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## Digital fixed-frequency hysteresis current control of a BLDC motor applied for aerospace electrically powered actuators

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#### **KEYWORDS**

- 15 BLDC motor;
- 16 Current control;
- Fixed-frequency modulation; 17
- 18 Flexible bound size;
- 19 Hysteresis current control; 20 PWM:
- 21 Triangular carrier

Abstract In the conventional cascade control structure of aerospace electrically powered actuators, the current (or electromagnetic torque) loop plays a critical role in realizing a rapid response for a digitally controlled BrushLess Direct Current (BLDC) motor. Hysteresis Current Control (HCC) is an effective method in improving the performance of current control for a BLDC motor. Nevertheless, the varying modulating frequency in the traditional HCC causes severe problems on the safety of power devices and the electromagnetic compatibility design. A triangular carrier-based fixed-frequency HCC strategy is expanded by relaxing the constraints on the rising and descending rates of the winding current to advance the capability of HCC to realize fixed-frequency modulation in the steady state. Based on that, a new flexible-bound-size quasi-fixed-frequency HCC is proposed, and the range feasible to realize fixed-frequency modulation control can cover the entire running process in the steady state. Meanwhile, a corresponding digital control strategy is designed, and four digitalization rules are proposed to extend the capacity to achieve fixed-frequency modulation control to the unsteady working state, that is, a novel fixed-frequency modulation is realized. Simulation and experimental results prove the effectiveness of this improved fixed-frequency HCC strategy.

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Safer, cheaper, and greener technologies are important initia-

tives for the future of air transport. In response to these needs,

the aerospace industry is searching for an innovation (incre-

mental or disruptive) in safety-critical actuation systems.<sup>1</sup>

Recently, significant interest is given toward "more electric air-

#### 1. Introduction

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craft" even "all electric aircraft".<sup>2,3</sup> The trend is to increase the 29 usage of power-by-wire electrical actuators: electro-hydrostatic 30 actuators and electro-mechanical actuators.<sup>4</sup> These actuators 31 are projected to replace the conventional hydraulic servo actu-32 ators. From the power-to-weight ratio viewpoint, the high per-33 formance (significant efficiency and torque/power density)<sup>5</sup> 34 and maturity improvements of the robust design for perma-35 nent magnet BrushLess Direct Current (BLDC) motor and 36 their power drive electronics make electrically supplied actua-37 tors increasingly attractive.<sup>6,7</sup> However, alternative solutions 38 need to be studied for BLDC motor control to ensure the 39 40 required dynamic performance of an actuator under a wide 41 range of in-flight maneuvers. The current loop is an innermost control loop in the control of a motor drive electronics. 42 and its control strategy has a dramatic effect on the perfor-43 mance of a motor-driven device.<sup>8</sup> Thus, the study of a high-44 performance current control strategy has been an issue amid 45 46 studies of motor control.9

47 In practical applications, the triangular-carrier-based Pulse Width Modulation (PWM) is adopted as a common method in 48 current modulation, and a certain upper controller, such as a 49 PID controller, a sliding mode controller, a predictive con-50 troller, and so on, is used to control the current quantita-51 tively.<sup>10–13</sup> In these current control strategies, the dynamic 52 response of the current controller can be effectively improved 53 54 through increasing the frequencies of current sampling and 55 PWM carrier. However, because the current is not controlled directly and an updating delay of the PWM carrier duty cycle 56 57 exists, the actual winding current can easily exceed its upper limit confined by the power device capability due to an extre-58 mely high rising rate of current. Efforts have been done to 59 solve this problem. For instance, Zhang et al. proposed a 60 feed-forward control method combined with a dual current 61 sampling and dual PWM duty ratio update scheme in Ref. 62 14 to decrease the time delay caused by a digital control sys-63 tem. In Ref. 15, twofold of current sampling and duty cycle 64 updating were performed in a single carrier period, which 65 decreased the updating delay to half of that in traditional 66 PWM. Nevertheless, the disadvantage of these PWM-based 67 current control strategies has not been overcome 68 69 fundamentally.

Hysteresis Current Control (HCC)<sup>16</sup> is an alternative to 70 achieve high-performance current control. In HCC, the con-71 trol target is the bus current instead of the bus voltage, which 72 overcomes the inherent disadvantage of PWM-based current 73 control strategies. In addition, the simple structure, rapid 74 75 response speed, inherent overcurrent protection function, lower switching losses, and excellent control stability of this 76 strategy constitute the merits of HCC.<sup>17,18</sup> When HCC is 77 applied to a current control loop, stability can also be 78 achieved, although the outer speed control loop has a high 79 control gain. Hence, HCC is fairly suitable for applications 80 81 with high dynamical response. However, in traditional HCC, 82 the switching frequency of a power device (namely, the modu-83 lating frequency) varies with a change of the system working state, which causes a severe electromagnetic compatibility 84 problem and may result in an excessive switching frequency 85 that will damage the power device; this disadvantage hinders 86 the spread and application of HCC.<sup>19,20</sup> 87

Extensive work has been conducted to overcome the disad-88 vantages of HCC. The use of a flexible hysteresis band size is a 89 common way to achieve a fixed modulating frequency.<sup>21–27</sup>. In 90

these HCCs, the hysteresis band size is calculated in each 91 switching period in real time according to transient system 92 state variables. However, this calculation is computationally 93 expensive and suffers from stability problems.<sup>25</sup> Meanwhile, 94 other ways exist. In Ref. 28, to realize a fixed-frequency mod-95 ulation, the hysteresis band is removed, and the switch-on and 96 switch-off times are determined using the predicted reference 97 current, system behavior, and past time within a predefined 98 switching period. Comparing the real-time current with the 99 hysteresis bounds to determine the switching signal at a fixed frequency is another way to reach the target,<sup>29</sup> and if the hysteresis band size is set as zero, this current control strategy becomes similar to the bang-bang control.<sup>30</sup> Nevertheless, this strategy has the same problem concerning the sampling interval as that in PWM-based current control strategies. The triangular carrier-based fixed-frequency HCC strategy is a new way to obtain the fixed modulating frequency.<sup>31,32</sup> In this strategy, the triangular carrier technology and HCC are combined, and by tuning the amplitude of the carrier and the hysteresis band size, only a pair of switching signals is guaranteed to occur during a carrier period. However, strict constraints on the rising and descending rates of winding current are observed, and these constraints are usually ineffective in the unsteady state.

In this paper, a flexible-bound-size quasi-fixed-frequency 114 HCC based on the triangular carrier-based fixed-frequency 115 HCC is proposed to tackle the problem of traditional HCC. 116 The digitalization of the proposed HCC is conducted to 117 expand its feasible range to the entire running process. This 118 paper is organized as follows. In the second section, the math-119 ematical model of a BLDC motor using a PWM ON modula-120 tion mode is constructed. In the third section, the triangular 121 carrier-based fixed-frequency HCC is studied, and the new 122 method is applied to analyze constraints to realize a fixed-123 frequency modulation control. In the fourth section, based 124 on the results obtained in the third section, a new flexible-125 bound-size fixed-frequency HCC feasible during the entire run-126 ning process is proposed, and the process of obtaining the flex-127 ible bound size is analyzed. In the fifth section, simulations and 128 experiments are conducted to verify the effectiveness of the 129 newly proposed digital fixed-frequency HCC. Finally, conclu-130 sions are made in the last section. 131

#### 2. Modelling of a BLDC motor

In this paper, a Y-shaped BLDC motor is used as the research 133 target. This motor is driven by a three-phase inverter con-134 trolled using six steps for commutation, in which only two 135 phases conduct current at any time; for each phase, the con-136 ducting interval is 120 electrical degrees. For the modulation 137 of conducting current, a PWM ON modulation mode is used 138 to produce switching signals for power electronic devices. 139 Specifically, assumptions are made as follows: 140

- (1) The three-phase windings are perfectly symmetrical.
- (2) The back-ElectroMotive Force (back-EMF) is a trapezoidal wave of 120 electrical degrees.
- (3) The stator core is unsaturated.

In addition, the armature reaction, eddy current, hysteresis 146 loss, and cogging effect are neglected. The simplified circuit 147 diagram of the BLDC motor and the three-arm power drive 148 Download English Version:

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