(k) \\ f(k-1) \end{bmatrix}
$$
 (9)

the faulty system (8) is equivalent to

$$
\begin{cases} E\bar{x}(k+1) = \bar{A}\bar{x}(k) + \bar{B}u(k) \\ y(k) = \bar{C}\bar{x}(k) \end{cases}
$$
 (10)

where

$$
E = \begin{bmatrix} I_n & B \\ 0 & 0 \end{bmatrix}, \, \bar{A} = \begin{bmatrix} A & 0 \\ 0 & 0 \end{bmatrix}, \, \bar{B} = \begin{bmatrix} B \\ 0 \end{bmatrix}, \, \bar{C} = \begin{bmatrix} C & 0 \end{bmatrix} \tag{11}
$$

Using the relation in (7), the estimate of Λ can be easily obtained the additive fault term is estimated (this will be shown later). Moreover, according to the definition of $\bar{x}(k)$ in (9), the actuator fault $f(k-1)$ can be estimated if the estimation of the augmented state $\bar{x}(k)$ is obtained. Therefore, it can be concluded that fault estimation for system (4) is converted as an observer design problem for the descriptor system (10).

In the literature, there has been some results on observer design for discrete-time descriptor systems, see e.g. Dai (1988), Darouach et al. (2010), Wang et al. (2012). Among these results, Wang et al. (2012) proposes a new observer structure and presents a systemic design approach based on LMI technique. In this paper, the method in Wang et al. (2012) is used to address fault estimation problem. The proposed observer has the following form

$$
\begin{cases} \zeta(k+1) = T\bar{A}\hat{x}(k) + T\bar{B}u(k) + L\left[y(k) - \bar{C}\hat{x}(k)\right] \\ \hat{x}(k) = \zeta(k) + Ny(k) \end{cases}
$$
(12)

where $\hat{\bar{x}}(k) \in \mathbb{R}^{(n+p)}$ is the estimate of the augmented state $\bar{x}(k)$ and $L \in \mathbb{R}^{(n+p)\times m}$ the gain matrix to be synthesized. Moreover, the matrices $T \in \mathbb{R}^{(n+p) \times (n+p)}$ and $N \in \mathbb{R}^{(n+p)\times m}$ are designed such that

$$
TE + N\bar{C} = I_{n+p} \tag{13}
$$

Remark 1. A necessary condition to use the observer (12) is the matrices E and \overline{C} satisfy

$$
rank\left[\frac{E}{\bar{C}}\right] = n + p \tag{14}
$$

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